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ECE

PMI(B)

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Electromagnetic Theory

Books

Dr. Koteswara Rao

- William Hyte
- Sudhakar
- Edminister
- Mahapatra & Mahapatra
- R.F. Harrington
- Jordan & Balmain



# ★ Topics

D: 24/08/13 3

✓ ⊙ Static fields (Electrostatics & steady magnetics).

→ The fields are independent of time. is called static fields.

✓ ⊙ Time Varying fields

→ Maxwell Eq<sup>n</sup>.

✓ ⊙ EM Waves.

- Def<sup>n</sup>:

→ A wave is a physical phenomena which reproduces after certain instant of time get some other place, the time delay bet<sup>n</sup> the prior to the later locations is proportional to travelled distance. The whole phenomena constitutes a wave. Therefore, an EM waves is not only f<sup>n</sup> of time but also a f<sup>n</sup> of distance. Instead of distance we use space co-ordinates.

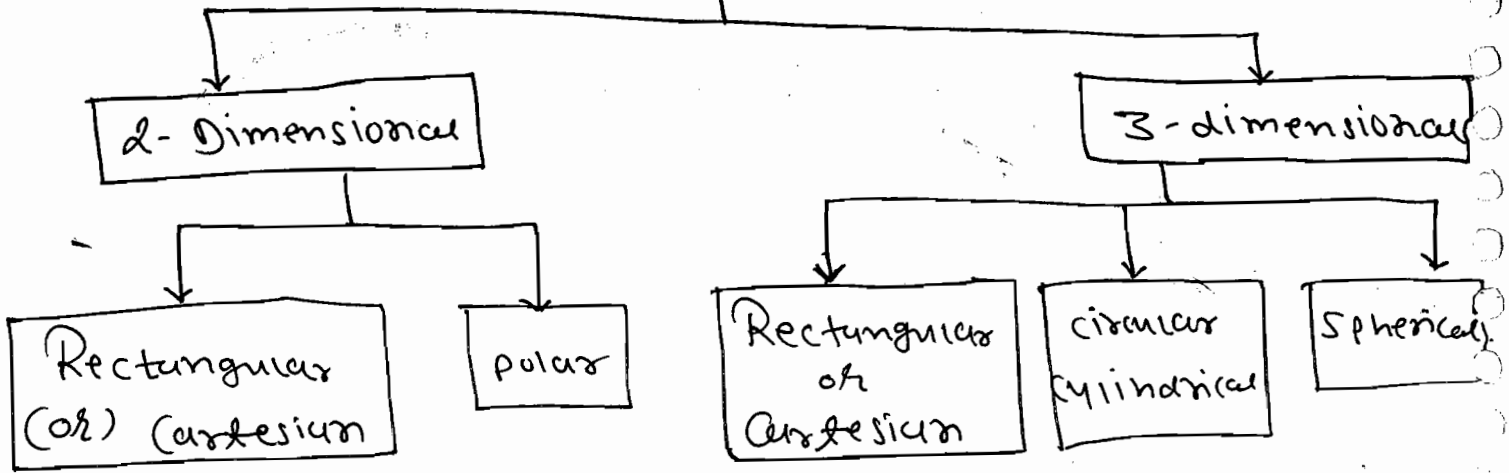
✓ ⊙ Waveguide (Rectangular)

⊙ Basics of Antennas

✓ ⊙ Two wire transmission lines.

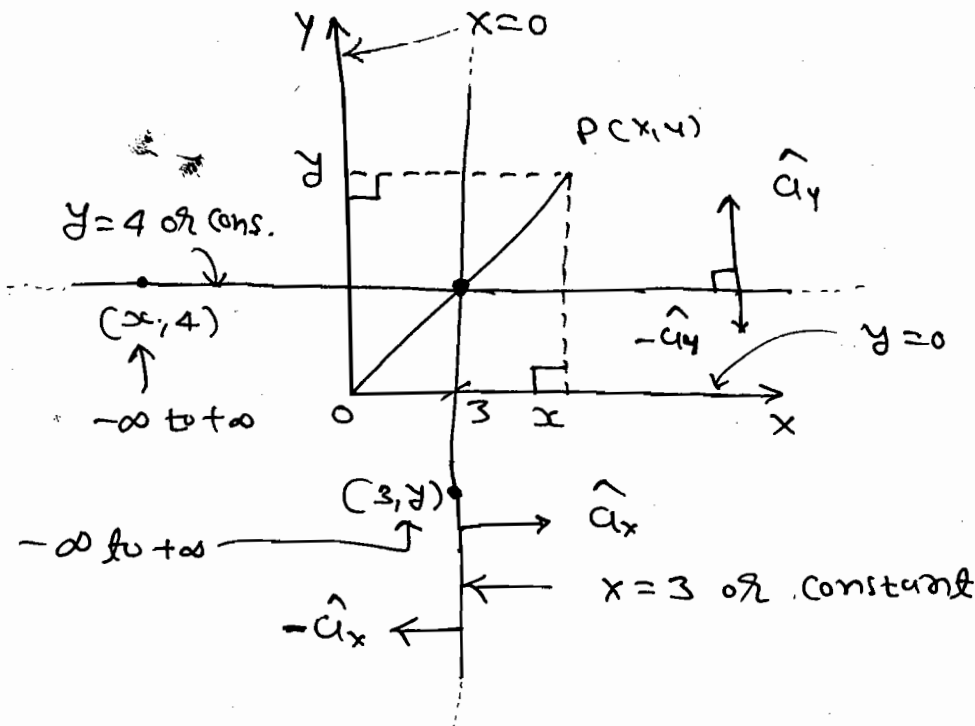
✓ ⊙ Scattering Parameters.

# Coordinate Systems.



\* 2-Dimensional:

(i) Rectangular (or) Cartesian



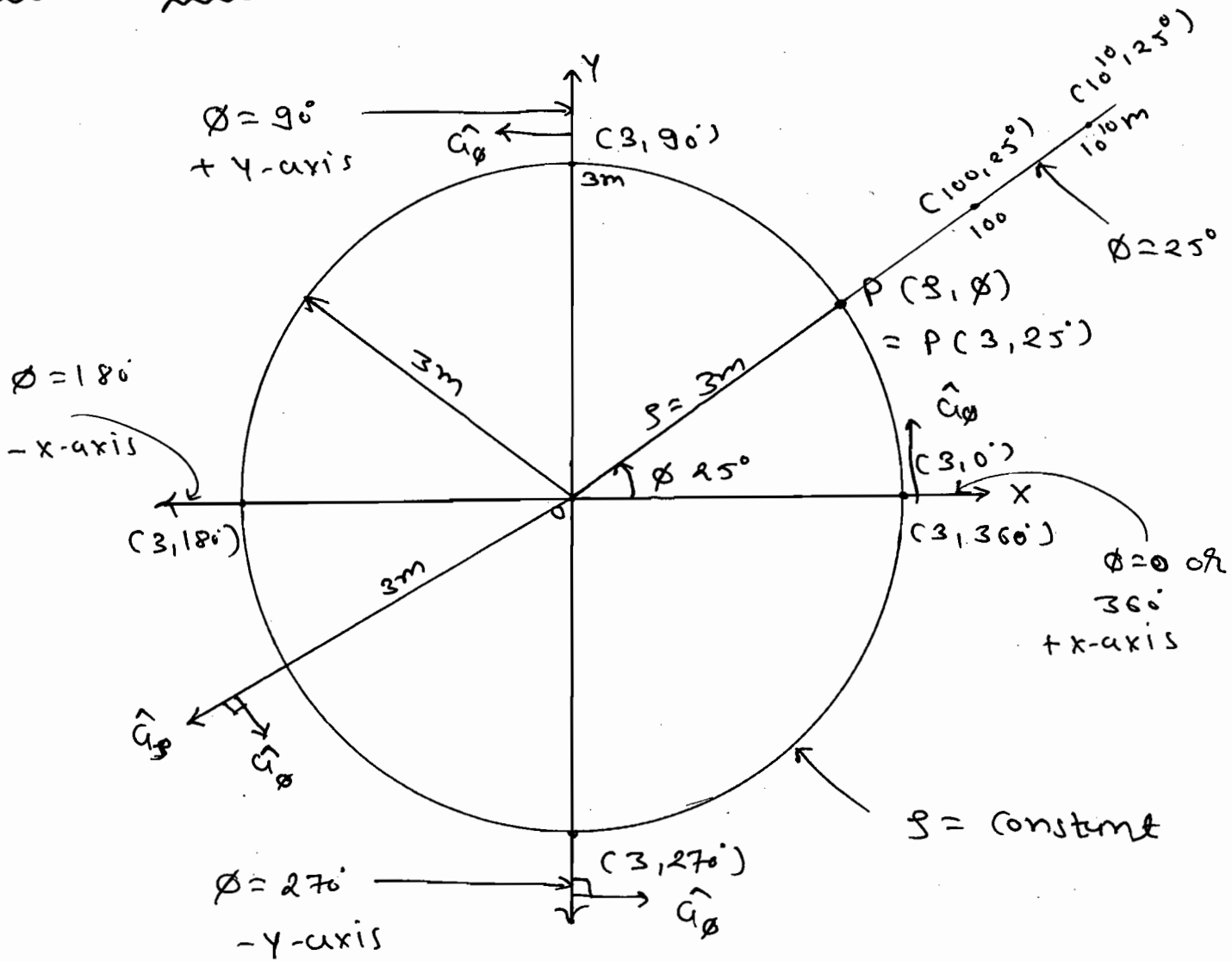
Integral	on $x = \text{const.}$	on $y = \text{const.}$
$x \rightarrow -\infty \text{ to } +\infty$	$y \rightarrow -\infty \text{ to } +\infty$	$x \rightarrow -\infty \text{ to } +\infty$
$y \rightarrow -\infty \text{ to } +\infty$		

→  $\hat{a}_x, \hat{a}_y$  are unit vectors and are orthogonal to each other.  $\Rightarrow |\hat{a}_x| = |\hat{a}_y| = 1.$

→ They are represented along x-axis and along y-axis respectively.

→ They may be also represented as unit vectors normal to  $x = \text{constant}$  and  $y = \text{constant}$  respectively.

(ii) Polar



→ Locus of  $S = \text{constant}$  represents a circle whose centre coincides with the origin. Therefore,  $S$  assumes all possible values ranging from 0 to  $\infty$ . All  $S = \text{constant}$ ,  $\phi$  assumes all possible values ranging from 0 to  $2\pi$ .

Integrals	on $\rho = \text{const.}$	on $\phi = \text{const.}$
$\rho \rightarrow 0 \text{ to } \infty$	$\phi \rightarrow 0 \text{ to } 2\pi$	$\rho \rightarrow 0 \text{ to } \infty$
$\phi \rightarrow 0 \text{ to } 2\pi$		

→ Locus of  $\phi = \text{constant}$  is a line emerging out from the origin.  $\phi$  assumes all possible values ranging from 0 to  $2\pi$ .

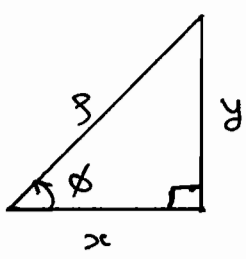
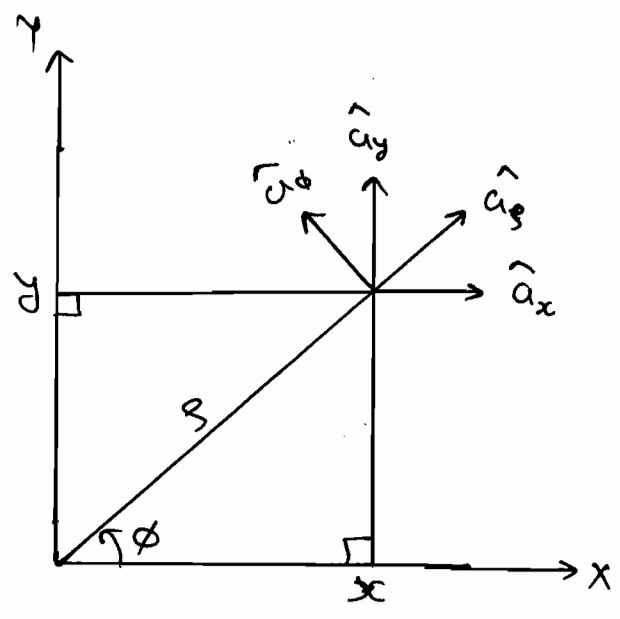
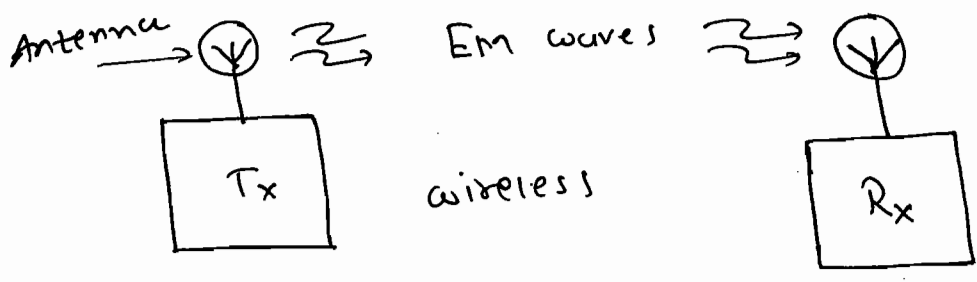
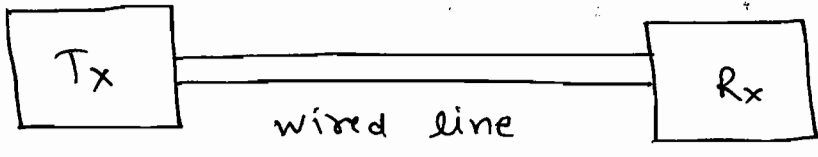
On  $\phi = \text{constant}$   $\rho$  assumes all possible values ranging from 0 to  $\infty$ .

→  $\hat{a}_\rho$  &  $\hat{a}_\phi$  are unit vectors orthogonal to each other.

→  $\hat{a}_\rho$  is represented normal to  $\rho = \text{constant}$  (OR) normal to the circle.

→ Similarly,  $\hat{a}_\phi$  is a unit vector projecting normal to  $\phi = \text{constant}$ , and it is projecting in the counter clock wise direction as shown in figure.

→  $\hat{a}_\rho$  is normal to the circle and  $\hat{a}_\phi$  is tangent to the circle.

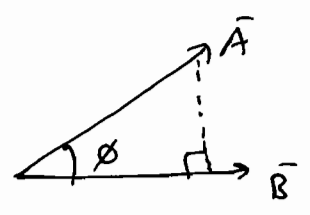


$$\rightarrow y = s \sin \phi$$

$$x = s \cos \phi$$

$$s = \sqrt{x^2 + y^2}$$

$$\phi = \tan^{-1}(y/x)$$



$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cdot \cos \phi$$

$$= AB$$

if  $\phi = 0$ .

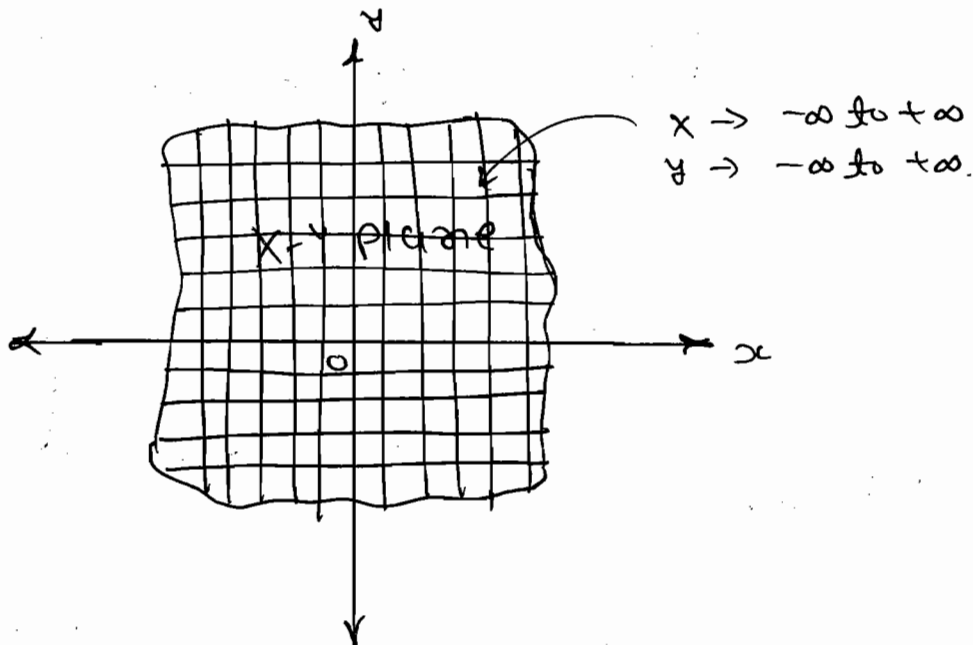


	$\hat{a}_1$	$\hat{a}_\phi$	$\hat{a}_2$
$\hat{a}_x$	$\cos\phi$	$-\sin\phi$	0
$\hat{a}_y$	$\sin\phi$	$\cos\phi$	0
$\hat{a}_z$	0	0	1

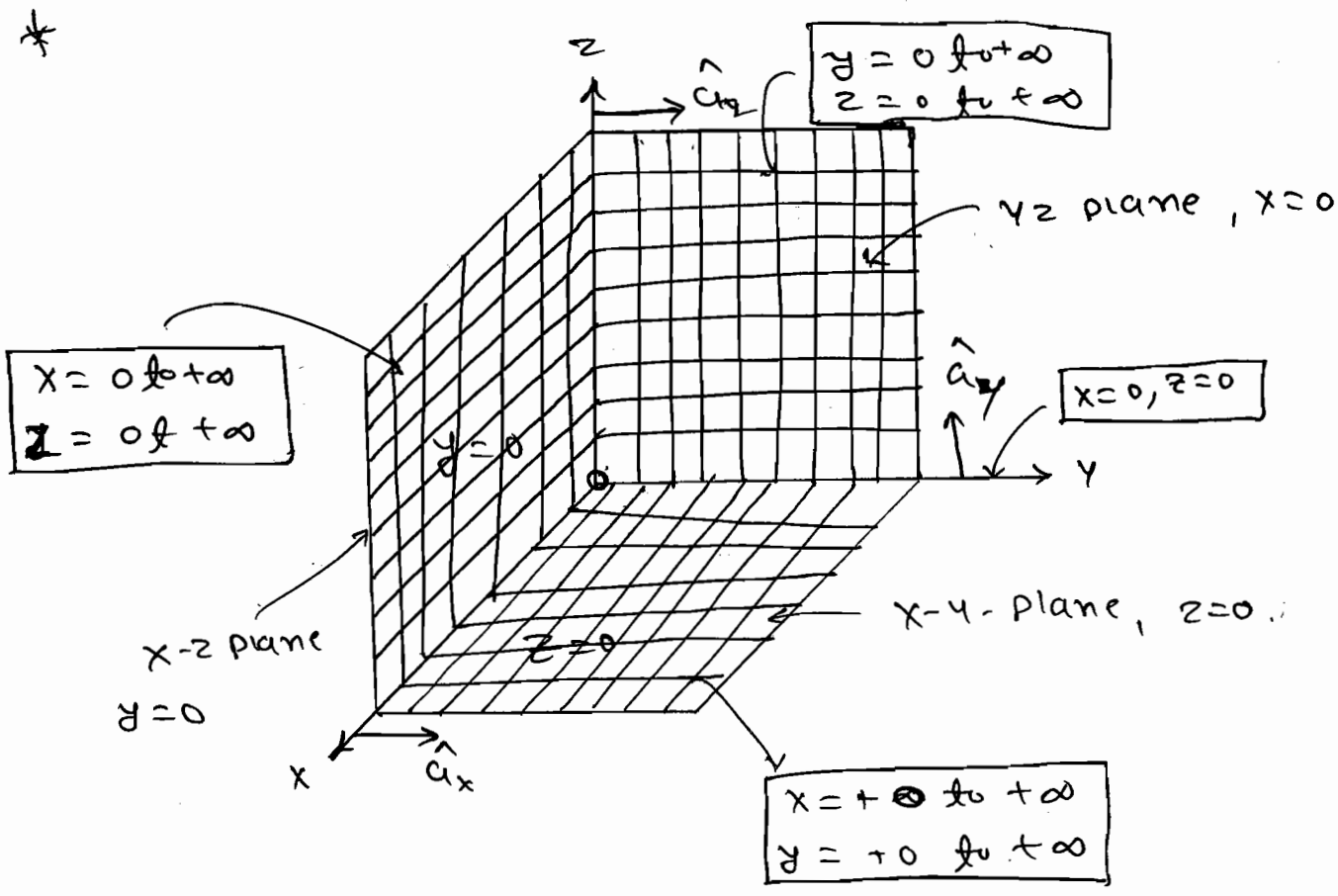


Plane:

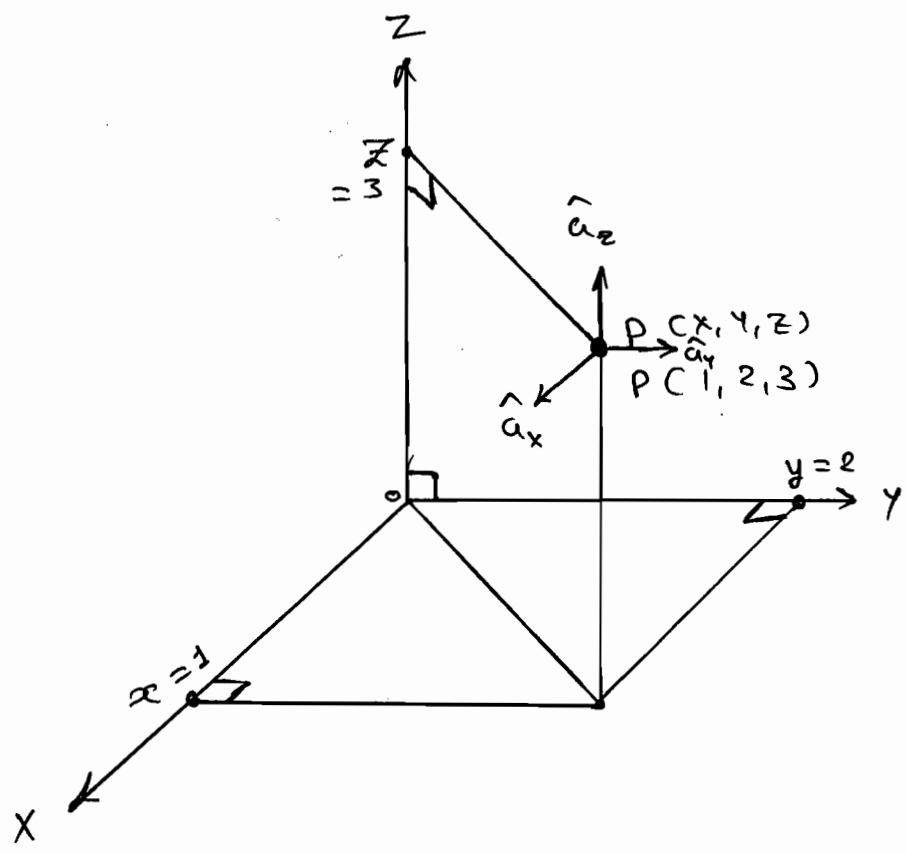
→ Plane is a sheet like structure whose thickness is neglected.







\* Cartesian Coordinates System



→ In general in a 3-D Co-ordinates system fixing 3 coordinates that represents a point

- fixing 2 coordinates that represents a line
- fixing 1 co-ordinates that represents a plane.

⇒ In general

$$x \rightarrow -\infty \text{ to } +\infty$$

$$y \rightarrow -\infty \text{ to } +\infty$$

$$z \rightarrow -\infty \text{ to } +\infty$$

⇒  $\hat{a}_x, \hat{a}_y, \hat{a}_z$  are unit vectors and orthogonal to each other.

$$\rightarrow |\hat{a}_x| = |\hat{a}_y| = |\hat{a}_z| = 1.$$

⇒  $\hat{a}_x, \hat{a}_y$ , and  $\hat{a}_z$  are unit vectors and orthogonal to each other.

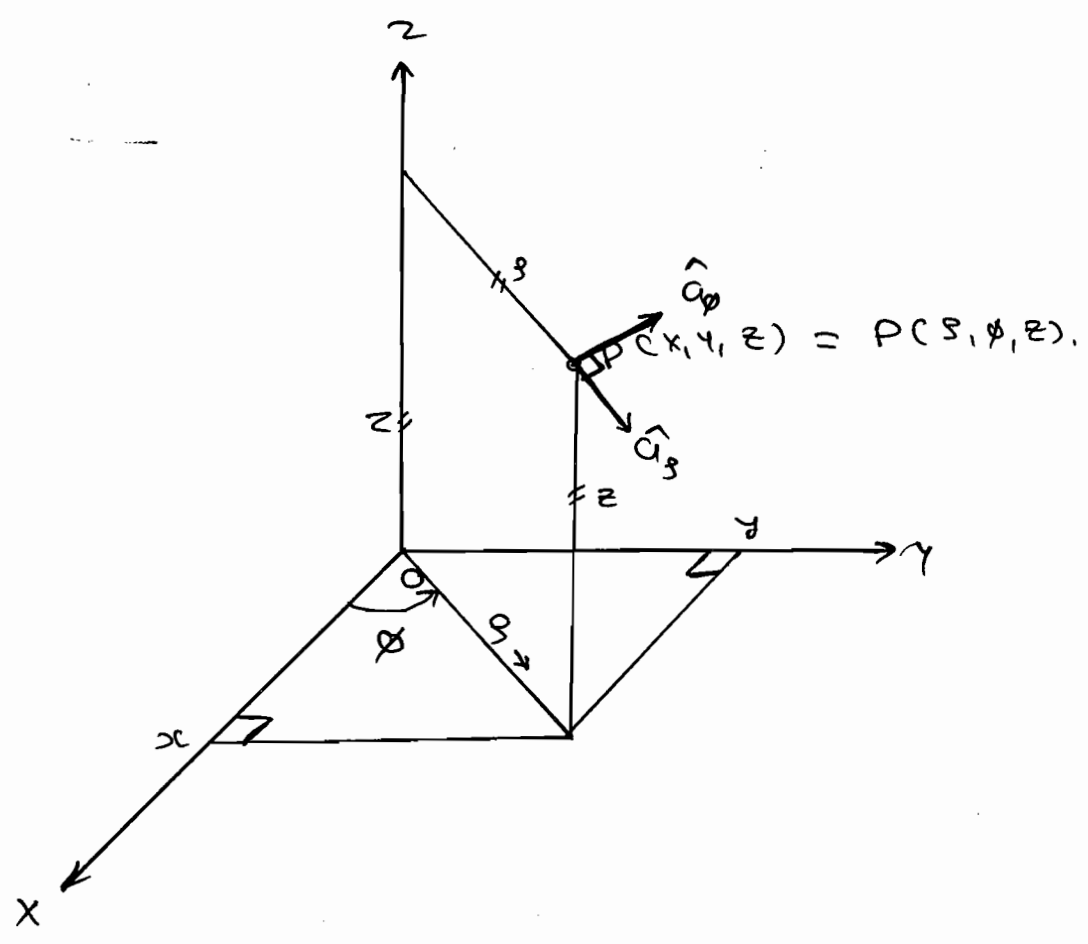
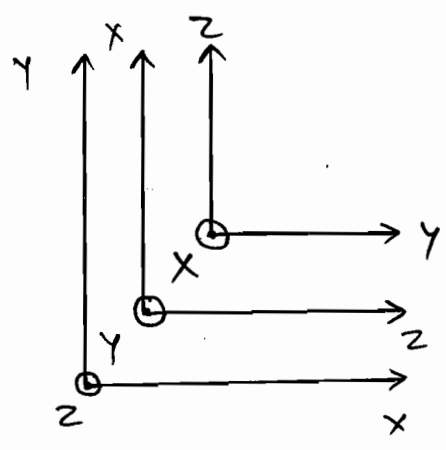
→ They are represented along x-axis, y-axis and z-axis.

→ They may be also represented as unit vectors normal to  $x = \text{constant}$ ,  $y = \text{constant}$ ,  $z = \text{constant}$  planes respectively.

\*  $\odot$  vector/x-axis coming out of the paper

\*  $\odot$  vectors / axis Coming out of the paper.

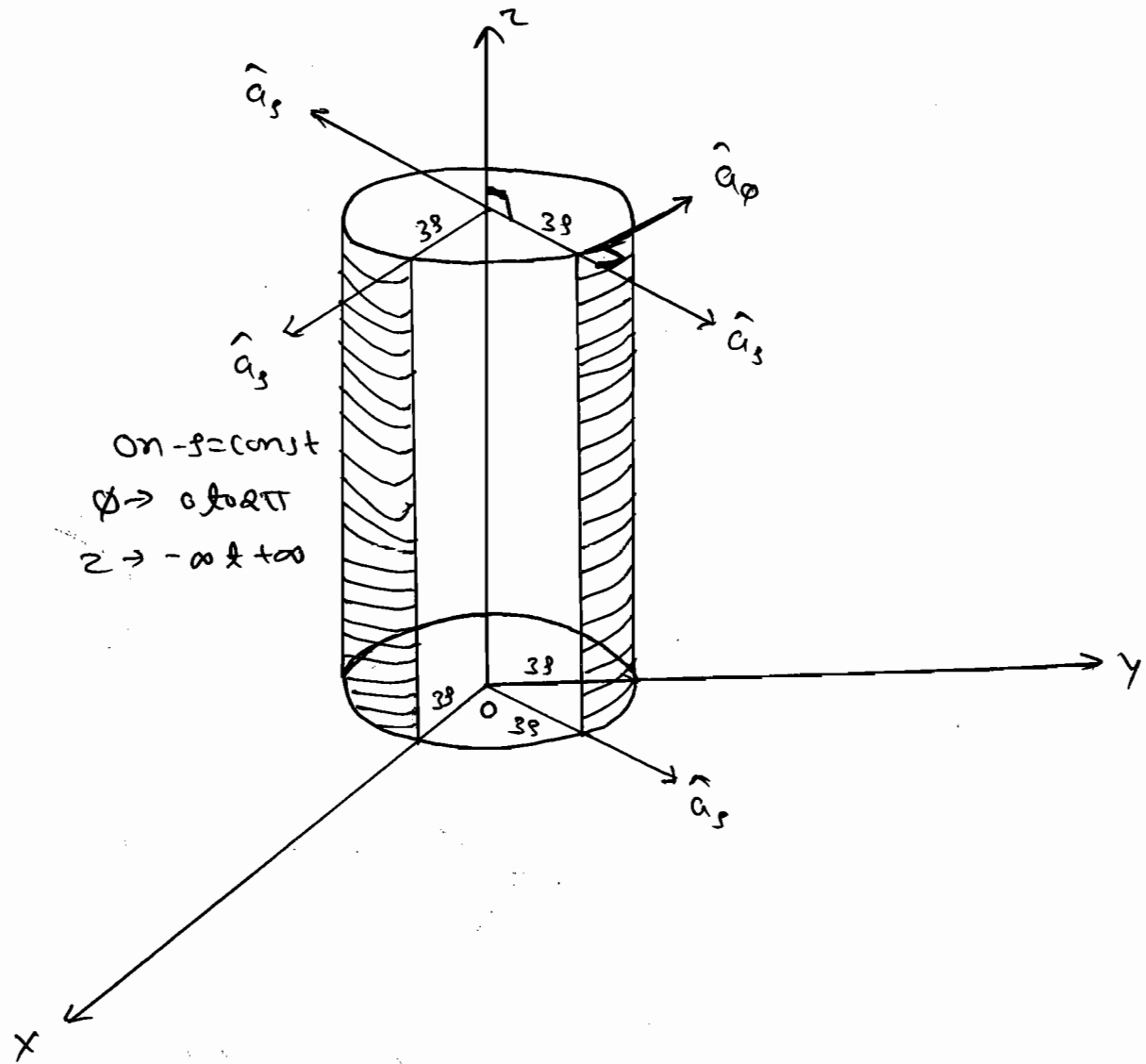
\* Circular or Cylindrical  
Coordinate System.



→  $\rho = \text{constant}$  represents a cylindrical plane whose cross-section is circular and whose axis coincides with z-axis.  $\rho$  is the distance measured normal to z-axis.  $\rho$  can assume all possible values ranging from 0 to  $\infty$ .

→  $\hat{a}_\phi$  is a unit vector projecting normal  
to  $\phi = \text{constant}$  plane.

⇒

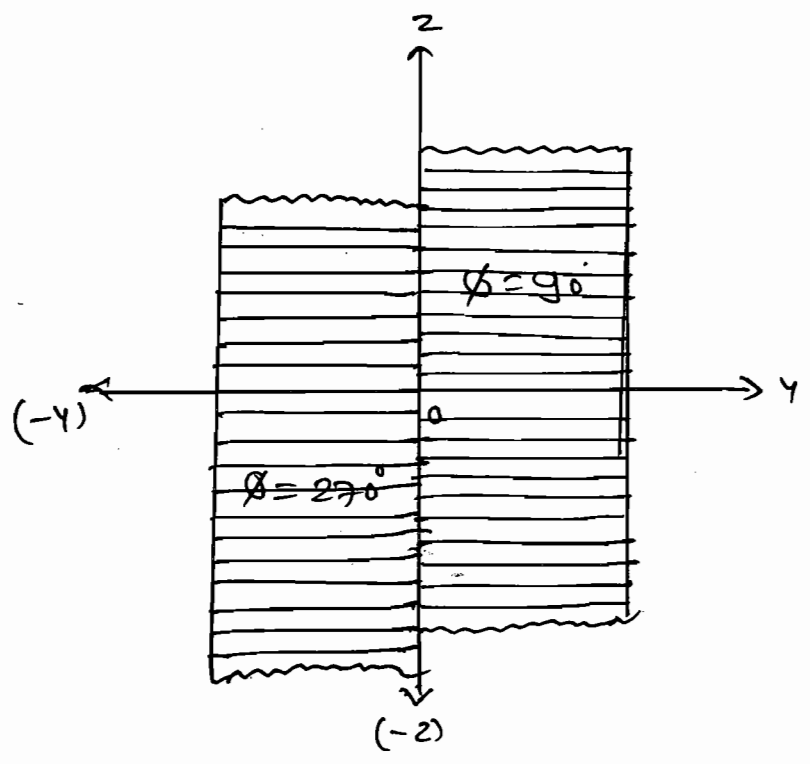
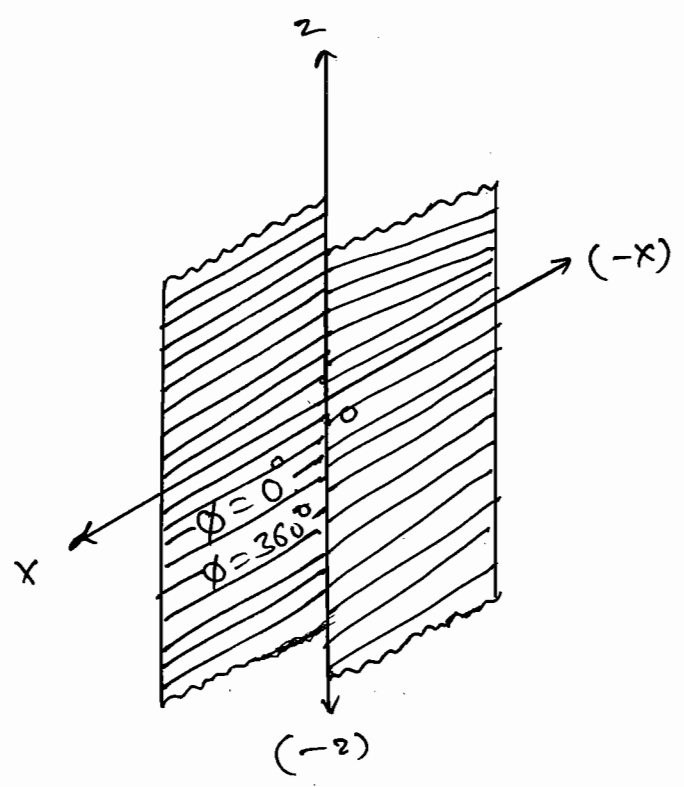


→  $\theta$  is called azimuth angle.

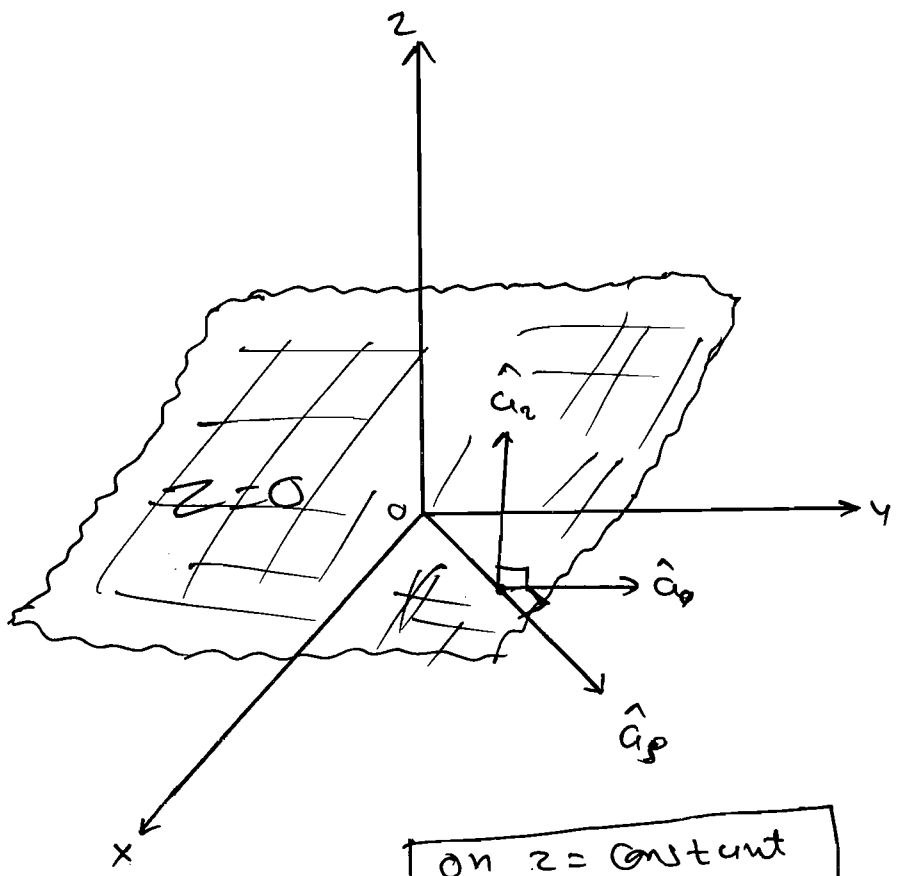
→  $\phi = \text{constant}$  plane is called elevation plane.

→  $\phi$  assumes all possible values ranging from  
 $0$  to  $2\pi$ .

→  $\hat{a}_\theta$  is a unit vector projecting normal  
to  $\theta = \text{constant}$  plane.



\*



on  $z = \text{constant}$   
 $s \rightarrow 0 \text{ to } \infty$   
 $\phi \rightarrow 0 \text{ to } 2\pi$

→ On a particular constant plane that particular unit vector would project normal to the plane then remaining 2 unit vectors could be projecting tangential to the plane.

for e.g. on  $s = \text{constant}$  plane  $\hat{a}_s$  could be projecting normal to  $s = \text{constant}$  and  $\hat{a}_\phi$  &  $\hat{a}_z$  could be projecting tangential to the plane.

In general

- $\rho \Rightarrow 0 \text{ to } \infty$
- $\phi \rightarrow 0 \text{ to } 2\pi$
- $z \rightarrow -\infty \text{ to } +\infty$

$\rightarrow \hat{a}_\rho, \hat{a}_\phi, \hat{a}_z$  are unit vectors and orthogonal to each other.

$\Rightarrow$  In general,

$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$	$\rightarrow$ cartesian
$\vec{B} = B_\rho \hat{a}_\rho + B_\phi \hat{a}_\phi + B_z \hat{a}_z$	$\rightarrow$ cylindrical

Ex-1 Let  $\vec{B} = 2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z$  is define at a point  $P(3, 4, 5)$  m. Convert this vector in cylindrical system.

Ans:

$$\vec{B} = B_\rho \hat{a}_\rho + B_\phi \hat{a}_\phi + B_z \hat{a}_z$$

$$\therefore \vec{B} \cdot \hat{a}_\rho = B_\rho \cdot \underbrace{\hat{a}_\rho \cdot \hat{a}_\rho}_1 + B_\phi \underbrace{\hat{a}_\phi \cdot \hat{a}_\rho}_0 + B_z \underbrace{\hat{a}_z \cdot \hat{a}_\rho}_0$$

$$\therefore \vec{B} \cdot \hat{a}_\rho = B_\rho$$

$$\therefore B_\rho = \vec{B} \cdot \hat{a}_\rho$$

$$\therefore B_\rho = 2\hat{a}_x \cdot \hat{a}_\rho + 3\hat{a}_y \cdot \hat{a}_\rho + 4\hat{a}_z \cdot \hat{a}_\rho$$

$$B_\rho = 2 \cos \phi + 3 \sin \phi + 0$$

Now,  $P(3, 4, 5)$ .

$$\therefore \rho = \sqrt{3^2 + 4^2} = 5$$

$$\phi = \tan^{-1} \left( \frac{4}{3} \right) = 53.13^\circ$$

$$\therefore B_3 = 2.6 \sin 53.13^\circ + 3 \sin 53.13^\circ$$

$$\therefore \boxed{B_3 = 3.6}$$

Similarly,

$$\therefore B_\phi = \vec{B} \cdot \hat{a}_\phi, \quad B_z = \vec{B} \cdot \hat{a}_z$$

$$\therefore B_\phi = -2 \sin \phi + 3 \cos \phi.$$

$$\therefore \boxed{B_\phi = 0.2}$$

$$\therefore B_z = \vec{B} \cdot \hat{a}_z$$

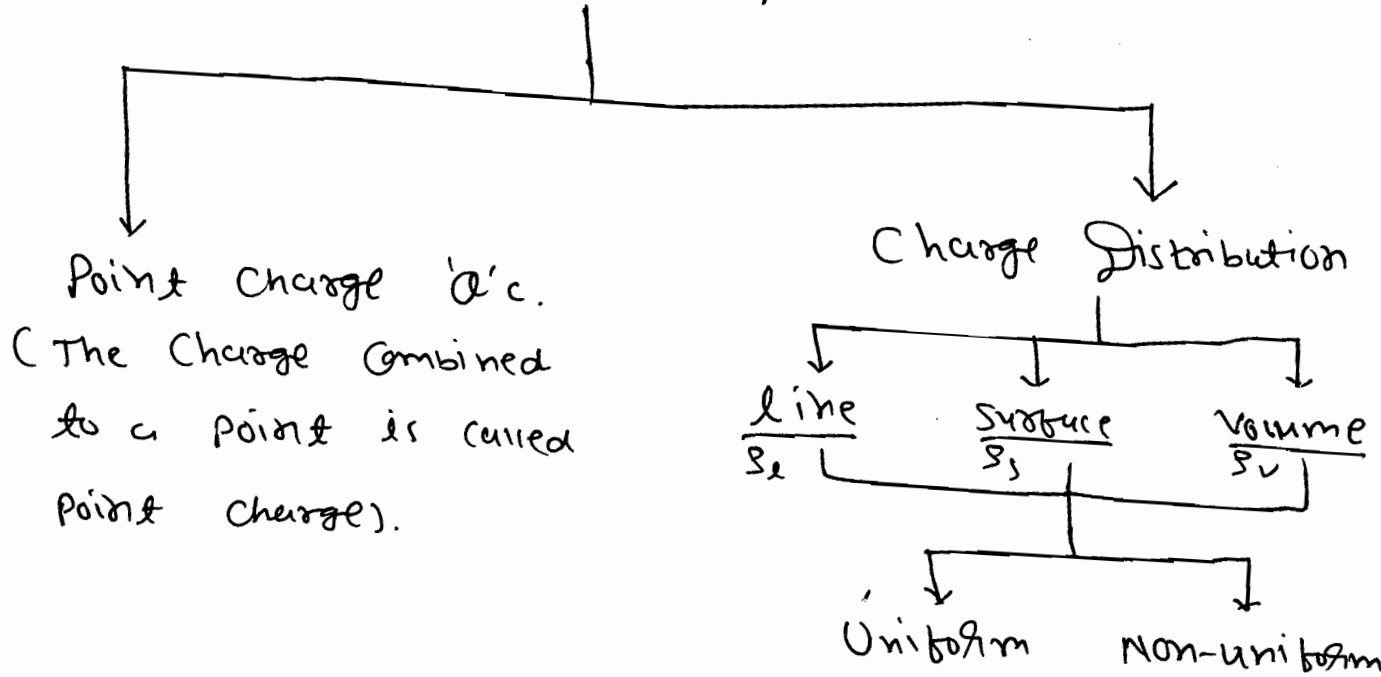
$$\therefore B_z = B_z$$

$$\therefore \boxed{B_z = 4}$$

$$\therefore \boxed{\vec{B} = 3.6 \hat{a}_3 + 0.2 \hat{a}_\phi + 4 \hat{a}_z}$$



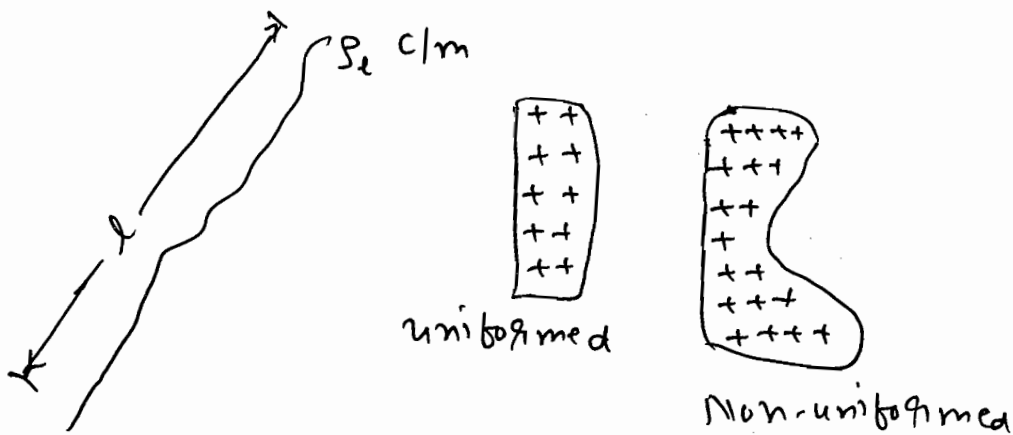
# Charge Configuration/Classification



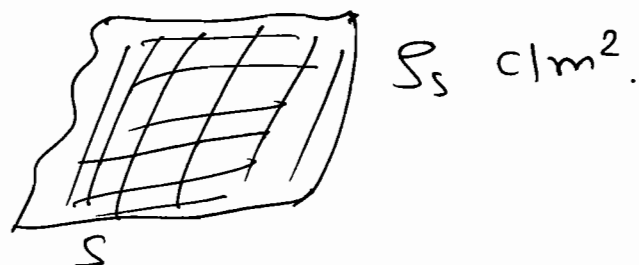
→ Distribution of Charge per unit line

is called line charge distribution if and is designated by  $\rho_L$ . If  $\rho_L$  is constant that may be called uniform otherwise nonuniform.

→ Having uniform charge distributions are impractical. The reason is due to mutual repulsion bet<sup>n</sup> the like charges.



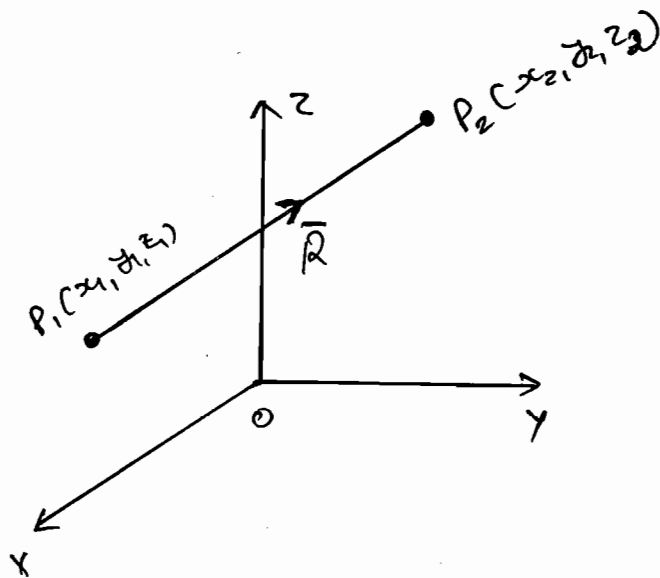
→ Distribution of charge per unit area is called surface charge density and is designated by  $\rho_s \text{ C/m}^2$



→ Distribution of charge per unit volume is called Volume charge density and is designated by  $\rho_v \text{ C/m}^3$



\*



→ R is vector drawn from P<sub>1</sub> to P<sub>2</sub>.

$$\therefore \vec{R} = (x_2 - x_1)\hat{a}_x + (y_2 - y_1)\hat{a}_y + (z_2 - z_1)\hat{a}_z$$

$$\therefore |\vec{R}| = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

$$\hat{a}_R = \frac{\vec{R}}{|\vec{R}|} \quad \vec{a}_R = \text{unit vector components of R.}$$

$$|\hat{a}_R| = \frac{|\vec{R}|}{|\vec{R}|} = 1.$$

\* ~~Electrostatic~~ ~~Force~~ ~~Law~~ Coulomb's Force Law:  
→ it gives force of attraction (or) repulsion

bet<sup>n</sup> charge conducting bodies.

→ if the charges are like the force is repulsive otherwise attractive.

→ Capacitivity (or) Permittivity specifies property  
of a medium and that indicates ability  
to store electrical energy.

$$F \propto Q_1 Q_2 \\ \propto \frac{1}{|\vec{R}|^2}$$

$$E = \epsilon_0 \epsilon_r \quad \text{F/m}$$

$$\therefore |\vec{F}| = \frac{Q_1 Q_2}{4\pi\epsilon |\vec{R}|^2} \text{ N}$$

$$\rightarrow E = \epsilon_r \epsilon_0 \quad \text{F/m}$$

E : Permittivity (or) capacitivity

ε<sub>0</sub> : Absolute permittivity → 8.854 × 10<sup>-12</sup> F/m

ε<sub>r</sub> = relative permittivity  $\epsilon_r = \frac{10^{-9}}{36\pi} \text{ F/m.}$

(c) Dielectric constant has no unit.  
( $\epsilon_r$ )

→ The vector force <sup>acting</sup> on  $Q_2$  due to  $Q_1$  ~~charge~~ is given by.

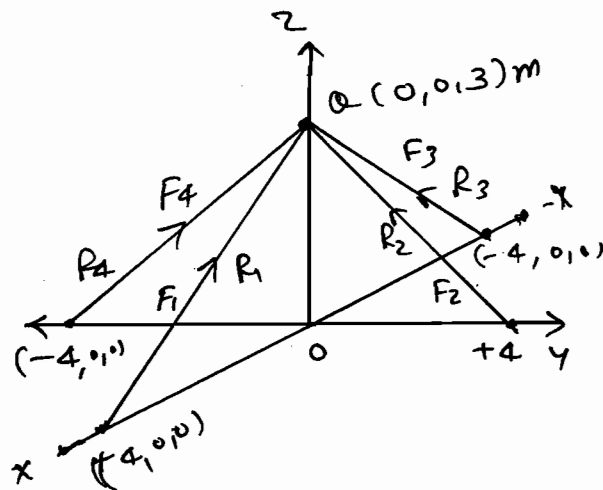
$$\therefore \vec{F} = \frac{Q_1 \cdot Q_2}{4\pi\epsilon |\vec{R}|^2} \cdot \hat{C}_R$$

$$\vec{F} = \frac{Q_1 \cdot Q_2}{4\pi\epsilon |\vec{R}|^2} \cdot \frac{\vec{R}}{|\vec{R}|} \quad \text{N}$$

→ The vector force acting on  $Q_1$  due to  $Q_2$  is  $-\vec{F}$ .  
further we write  $|\vec{F}| = |-\vec{F}|$

Ex-1 Four point charges of  $1\text{mc}$  each one located on the x & y axis at  $\pm 4\text{m}$ .  
Find the vector force acting on  $1\text{mc}$  charge which is located on z-axis  
at  $z = 3$  meters.

Ans:



$$\vec{F}_1 = \frac{10 \times 10^{-6} \times 10^{-3}}{4\pi \times \frac{10^{-9}}{36\pi} \times (5)^2} \times \frac{-4\hat{a}_x + 3\hat{a}_z}{(5)} \quad 21$$

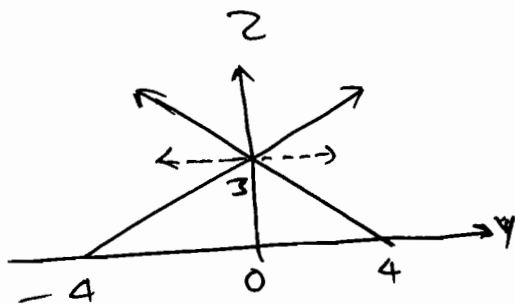
$$\vec{F}_2 = \frac{10 \times 10^{-6} \times 10^{-3}}{4\pi \times \frac{10^{-9}}{36\pi} \times (5)^2} \times \frac{-4\hat{a}_y + 3\hat{a}_z}{(5)}$$

$$\vec{F}_3 = \frac{10 \times 10^{-6} \times 10^{-3}}{4\pi \times \frac{10^{-9}}{36\pi} \times (5)^2} \times \frac{+4\hat{a}_x + 3\hat{a}_z}{(5)}$$

$$F_4 = \frac{10 \times 10^{-6} \times 10^{-3}}{4\pi \times \frac{10^{-9}}{36\pi} \times (5)^2} \times \frac{+4\hat{a}_y + 3\hat{a}_z}{(5)}$$

$$\therefore \vec{F} = \vec{F}_1 + \vec{F}_2 + \vec{F}_3 + \vec{F}_4$$

$$\boxed{\vec{F} = 8.64 \hat{a}_z \text{ N}}$$

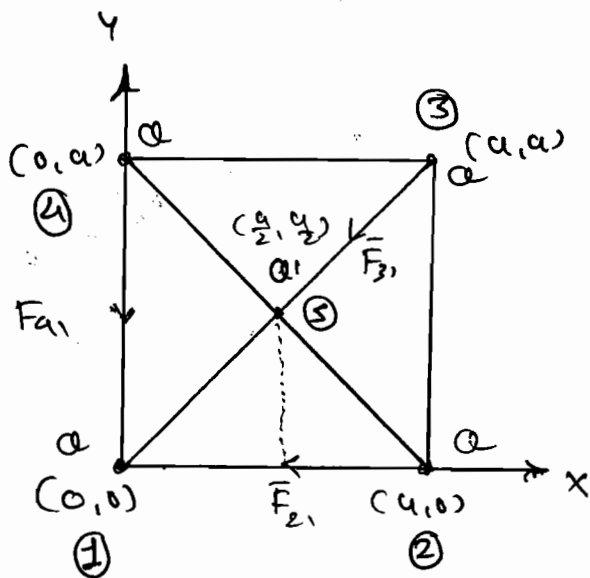


→ The 10 μC charges are located symmetrically on the x & y axis, about z-axis which results in cancellation of horizontal force components and the resultant force would be along  $\hat{a}_z$  direction only.

Ex-2 4 point charges of  $+q$  each are located at the corners of a square. What point charge to be kept at a centre of a square so that the resultant force acting on any charge which are located at a corner of a square is zero. (Or) it is required to hold 4 point charges of  $+q$  each in equilibrium at corners of a square. What point charge to be kept at the centre of the square so that the charges would be in equilibrium.

Hint: equilibrium means the resultant force acting on any charge which are located at the corners of the square is zero.

Ans:



→ We have to find value of  $q'$  in terms of  $q$  so that resultant force acting on any charge which are located at the corners of the square is zero.

for e.g.

Let's find force on ①

$$\therefore \vec{F}_{21} + \vec{F}_{31} + \vec{F}_{41} + \vec{F}_{51} = 0.$$

$$\Rightarrow \vec{F}_{21} = \frac{Q^2}{4\pi\epsilon (a^2)} \times \frac{-a\hat{a}_x}{a}$$

$$\vec{F}_{41} = \frac{Q^2}{4\pi\epsilon (a^2)} \times \frac{-a\hat{a}_y}{a}$$

$$\vec{F}_{31} = \frac{Q^2}{4\pi\epsilon (\sqrt{2}a)^2} \times \frac{-a\hat{a}_x - a\hat{a}_y}{\sqrt{2}a}$$

$$\therefore \vec{F}_{51} = \frac{Qq}{4\pi\epsilon \left(\frac{a}{\sqrt{2}}\right)^2} \times \frac{-\hat{a}_x - \hat{a}_y}{\sqrt{2}}$$

→ Consider the sum and of  $\hat{a}_x$  components of all forces and the same make equals to 0

$$\therefore \frac{-Q^2}{4\pi\epsilon a^2} - \frac{Q^2}{4\pi\epsilon \sqrt{2}a^2} - \frac{Qq}{4\pi\epsilon \frac{a^2}{\sqrt{2}}} = 0$$

$$\therefore q = -0.956a.$$

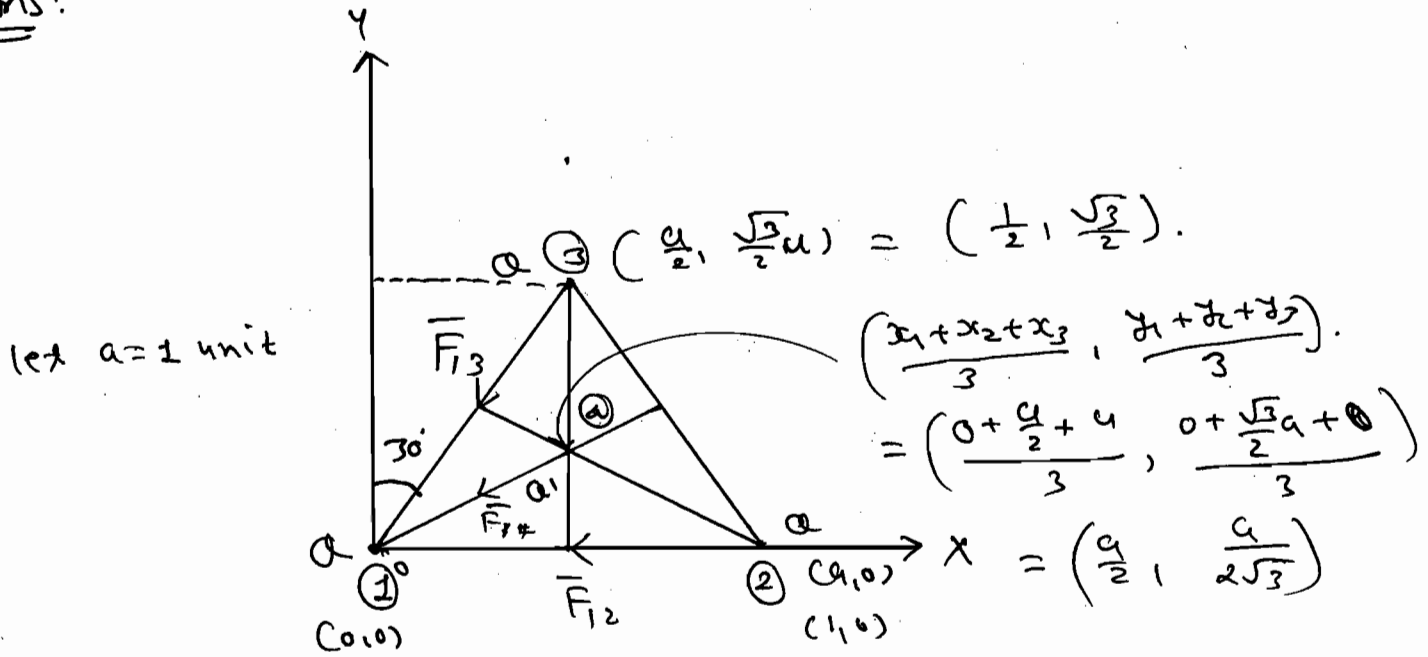
→ Even we consider the sum of  $\hat{a}_y$  components the same ans is expected.

✓  
→

Ex-3 3 point charges of +q each are located at the corners of an equilateral triangle. What point charge to be kept at the centre of the triangle so that the resultant force acting on any charge which are located at the corners of the triangle is 0.

Ans:  $q' = -\frac{q}{3}$

Ans:



$$\Rightarrow \vec{F}_{13} = \frac{kq^2}{1} (-\hat{a}_{x2} - \sqrt{3}\hat{a}_{y4}) \quad \vec{R} = -\frac{q}{2}\hat{a}_{x2} - \frac{\sqrt{3}}{2}q\hat{a}_{y4}$$

$$\vec{R} = -\frac{q}{2}\hat{a}_{x2} - \frac{\sqrt{3}}{2}q\hat{a}_{y4}$$

$$\Rightarrow \vec{F}_{12} = \frac{-kq^2}{1} (\hat{a}_{x2}) \quad \vec{R} = -q\hat{a}_{x2}$$

$$|\vec{R}| = 1$$

$$\Rightarrow \vec{F}_{14} = \frac{-kqaq'}{\frac{1}{3}} \times \left( +\frac{\hat{a}_{x2}}{2} + \frac{1}{2\sqrt{3}}\hat{a}_{y4} \right)$$

$$\vec{R} = -\frac{q}{2}\hat{a}_{x2} - \frac{1}{2\sqrt{3}}q\hat{a}_{y4}$$

$$|\vec{R}| = \sqrt{\frac{1}{4} + \frac{1}{12}} = \sqrt{\frac{1}{3}}$$



$$\Rightarrow \overline{F_{14}} = -k\alpha\alpha' \times \frac{3\sqrt{3}}{2} \left( \hat{a}_x + \hat{a}_y \times \frac{1}{\sqrt{3}} \right)$$

Now,  $\overline{F_{12}} + \overline{F_G} + \overline{F_{14}} = 0.$

$\therefore$  let, only  $\hat{a}_x$  - a component

$$\therefore \frac{-k\alpha^2}{2} - k\alpha^2 - k\alpha\alpha' \times \frac{3\sqrt{3}}{2} = 0.$$

$$\therefore -\frac{3}{2}\alpha = \alpha' \times \frac{3\sqrt{3}}{2}$$

$$\alpha' = -\frac{\alpha}{\sqrt{3}}$$

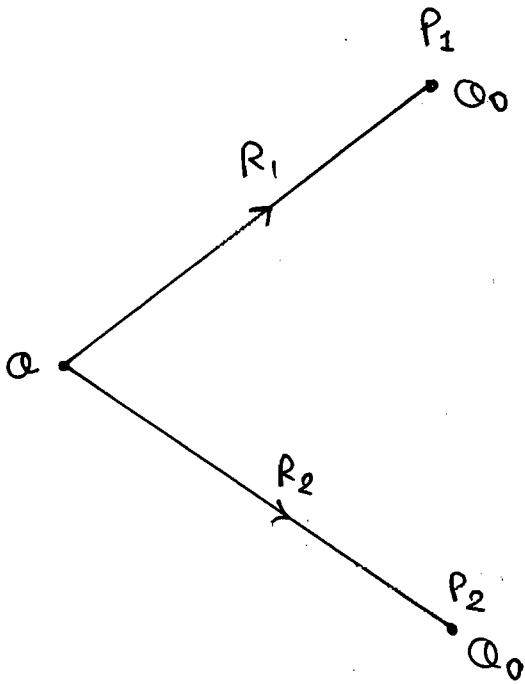
$$\alpha' = \frac{-\alpha}{\sqrt{3}} c$$

$\rightarrow$  If we considered only y-component then we also get same answers.

## \* Electric Field ( $\vec{E}$ ):-

→ It is defined as force per unit charge.

→ Unit is  $N/C$  (or)  $V/m$ .



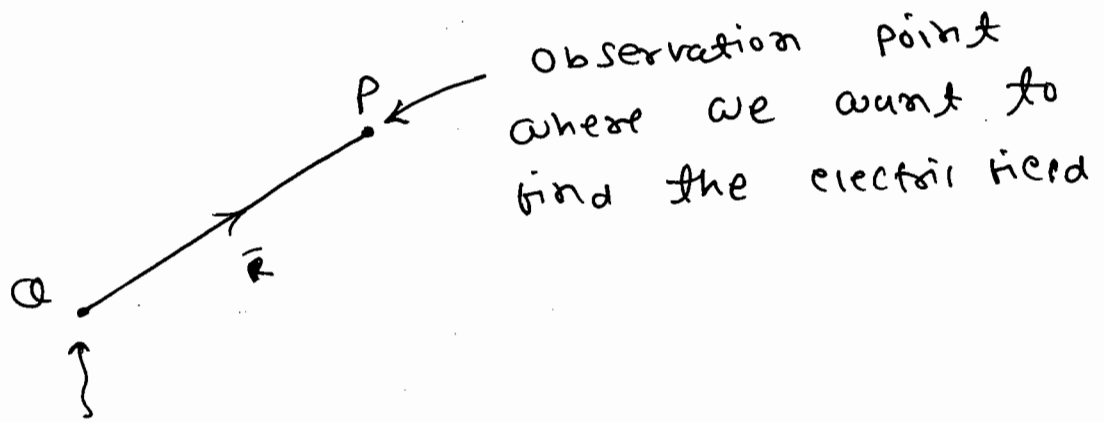
$$\rightarrow \vec{F}_1 = \frac{Q \cdot Q_0}{4\pi\epsilon |\vec{R}_1|^2} \cdot \hat{a}_{R_1}$$

$$\text{At } P_1 \Rightarrow \frac{\vec{F}_1}{Q_0} = \frac{Q}{4\pi\epsilon |\vec{R}_1|^2} \cdot \hat{a}_{R_1} = \text{Electric field}$$

$$\rightarrow \vec{F}_2 = \frac{Q \cdot Q_0}{4\pi\epsilon |\vec{R}_2|^2} \cdot \hat{a}_{R_2}$$

$$\text{At } P_2 \Rightarrow \frac{\vec{F}_2}{Q_0} = \frac{Q}{4\pi\epsilon |\vec{R}_2|^2} \cdot \hat{a}_{R_2} = \text{Electric field}$$

⇒ In general

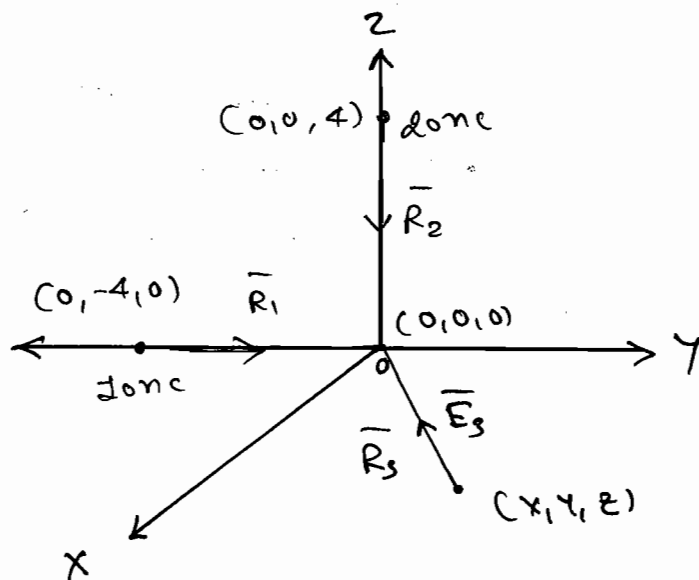


Source point,  
Source of electric field  
is electric charge.

$$\vec{E} = \frac{q}{4\pi\epsilon_0 |\vec{r}|^2} \hat{r}$$
$$\vec{E} = \frac{q}{4\pi\epsilon_0 |\vec{r}|^2} \times \frac{\vec{r}}{|\vec{r}|}$$

- ★  
Ex-1 A point charge of  $10\text{ nC}$  is located at  $(0, -4, 0)\text{ m}$ . Another charge of  $20\text{ nC}$  is located at  $(0, 0, 4)\text{ m}$ .
- (i) find the electric field at the origin.  
(ii) Where should a  $30\text{ nC}$  point charge be located so that electric field at origin is 0.

Ans:



$$\vec{E}_1 = \frac{10 \times 10^{-9}}{4\pi\epsilon_0 \times (4)^2} \times \frac{4 \hat{a}_y}{(4)} = 5.625 \hat{a}_y \text{ V/m}$$

$$\vec{E}_2 = \frac{20 \times 10^{-9}}{4\pi \times \frac{20 \times 10^{-9}}{36\pi} (4)^2} \times \frac{-4 \hat{a}_z}{4} = -11.25 \hat{a}_z \text{ V/m.}$$

① Electric field at the origin

$$= \vec{E}_1 + \vec{E}_2 = (5.625 \hat{a}_y - 11.25 \hat{a}_z) \text{ V/m.}$$

②  $\vec{E}_1 + \vec{E}_2 + \vec{E}_3 = 0 \Rightarrow \vec{E}_3 = -(\vec{E}_1 + \vec{E}_2).$

$$\therefore \vec{E}_3 = -[5.625 \hat{a}_y - 11.25 \hat{a}_z] \text{ V/m.}$$

$$\rightarrow \vec{E}_3 = \frac{30 \times 10^{-9}}{4\pi \times \frac{10^{-9}}{36\pi} \times (x^2 + y^2 + z^2)^{3/2}} \times (-x \hat{a}_x + (-y) \hat{a}_y - z \hat{a}_z)$$

$$\vec{E}_3 = \frac{270}{(x^2 + y^2 + z^2)^{3/2}} (-x \hat{a}_x - y \hat{a}_y - z \hat{a}_z)$$

$$\Rightarrow \text{Compare } \hat{a}_x \Rightarrow x=0$$

$$\text{Compare } \hat{a}_y \Rightarrow \frac{-270y}{(y^2+z^2)^{3/2}} = -5.625 \quad \text{--- (A)}$$

$$\text{Compare } \hat{a}_z \Rightarrow \frac{-270z}{(y^2+z^2)^{3/2}} = 11.25 \quad \text{--- (B)}$$

$$\frac{\text{(A)}}{\text{(B)}} \Rightarrow -\frac{y}{z} = \frac{1}{2} \Rightarrow \boxed{\frac{z}{y} = -2}$$

$$\text{from (A)} \quad \therefore \frac{270y}{y^3 [1 + (z/y)^2]^{3/2}} = 5.625.$$

$$\Rightarrow \frac{270y}{y^3 [1 + 4]^{3/2}} = 5.625.$$

$$\therefore y = \pm 2.07 \text{ m}$$

$$z = -2y = \mp 4.14 \text{ m.}$$

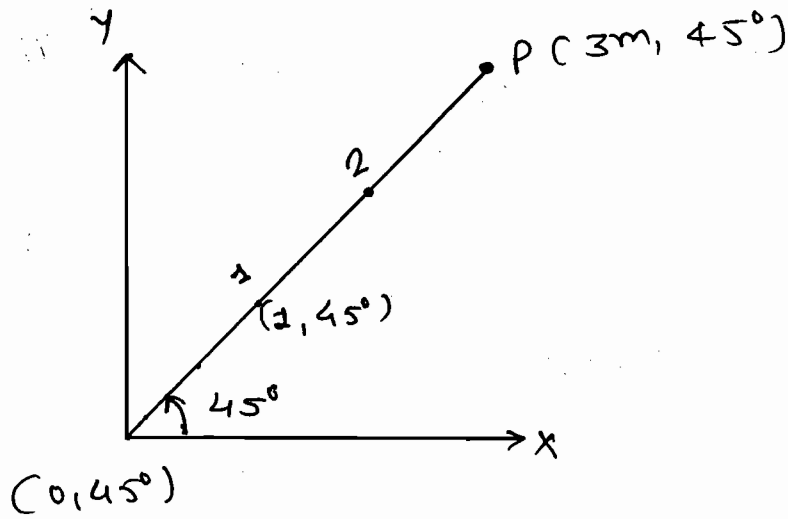
The possibilities.

$$(0, 2.07, -4.14) \checkmark$$

$$(0, -2.07, 4.14) \times$$

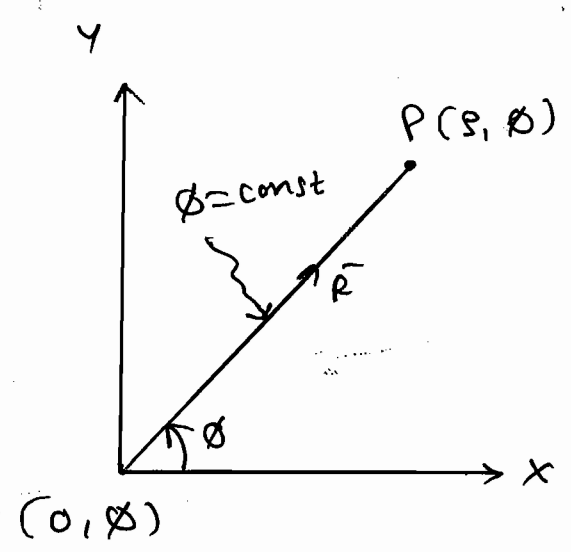
$$\therefore \text{Ans: } (0, 2.07, -4.14) \text{ m}$$

\*



→ We assume that the origin lines on  $\phi = 45^\circ$  line.

→ With ref. to  $P(3m, 45^\circ)$ , the origin is coordinated as  $(0m, 45^\circ)$



(origin lines on  $\phi = \text{const. lines}$ )

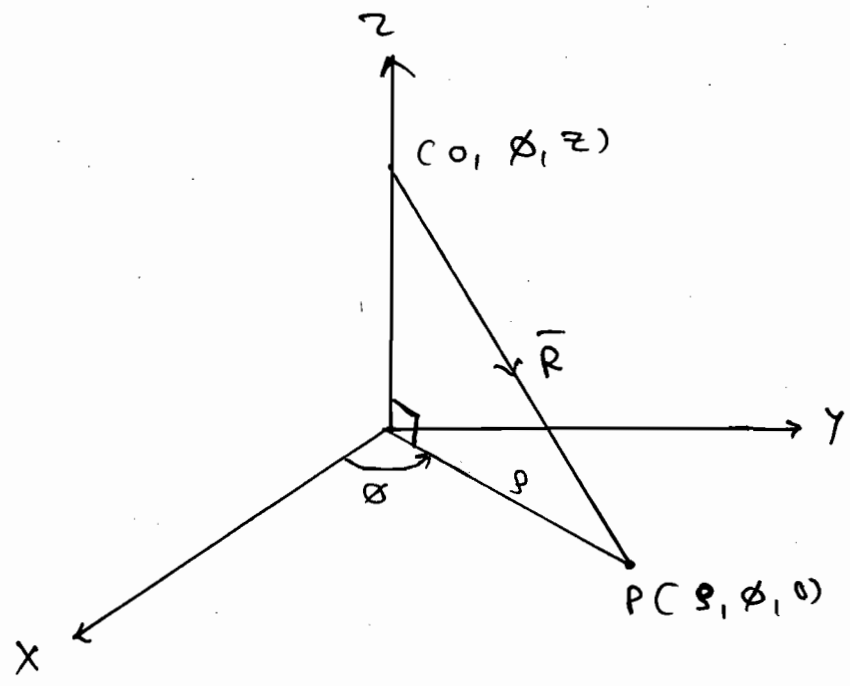
$$\vec{r} = (r-0) \hat{a}_r + (\phi-\phi) \hat{a}_\phi$$

$$\therefore \vec{r} = r \hat{a}_r$$

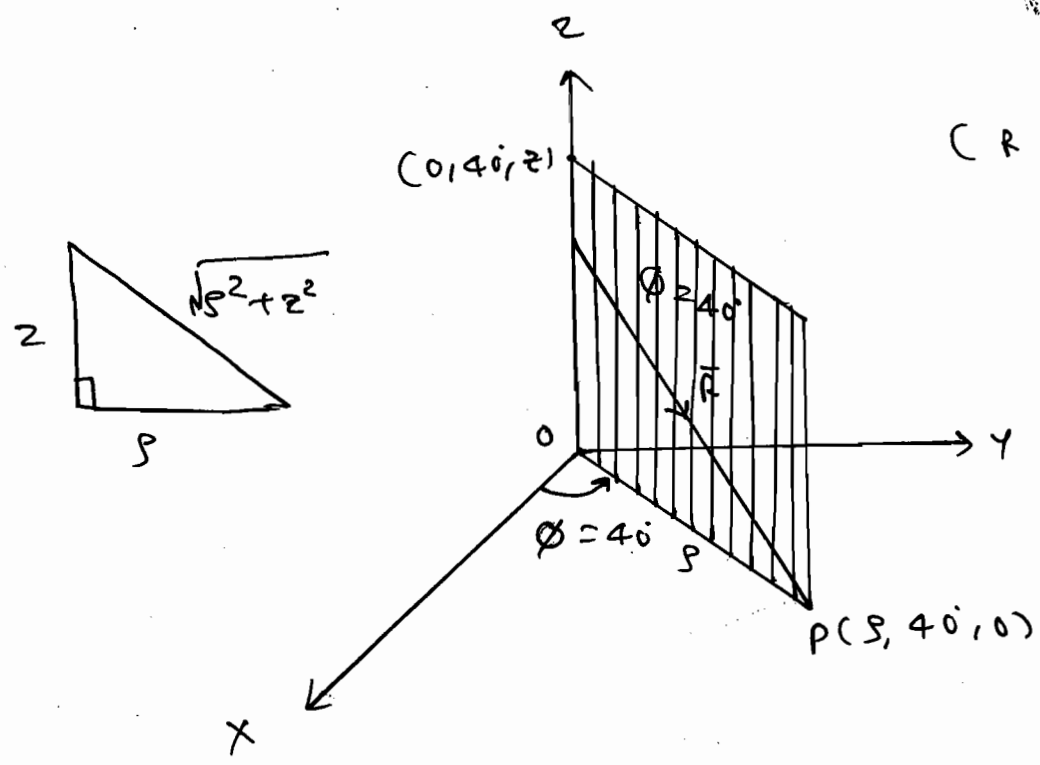
$$\therefore |\vec{r}| = r$$

$$\hat{a}_r = \frac{\vec{r}}{|\vec{r}|} = \hat{a}_r$$

\*



→ With ref. to  $P(\rho, \phi, 0)$  the point on the z-axis is co-ordinated as  $(0, \phi, z)$ .



(R lies on  $\phi = 40^\circ$ )

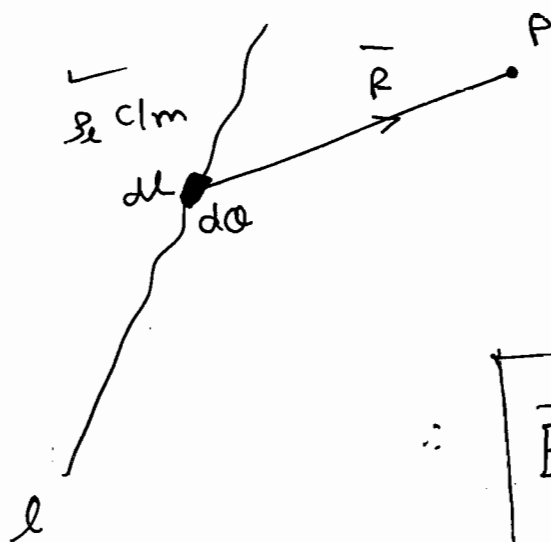
$$\vec{R} = \rho \hat{a}_3 - z \hat{a}_2$$

$$\therefore |\vec{R}| = \sqrt{\rho^2 + z^2}$$

→ The point on the z-axis also assumed to lying on  $\phi = 40^\circ$  plane.

∴ with ref to P (S,  $40^\circ$ , 0), the point on the z-axis is co-ordinated as (0,  $40^\circ$ , z).

Ex-1 Expression for  $\vec{E}$  due to a line with a charge density of  $S_e$  C/m.



$$d\vec{E} = \frac{dq}{4\pi\epsilon |\vec{R}|^2} \hat{C}_R$$

$$= \frac{S_e dl}{4\pi\epsilon |\vec{R}|^2} \times \hat{C}_R$$

$$\vec{E} = \int_l \frac{S_e dl}{4\pi\epsilon |\vec{R}|^2} \cdot \frac{\vec{R}}{|\vec{R}|} \text{ V/m.}$$

→  $dq = S_e dl$

→ We assume that 'dl' is so small such that it shrinks to the point. when we say it is a point, we consider that the 'dq' is located then it can have coordinates.

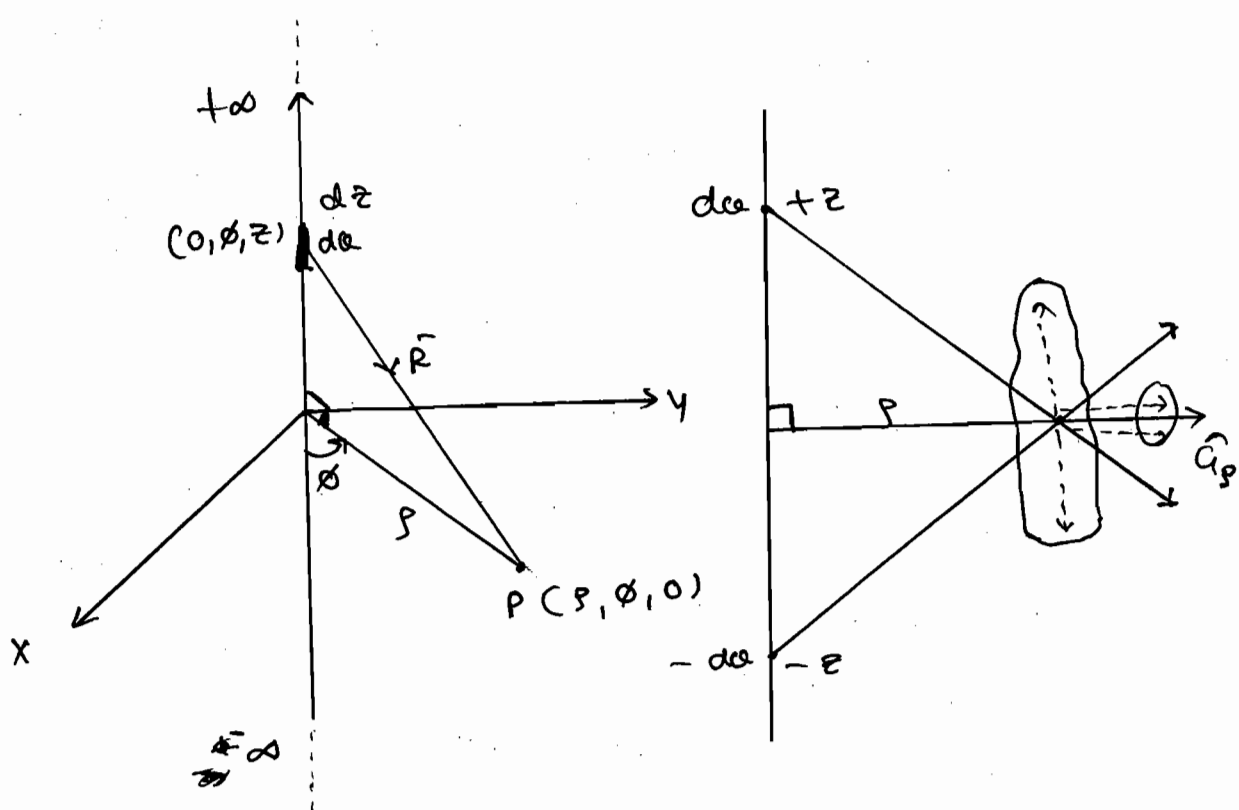
→ At this point, we consider that the 'dq' is located.



Ex-1 Find an expression for the electric field due to an infinite line with a uniform charge density of  $\lambda$  C/m and show that

- (i) Magnitude of the  $\vec{E}$  is inversely proportional to the distance bet<sup>n</sup> the infinite line and the observation ~~xxx~~ point.
- (ii) the direction of the  $\vec{E}$  could be projecting in a direction normal to the infinite line.

Ans: We assume that the infinite line lies along z-axis, extending from  $-\infty$  to  $+\infty$ . We find the electric field at some point on the x-y plane. for that convenience we further use cylindrical co-ordinates.



$$\rightarrow da = \rho_l dz$$

$dz \rightarrow$  Shown to point



At this point, we assume that 'da' is located.

$\therefore$  with ref.  $(\rho, \phi, 0)$ , the point on the z-axis is co-ordinated as  $(0, \phi, z)$ .

At this point da is located.

$$\vec{r} = \rho \hat{a}_\rho - z \hat{a}_z$$

$$\therefore d\vec{E} = \frac{\rho_l dz}{4\pi\epsilon_0 (\sqrt{\rho^2 + z^2})^2} \cdot \frac{\rho \hat{a}_\rho - z \hat{a}_z}{\sqrt{\rho^2 + z^2}}$$

NOTE: For every da at +z on the +ve z-axis there exist an another da on the -ve z-axis at -z.

$\rightarrow$  The charge configuration is symmetry about X-Y plane. which result in cancellation of  $\hat{a}_z$  components and the resultant field would be along  $\hat{a}_\rho$  direction only. i.e.

$\rightarrow$  In general, no field component exist along the ~~line~~ length of the line resulting  $\vec{E}$  exists normal to line ignoring  $\hat{a}_z$  component. The total

→ The total field given by.

$$\vec{E} = \frac{\rho_l \rho}{4\pi\epsilon_0} \hat{a}_\rho \int_{-\infty}^{\infty} \frac{dz}{(\rho^2 + z^2)^{3/2}}$$

$$z = \rho \tan \theta$$

$$dz = \rho \sec^2 \theta d\theta$$

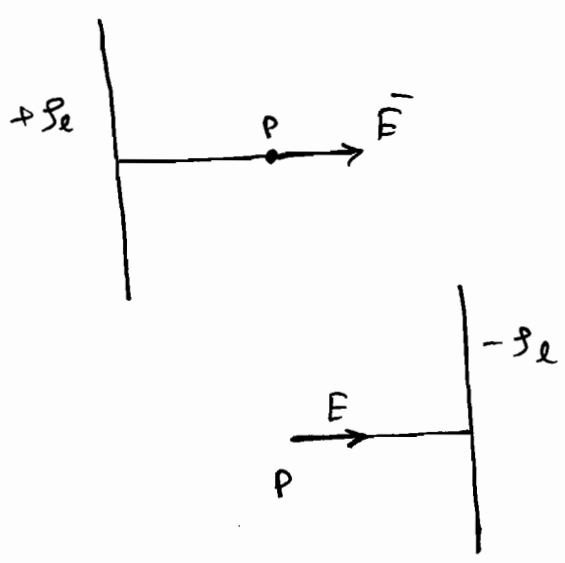
$$(\rho^2 + z^2)^{3/2} = \rho^3 \sec^3 \theta$$

$$\therefore \vec{E} = \frac{\rho_l}{2\pi\epsilon_0 \rho} \hat{a}_\rho$$

$$\therefore \boxed{\vec{E} = \frac{\rho_l}{2\pi\epsilon_0 \rho} \hat{a}_\rho} \Rightarrow \boxed{|\vec{E}| \propto \frac{1}{\rho}}$$

→ where, ' $\rho$ ' is the distance b/w the infinite line and the observation point.

⇒

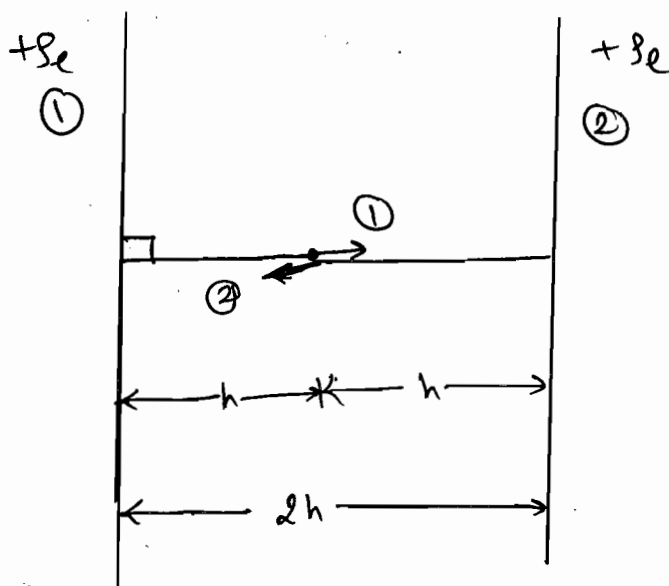


→ If  $\rho_l$  is +ve the direction of  $\vec{E}$  would be away from the infinite line.

→ If  $\rho_l$  is -ve the direction of the  $\vec{E}$  would be towards the infinite line.

Ex-1 Two infinite lines are parallel they are separated by  $2h$  m  $(h > 0)$ . They are distributed with uniform line charge density of  $+s_e$  C/m each. Find mag. of the electric field bet<sup>n</sup> this infinite line and also find direction of the electric field.

Ans:

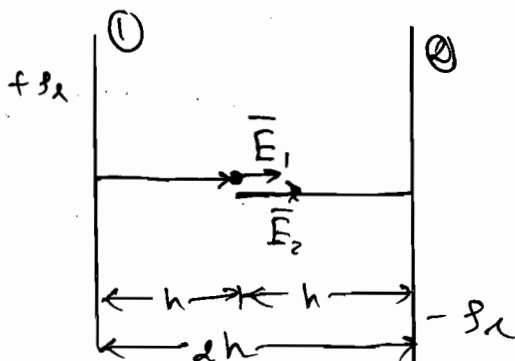


$$|\vec{E}| = 0$$

$\therefore$  No point in defining the direction of  $\vec{E}$ .

Ex-2 Repeat the above problem if they are distributed with  $+s_e$  C/m and  $-s_e$  C/m.

Ans:

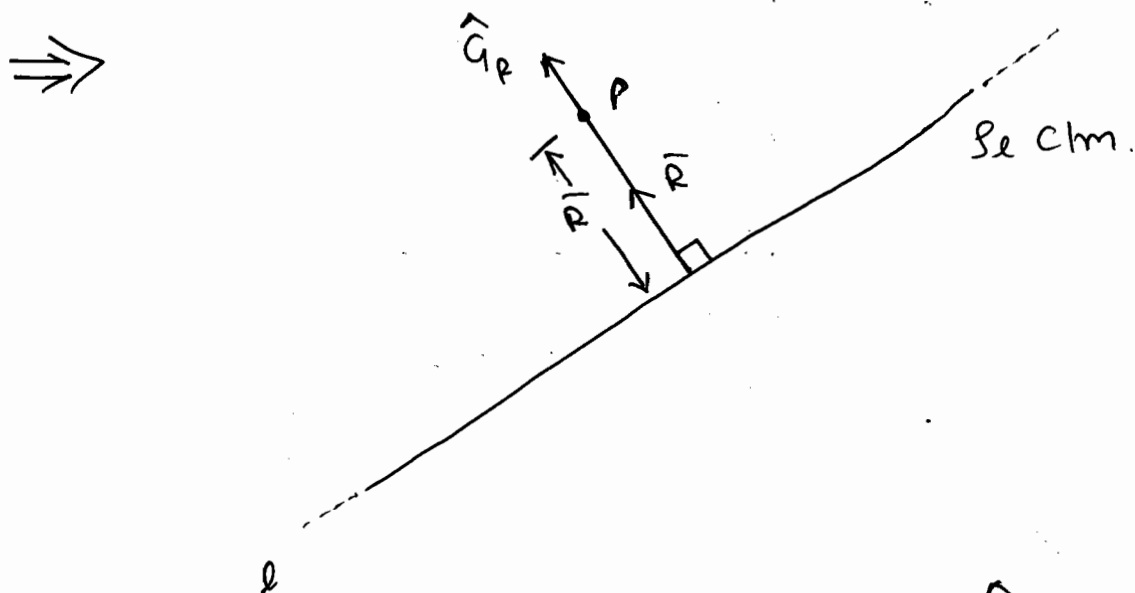


$$|\vec{E}| = \frac{\rho_l}{2\pi\epsilon h} + \frac{\rho_l}{2\pi\epsilon h}$$

$$|\vec{E}| = \frac{\rho_l}{\pi\epsilon h}$$

→ The direction of  $\vec{E}$  would be towards the line which is having  $-\rho_l$  clm.

(\*) Expression for  $\vec{E}$  due to an arbitrary oriented infinite line with a uniform charge density of  $\rho_l$  clm.

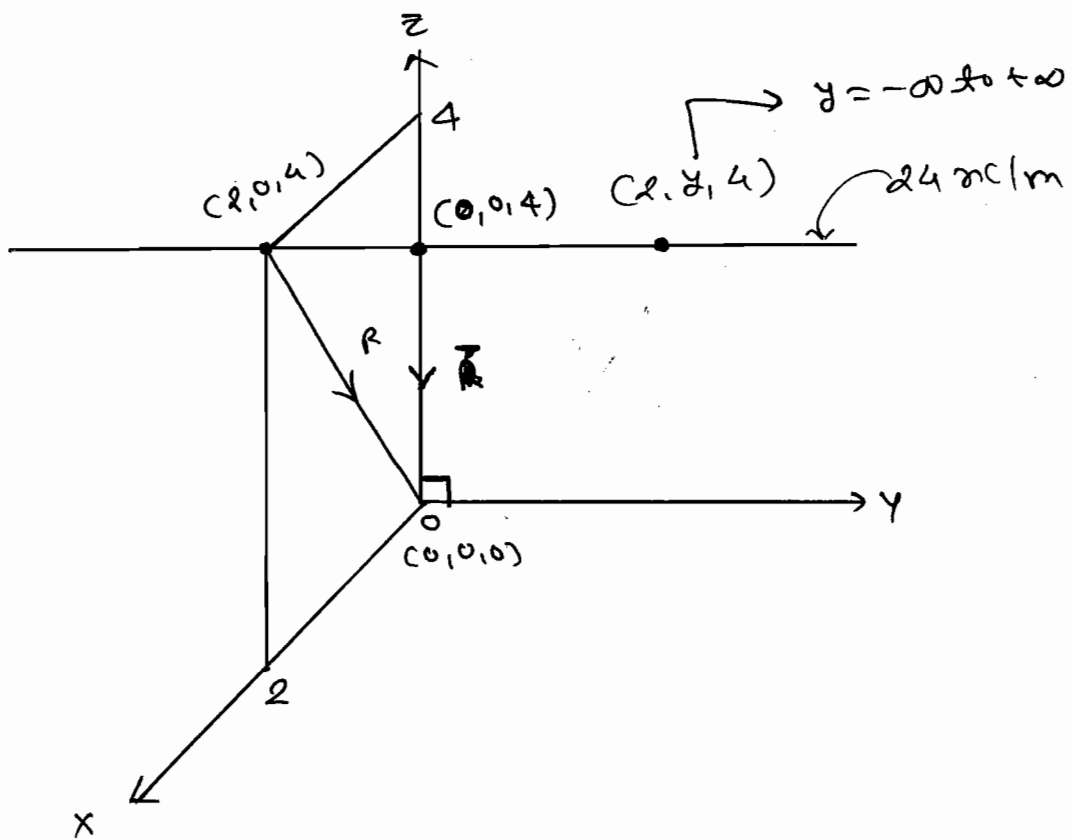


$$\vec{E} = \frac{\rho_l}{2\pi\epsilon |\vec{R}|} \cdot \hat{a}_r$$

$$\therefore \vec{E} = \frac{\rho_l}{2\pi\epsilon |\vec{R}|} \cdot \frac{\vec{R}}{|\vec{R}|} \text{ V/m.}$$

Ex-1 Find expression for the electric field at  
 (a) origin (b)  $(4, 5, 6)$  m (c)  $(10, 10, 10)$  m.  
 due to an infinite line with uniform  
 charge density of  $24 \text{ nC/m}$ . which lies  
 at  $x=2, z=4$  m.

Ans.



① at origin

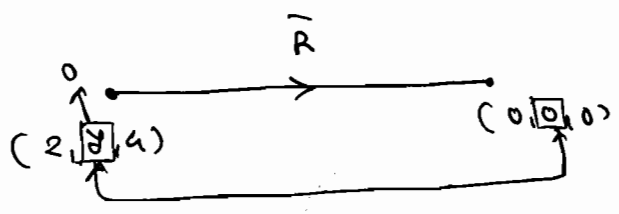
$$\therefore \vec{R} = -2\hat{a}_x - 4\hat{a}_z$$

$$\therefore \vec{E} = \frac{24 \times 10^{-9}}{9 \times 10^9 \times \sqrt{20}} \times \frac{-2\hat{a}_x - 4\hat{a}_z}{\sqrt{20}}$$

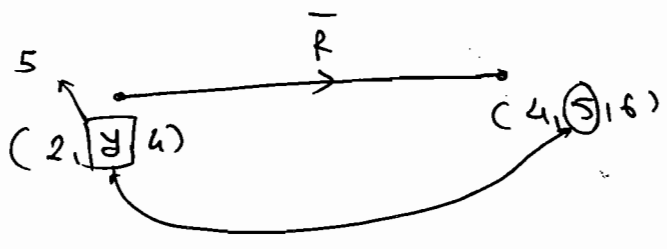
$$= \frac{216 \times 2}{20} (\hat{a}_x + 2\hat{a}_z)$$

$$\therefore \boxed{\vec{E} = -43.2 (\hat{a}_x + 2\hat{a}_z) \text{ V/m}}$$

Short cut:



2)



$$\vec{R} = 2\hat{a}_x + 2\hat{a}_z$$

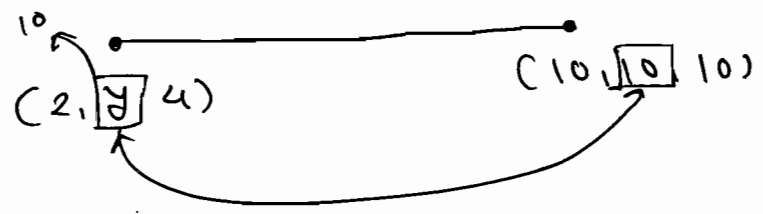
$$\therefore \vec{E} = \frac{q_e}{4\pi\epsilon |\vec{R}|} \times \frac{\vec{R}}{|\vec{R}|}$$

$$= \frac{3 \times 10^{-9}}{4\pi \times 10^{-9} \times \sqrt{8}} \times \frac{2\hat{a}_x + 2\hat{a}_z}{\sqrt{8}}$$

$$E = 54 (2\hat{a}_x + 2\hat{a}_z)$$

$$\therefore \vec{E} = 108 (\hat{a}_x + \hat{a}_z) \text{ v/m}$$

3)

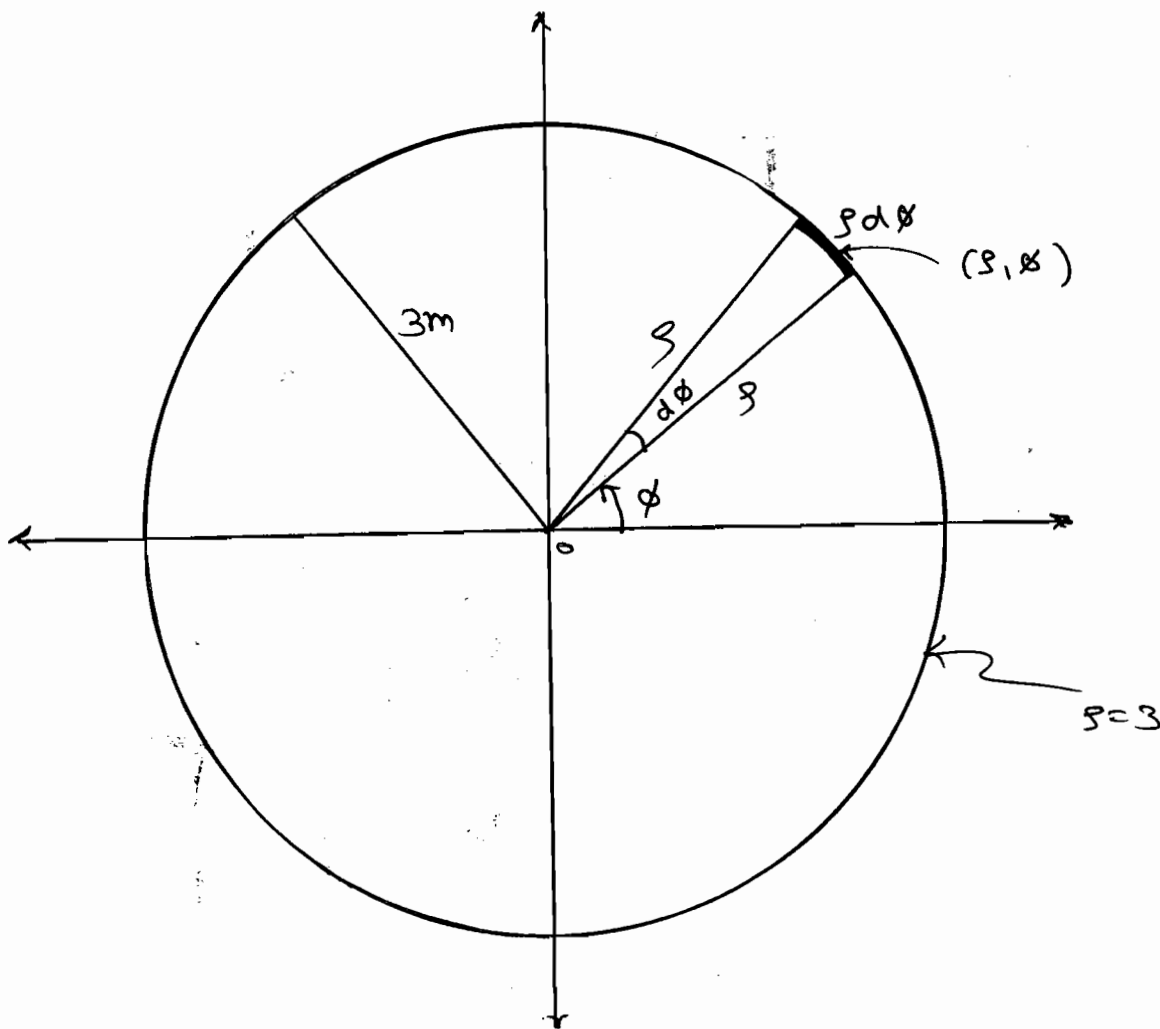


$$\vec{R} = 8\hat{a}_x + 6\hat{a}_z$$

$$\therefore \vec{E} = \frac{24 \times 10^{-9}}{4\pi \times 10^{-9} \times 10} \times \frac{8\hat{a}_x + 6\hat{a}_z}{10}$$

$$\therefore \vec{E} = 4.32 (8\hat{a}_x + 6\hat{a}_z) \text{ v/m}$$

\*



→  $s=3, 0 \leq \phi < 2\pi, z=0$

⇒ This represents, there exists a circle of radius 3m centered at origin and is located in  $z=0$  plane.

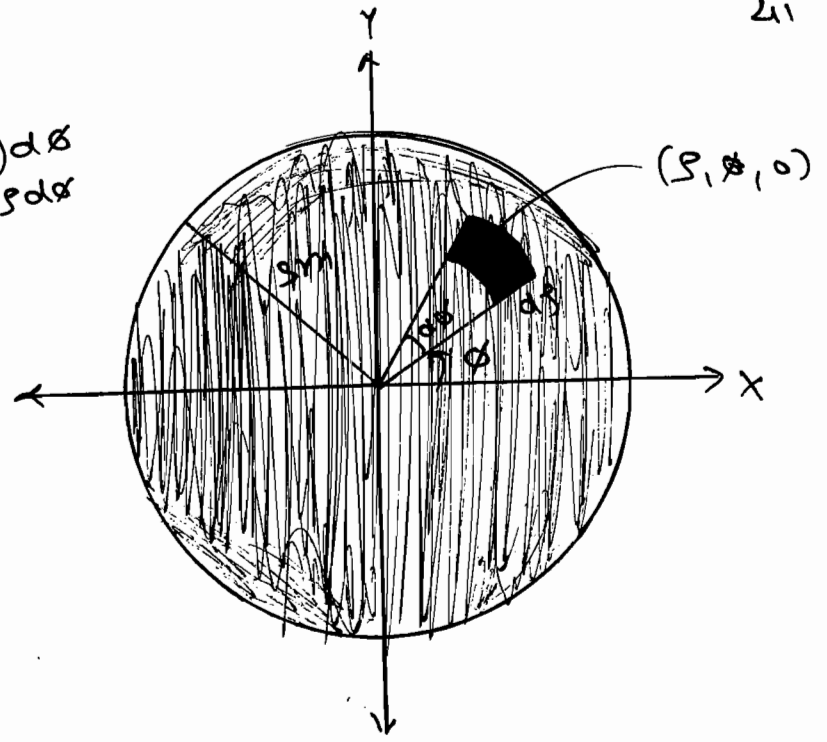
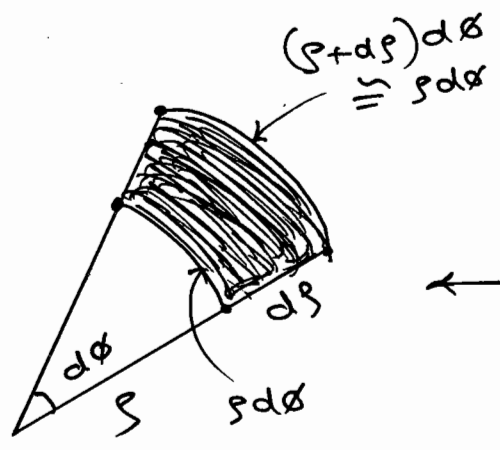
$dl = s d\phi$

$l = \int_{(z=0, s=3)}^{2\pi} s d\phi = 3 \int_0^{2\pi} d\phi = 6\pi m$

$dl \rightarrow$  so small such that it is shrinking to a point (i.e)  $d\phi \rightarrow 0$ .  
Then, that point is considered as  $(s, \phi)$ .



→ \*



→  $\circ 0 \leq \rho \leq 3, 0 \leq \phi \leq 2\pi, z=0$   
 $\circ \bullet 0 \leq \rho \leq 3, 0 \leq \phi \leq 2\pi, z=0$   
 $\circ \rho \leq 3, z=0$

This represents a circular disk of radius  $3m$ , centered at origin and is located in  $z=0$  plane.

$$ds = \rho d\rho d\phi$$

$$S = \int_0^3 \int_0^{2\pi} \rho d\rho d\phi$$

$$= \int_0^3 \rho [\phi]_0^{2\pi} d\rho$$

$$= \int_0^3 (2\pi) \rho d\rho$$

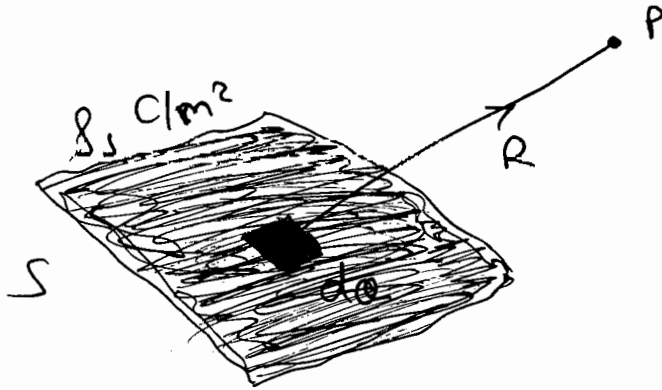
$$= \left[ \frac{\rho^2}{2} \right]_0^3 \times 2\pi$$

$\therefore S = 9\pi m^2$

$ds \rightarrow \rho$  small such that it shrinks to a point (i.e)  $d\rho \rightarrow 0, d\phi \rightarrow 0$ .  
 $\therefore$  That point is coordinated as  $(\rho, \phi)$  or  $(\rho, \phi, 0)$ .

\* Electric field ( $\vec{E}$ ) due to a sheet with a uniform charge density of  $\rho_s$  C/m<sup>2</sup>.

⇒



→  $da = \rho_s ds$

$ds \rightarrow$  shrunk to a point.

At this point, we consider that 'da' is located. When we say, it is a point, then it can have co-ordinates.

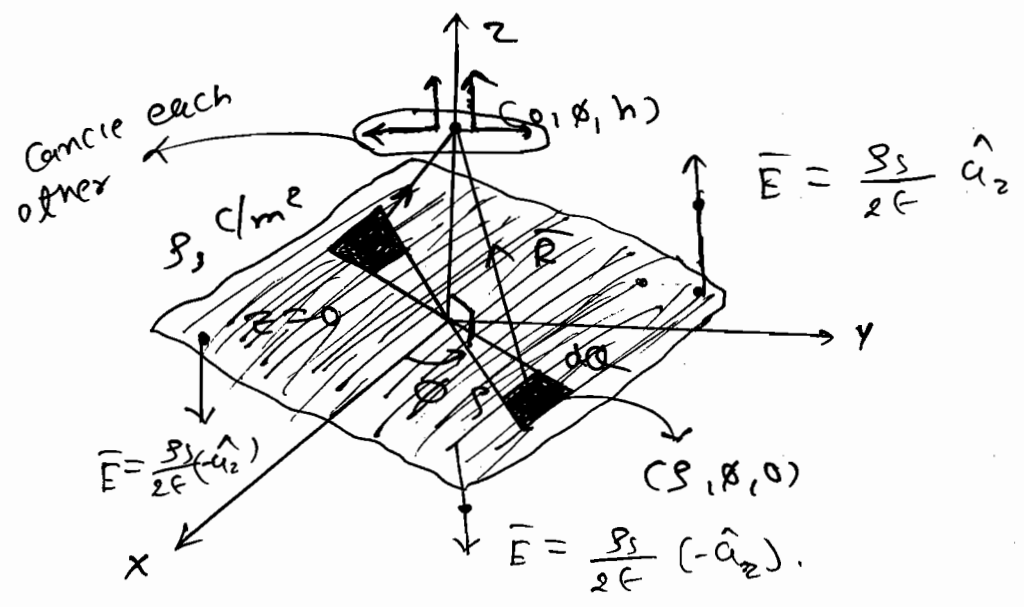
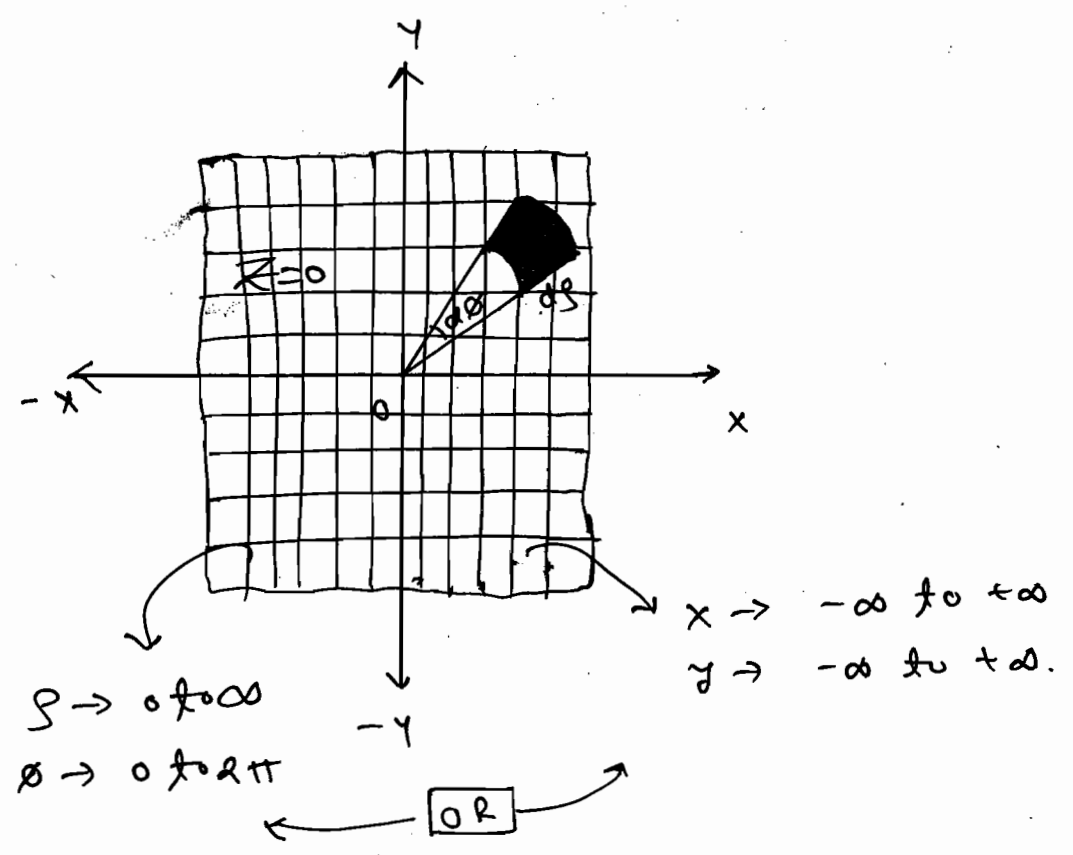
$$d\vec{E} = \frac{da}{4\pi\epsilon |\vec{R}|^2} \hat{q}_R$$

$$\therefore \vec{E} = \int_S \frac{\rho_s ds}{4\pi\epsilon |\vec{R}|^2} \times \frac{\vec{R}}{|\vec{R}|} \text{ V/m}$$

double integral.

Ex-1 Find an expression for the  $\vec{E}$  due to an infinite sheet with the uniform charge density of  $\rho_s \text{ C/m}^2$ .

Ans:  $\rightarrow$  We assume that the infinite sheet is located in the  $z=0$  plane. We find the  $\vec{E}$  at some point on the  $z$ -axis. For the convenience we use cylindrical coordinates.



$$\rightarrow ds = r dr d\theta.$$

$$d\alpha = r_s ds$$

$$d\alpha = r_s r dr d\theta$$

$ds \rightarrow$  shrinks to a point



This point is coordinated as  $(r, \theta, 0)$

[i.e.  $dr \rightarrow 0, d\theta \rightarrow 0$ ].

At this point 'd $\alpha$ ' is located,

$$d\vec{E} = \frac{r_s \cdot r dr d\theta}{4\pi\epsilon (\sqrt{r^2 + h^2})^2} \times \frac{-r\hat{q}_r + h\hat{q}_z}{\sqrt{r^2 + h^2}}$$

→ As shown in figure for every  $d\alpha$  on the sheet there exists an another  $d\alpha$  diametrically opposite side. Therefore, the charge configuration is symmetry about z-axis. which results in cancellation of horizontal field components. And the resultant  $\vec{E}$  would be along  $\hat{q}_z$  direction only. i.e. No field component exists  $\parallel$  to the infinite sheet.

→ The resultant field exists in the direction to the normal to the sheet. Here, ignoring  $\hat{q}_r$  components. The total field is given by,

→ Ignoring  $\hat{a}_3$  component,

the total field is given by,

$$\vec{E} = \frac{S_s h}{4\pi\epsilon} \hat{a}_2 \int_0^\infty \int_0^{2\pi} \frac{s ds d\phi}{(s^2+h^2)^{3/2}}$$

$$\int_0^{2\pi} d\phi = 2\pi$$

$$\int_0^\infty \frac{s ds}{(s^2+h^2)^{3/2}} = \frac{1}{h}$$

put  $s^2+h^2 = t$ .

$\therefore 2s ds = dt$

$\therefore s ds = \frac{1}{2} dt$

$$\vec{E} = \frac{S_s}{2\epsilon} \hat{a}_2 \text{ V/m}$$

→ In general

$$\vec{E} = \frac{S_s}{2\epsilon} \hat{a}_n \text{ V/m}$$

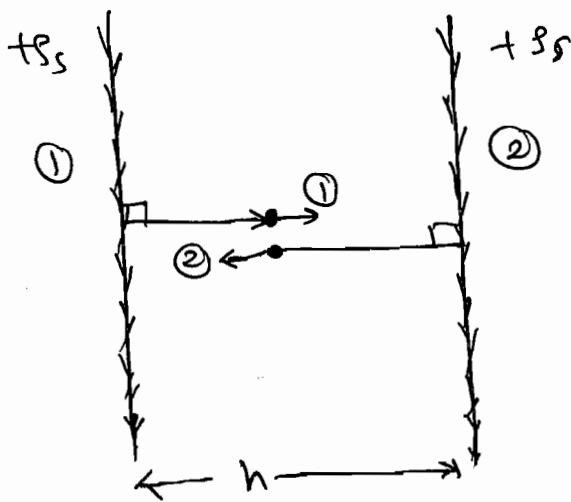
where,  $\hat{a}_n$  is the normal unit vector at the observation point with ref. to infinite sheet.

→ If  $S_s$  is +ve, the direction of  $\vec{E}$  would be away from the infinite sheet.

→ If  $S_s$  is -ve, the direction of  $\vec{E}$  would be towards to the infinite sheet.

Ex-1 Two infinite sheets are  $11^{\text{th}}$ , they are separated by  $2h$  m. they are distributed with uniform charge density of  $\sigma_s$   $\text{C/m}^2$ .  
 Each find the electric field at any point bet<sup>n</sup> this two infinite sheet.

Ans:

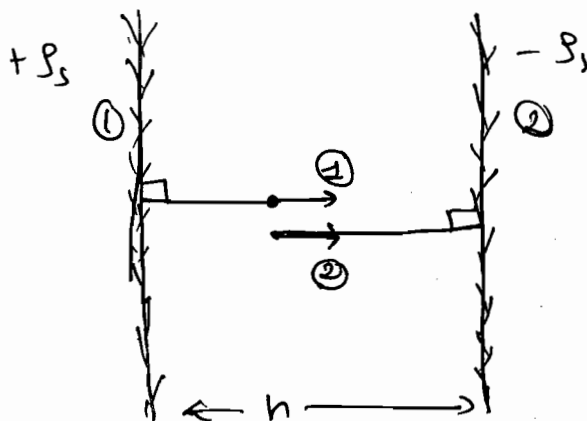


$$|\vec{E}| = 0.$$

The fields add in out of phase.

Ex-2 Repeat the above example If they are distributed with uniform charge density of  $+\sigma_s$   $\text{C/m}^2$  and  $-\sigma_s$   $\text{C/m}^2$ . The

Ans:

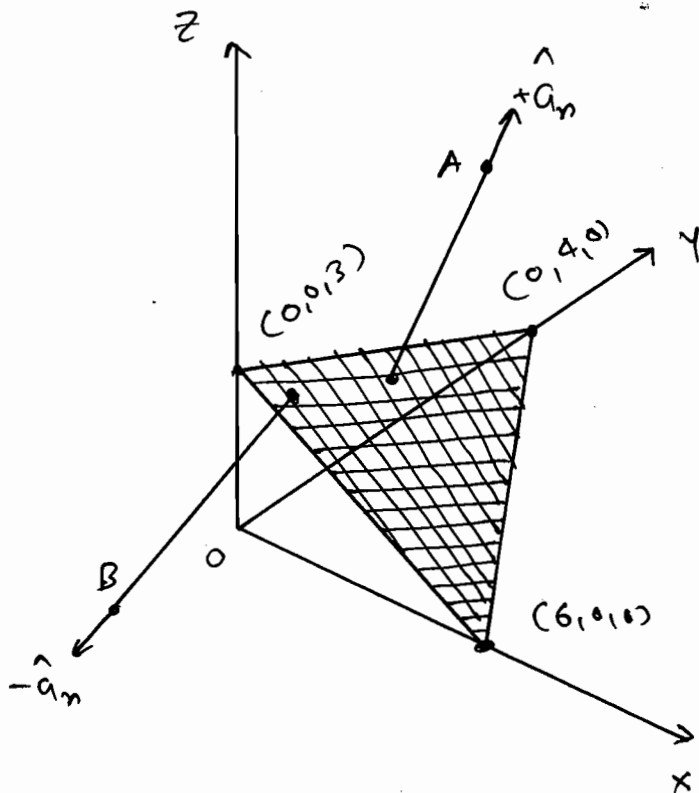


$$|\vec{E}| = \frac{\rho_s}{2\epsilon} + \frac{\rho_s}{2\epsilon} = \frac{\rho_s}{\epsilon}$$

→ The fields add in in-phase.  
 The direction of  $\vec{E}$  would be towards  
the sheet which is having  $-\rho_s \text{ C/m}^2$ .

Ex-3 An Infinite Sheet with a uniform charge density of  $24 \text{ nC/m}^2$  is lies in a plane define by  $2x + 3y + 4z = 12$ .  
 find the  $\vec{E}$  in all the regions.

Ans:



$$\rightarrow E \text{ (at A)} = \frac{\rho_s}{2\epsilon} \hat{a}_n$$

$$E \text{ (at B)} = \frac{\rho_s}{2\epsilon} (-\hat{a}_n)$$

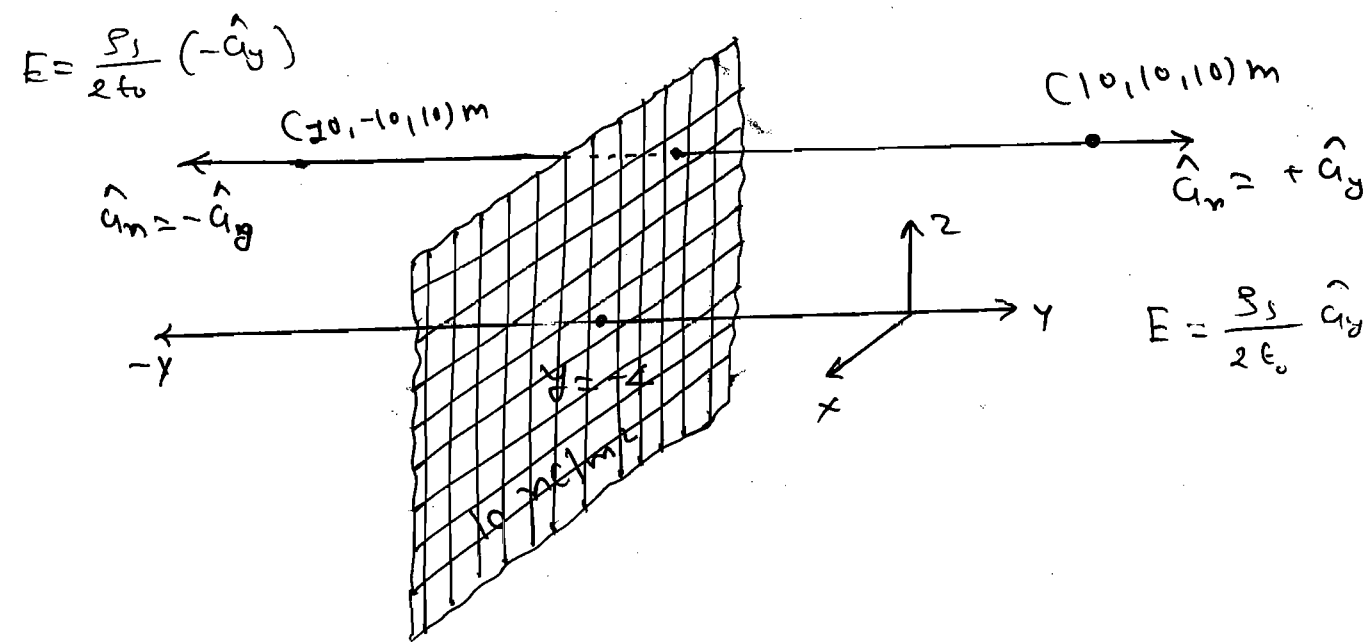
$$\hat{a}_n = \frac{2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z}{\sqrt{2^2 + 3^2 + 4^2}}$$

Ex-4 An Infinite sheet with a uniform charge density of  $10 \text{ nC/m}^2$  is lies at  $y = -4 \text{ m}$ .  
 Find the  $\vec{E}$  at

(i)  $(10, 10, 10) \text{ m}$

(ii)  $(10, -10, 10) \text{ m}$ .

Ans:  
 The infinite sheet is parallel to  $z$ - $x$  plane.



(i) at  $(10, 10, 10) \text{ m}$

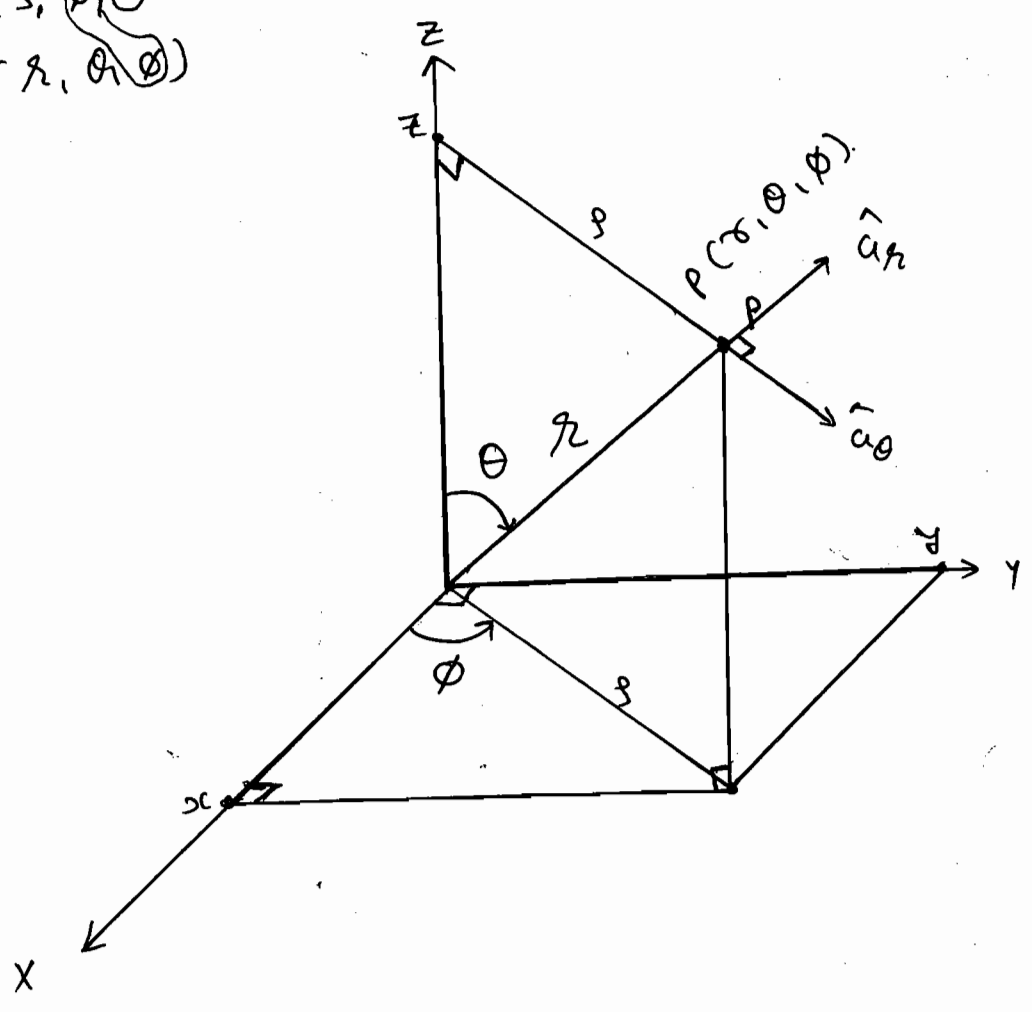
$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_y \text{ V/m}$$

(ii) at  $(10, -10, 10)$

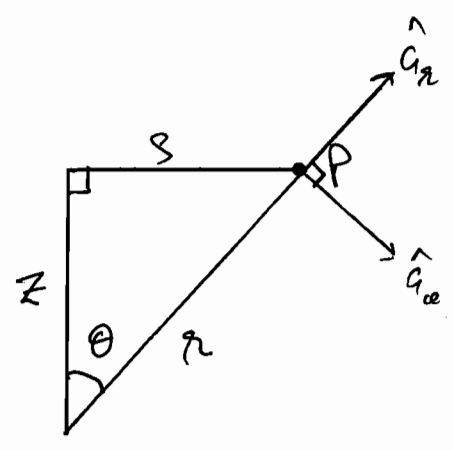
$$\vec{E} = \frac{\rho_s}{2\epsilon_0} (-\hat{a}_y) \text{ V/m}$$



\*  
 $P(x, y, z)$   
 $P(\rho, \theta, \phi)$   
 $P(r, \theta, \phi)$



$\Rightarrow \rho = r \sin \theta$   
 $z = r \cos \theta$   
 $x = \rho \cos \phi$   
 $\therefore x = r \sin \theta \cdot \cos \phi$   
 $\therefore y = \rho \sin \phi$   
 $\therefore y = r \sin \theta \cdot \sin \phi$



$r = \sqrt{x^2 + y^2 + z^2} \quad 0 \leq r < \infty$   
 $\theta = \cos^{-1} \left( \frac{z}{r} \right) \quad 0 \leq \theta \leq \pi$   
 $\phi = \tan^{-1} \left( \frac{y}{x} \right) \quad 0 \leq \phi \leq 2\pi$

→ Locus of  $r = \text{constant}$  represents a sphere (or) a spheroidal whose centre coincides with the origin. Therefore,  $r$  assume all possible values ranging from 0 to  $\infty$ .

→  $\hat{a}_r$  is a unit vector projecting normal to  $r = \text{constant}$  (or) normal to the sphere.

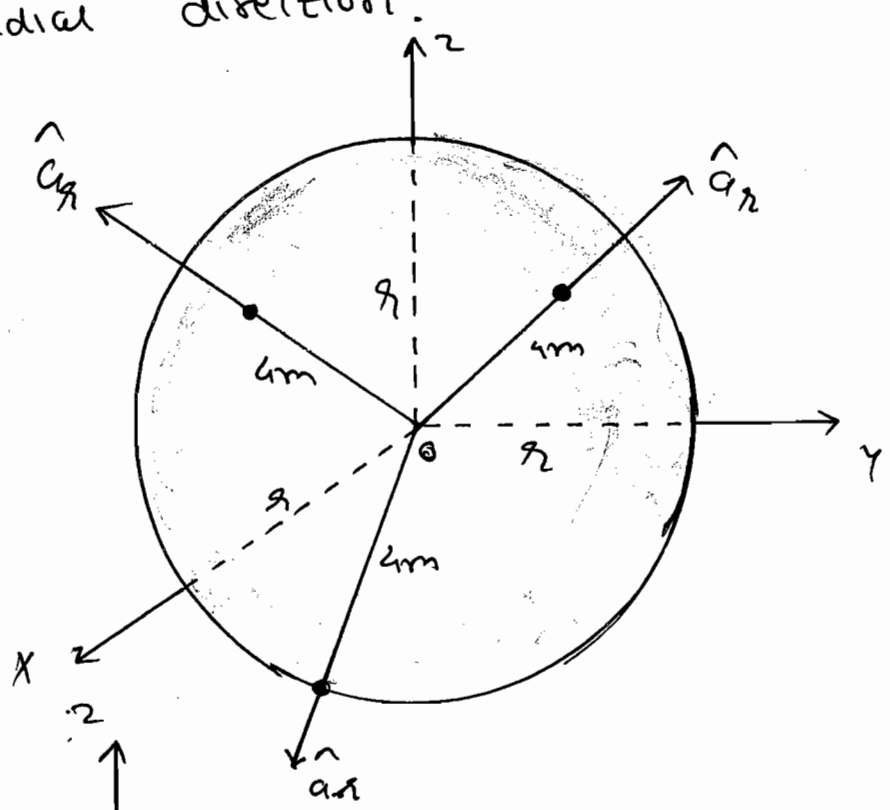
also called radial direction.

→

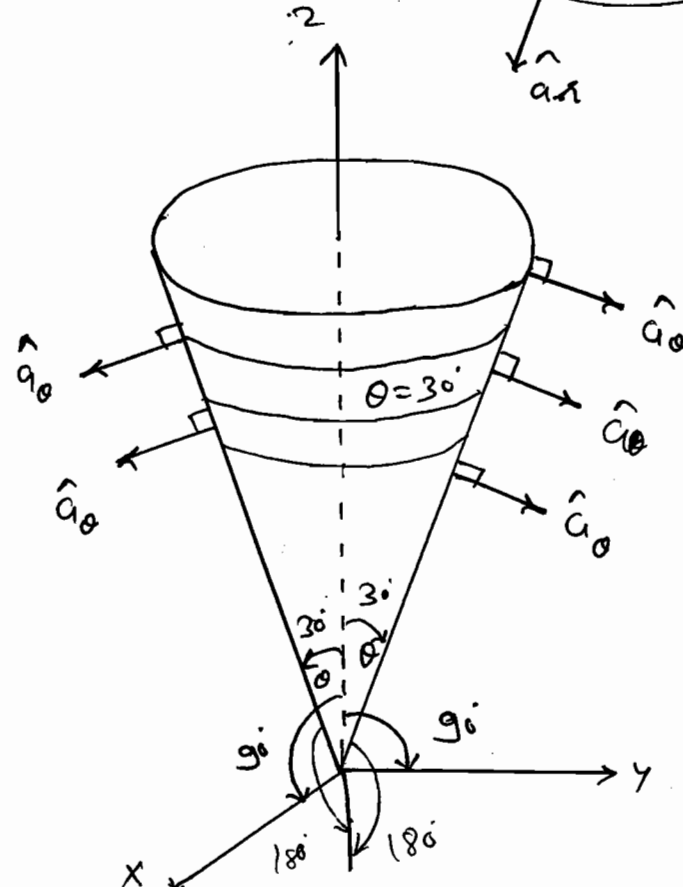
on  $r = \text{const.}$

$\theta \rightarrow 0 \text{ to } \pi$

$\phi \rightarrow 0 \text{ to } 2\pi$



→  $\theta = \text{const.}$



on  $\theta = \text{const.}$

$r \rightarrow 0 \text{ to } \infty$

$\phi \rightarrow 0 \text{ to } 2\pi$

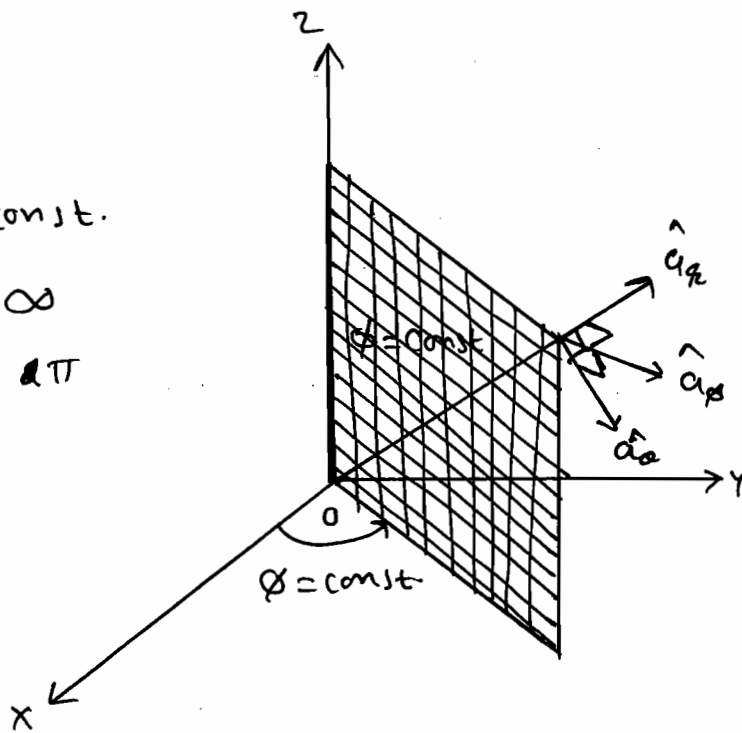
51  
 $\rightarrow \theta = \text{constant}$  for  $0 < \theta < 90^\circ$  represents a  
 Conical plane,  $\theta = 90^\circ$  represents  
 x-y plane,  $\theta = 90^\circ$  is called azimuthal  
 plane.

$\rightarrow$  As shown in the figure  $\theta$  assumes all  
 possible values ranging from  $0$  to  $\pi$ .

$\rightarrow \hat{a}_\theta$  is a unit vector projecting normal  
 to  $\theta = \text{constant}$  plane. Further,  $\hat{a}_r, \hat{a}_\theta, \hat{a}_\phi$   
 orthogonal to each other.

$\rightarrow$

on  $\phi = \text{const.}$   
 $r \rightarrow 0 \text{ to } \infty$   
 $\theta \rightarrow 0 \text{ to } \pi$

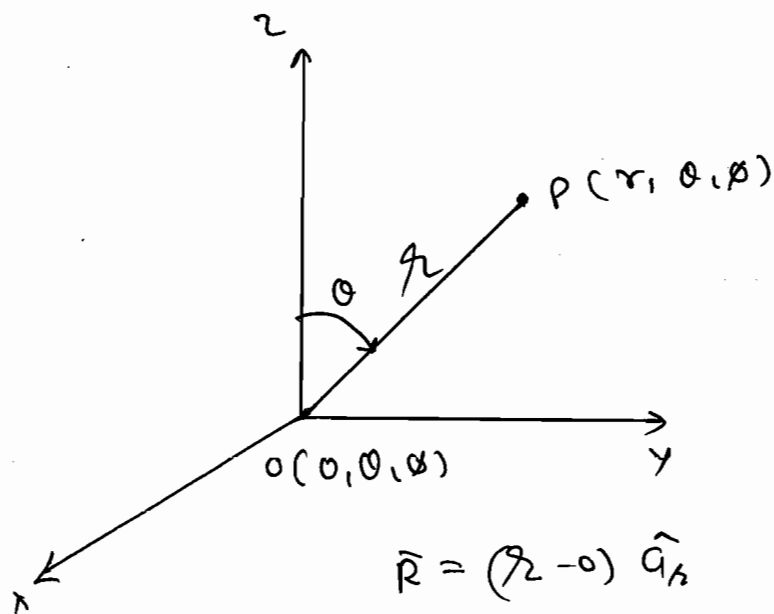


$\rightarrow \phi$  assumes all possible values ranging from  
 $0$  to  $2\pi$ .  $\hat{a}_\phi$  is a unit vector projecting  
 normal to  $\phi = \text{const.}$  plane. further we write  
 $\hat{a}_r, \hat{a}_\theta$  and  $\hat{a}_\phi$  are orthogonal to each other.

→  $\phi = \text{const.}$  plane is also called Elevation plane.

Q- With ref. to  $P(r, \theta, \phi)$  what are the co-ordinates of the origin?

A) =  $O(0, 0, 0)$ .



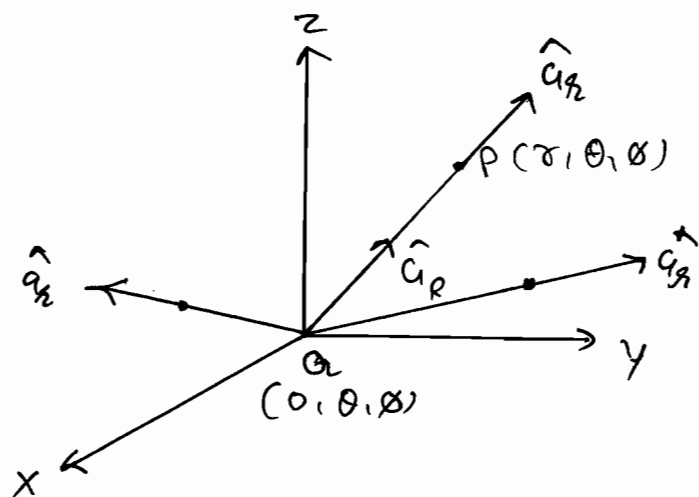
$$\vec{R} = (r - 0) \hat{a}_r$$

$$\therefore \vec{R} = r \hat{a}_r$$

$$\Rightarrow \hat{a}_R = \hat{a}_r$$

Q-1 A point charge of  $Q$  coulombs is located at the origin. Find  $\vec{E}$  at a distant point  $P$  in spherical co-ordinates.

Ans:



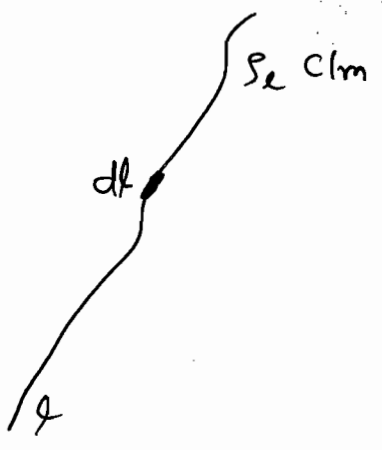
$$\vec{E} = \frac{Q}{4\pi\epsilon_0 R^2} \hat{a}_R$$

$$= \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

→ Thus, the direction of  $\vec{E}$  would be along radial (or)  $\hat{a}_r$  direction.

\* Total Charge Calculation:

(1) Line Charge:



$da = \sigma_l dl.$

$Q = \int \sigma_l dl.$

single I

(2) Surface Charge:

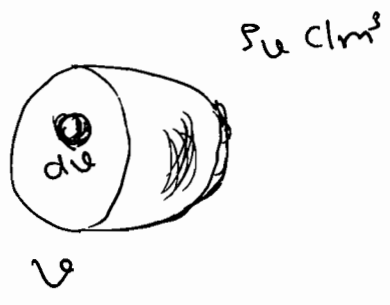


$da = \sigma_s dS$

$Q = \int \sigma_s dS.$

double I

(3) Volume Charge:

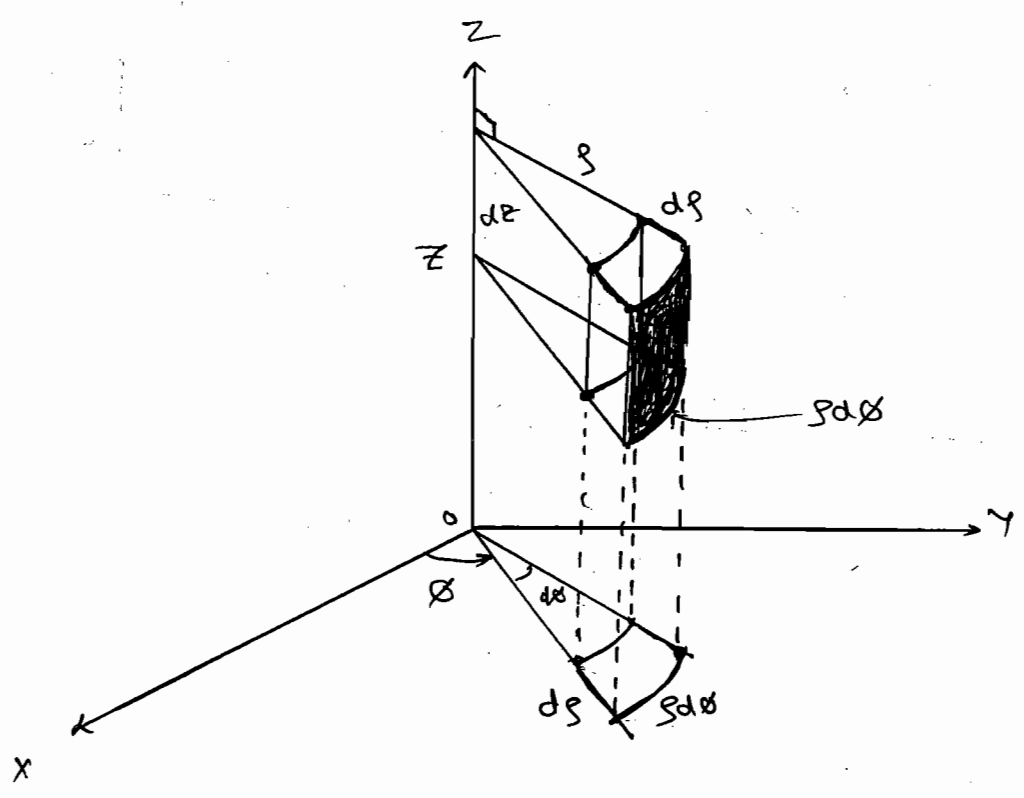
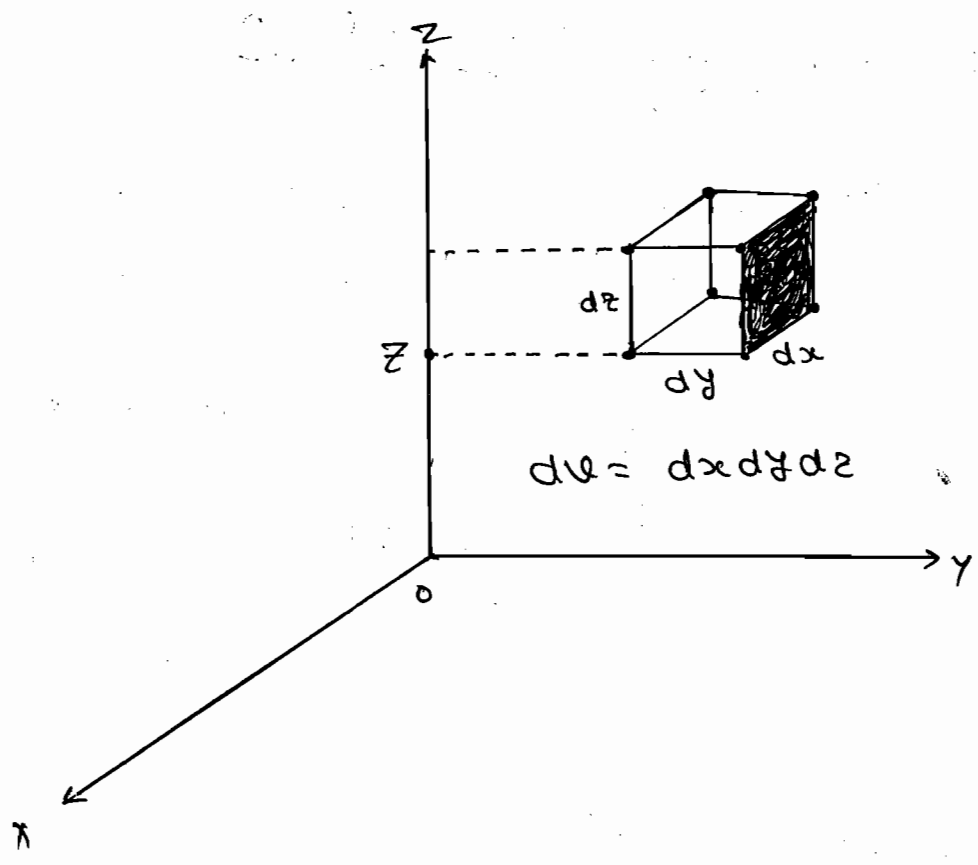


$da = \sigma_v dv$

$Q = \int \sigma_v dv.$

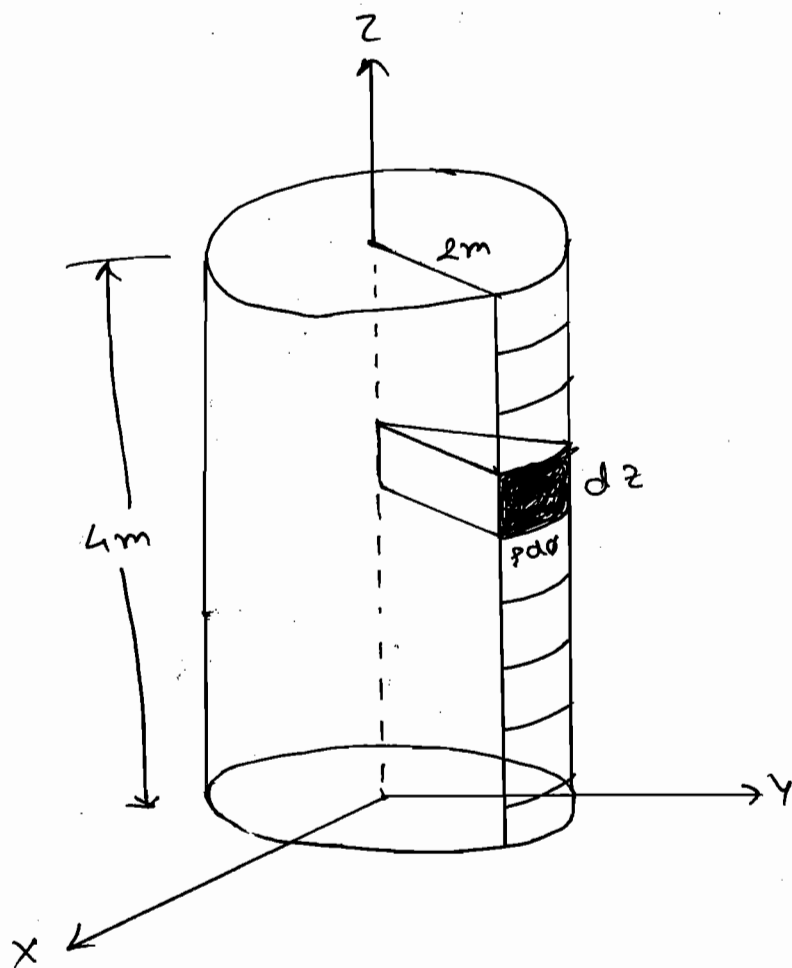
Triple I

\* Construction of  $dV$ .



$$dV = ds \cdot s \cdot d\phi dz$$

$$dV = s ds d\phi dz$$



→  $S = 2m, 0 \leq \phi \leq 2\pi, 0 \leq z \leq 4$

→ This represents a cylindrical sheet with radius 2m and height 4m.

$$dS = \rho d\phi dz$$

$$\therefore S = \int_0^{2\pi} \int_0^4 \rho d\phi dz$$

$$\therefore S = 2 (\phi)_0^{2\pi} (z)_0^4$$

$$\therefore S = 2(2\pi)(4)m$$

$$S = 16\pi \text{ m}^2$$

Ex-1 Find the total charge with in each of the volume indicate below:

①  $\rho_v = 10z^2 e^{-0.1x} \sin \pi y \text{ nC/m}^3$

$0 \leq x \leq 1, 1 \leq y \leq 2, 2.5 \leq z \leq 4.5.$

②  $\rho_v = 2xyz^2 \text{ nC/m}^3.$

$0 \leq \rho \leq 2, 0 \leq \theta \leq \frac{\pi}{2}, 0 \leq z \leq 1.$

③  $\rho_v = 10 e^{-10y} \cdot e^{-z} \text{ nC/m}^3$ ; 1<sup>st</sup> octant.

Ans:  $dv = dx dy dz.$

$dQ = \rho_v dv$

$\therefore$

$\therefore dQ = \rho_v dz$

①  $Q = \int_{x=0}^1 \int_{y=1}^2 \int_{z=2.5}^{4.5} 10z^2 \cdot e^{-0.1x} \sin \pi y \cdot dx dy dz$

$\therefore Q = 10 \times \left[ \frac{e^{-0.1x}}{-0.1} \right]_0^1 \times \left[ -\frac{\cos \pi y}{\pi} \right]_1^2 \times \left[ \frac{z^3}{3} \right]_{2.5}^{4.5}$

$\therefore Q = 10 \times \left[ \frac{e^{-0.1} - 1}{-0.1} \right] \times \left[ +\frac{1+1}{\pi} \right] \times \left[ \frac{(4.5)^3 - (2.5)^3}{3} \right]$

$\therefore Q = \underline{\hspace{2cm}}$

②  $x = \rho \cos \theta, y = \rho \sin \theta$

$\therefore \rho_v = \rho^2 \sin \theta \cdot z^2 \text{ nC/m}^3.$



$\therefore dQ = \rho ds d\phi dz.$

$\therefore Q = \int_V \rho_u dV.$

$\therefore Q = \int_{s=0}^2 \int_{\phi=0}^{\pi/2} \int_{z=0}^1 \rho \cdot s^2 \cdot \sin 2\phi \cdot z^2 \cdot ds d\phi dz$

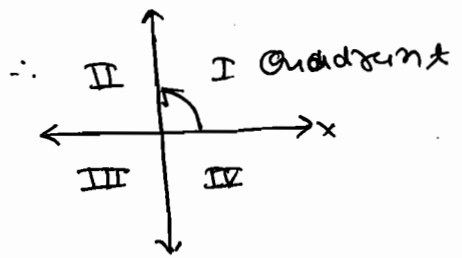
$\therefore Q = \left[ \frac{s^3}{3} \right]_0^2 \times \left[ \frac{-\cos 2\phi}{2} \right]_0^{\pi/2} \times \left[ \frac{z^3}{3} \right]_0^1$

$= \left[ \frac{8}{3} \right] \times \left[ \frac{2+1}{2} \right] \times \left[ \frac{1}{3} \right].$

$\therefore Q = \frac{14}{3} \pi C$

③  $\rho_u = 10e^{-10s} \cdot e^{-z} \text{ nC/m}^3.$

~~act~~ actual.



I - Octant: x, y are +ve

I - Octant  $\rightarrow x, y, z$  are +ve

$\Downarrow$   
 $\left. \begin{matrix} x \rightarrow 0 \text{ to } \infty \\ y \rightarrow 0 \text{ to } \infty \\ z \rightarrow 0 \text{ to } \infty \end{matrix} \right\} \Leftrightarrow \left\{ \begin{matrix} s \rightarrow 0 \text{ to } \infty \\ \phi \rightarrow 0 \text{ to } \pi/2 \\ z \rightarrow 0 \text{ to } \infty. \end{matrix} \right.$

i.e.  $\left. \begin{matrix} 0 \leq x \leq \infty \\ 0 \leq y \leq \infty \end{matrix} \right\} \Leftrightarrow \left\{ \begin{matrix} s \rightarrow 0 \text{ to } \infty \\ \phi \rightarrow 0 \text{ to } \pi/2 \end{matrix} \right.$

$dQ = \rho ds d\phi dz.$

$\therefore Q = 10 \int_0^{\infty} \int_0^{\pi/2} \int_0^{\infty} e^{-10s} \cdot e^{-z} \cdot s ds d\phi dz.$

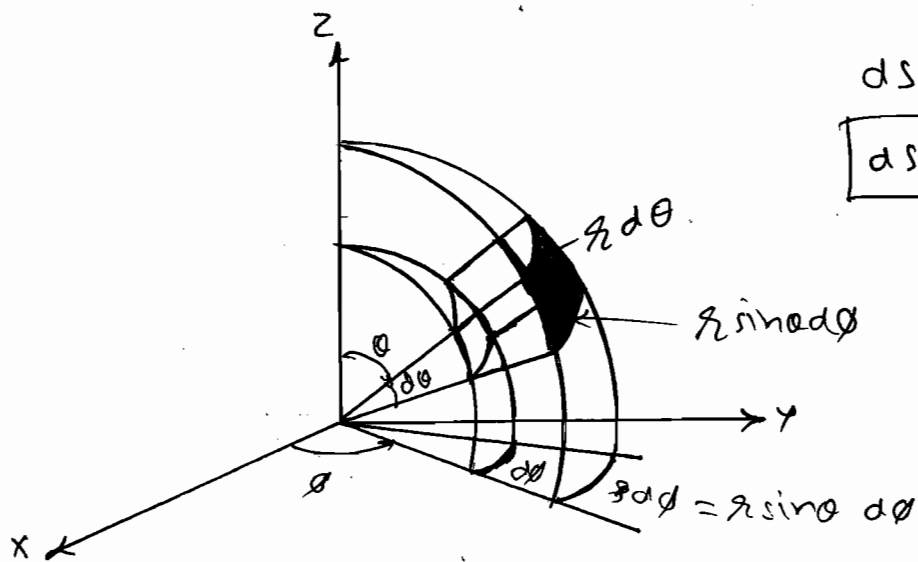
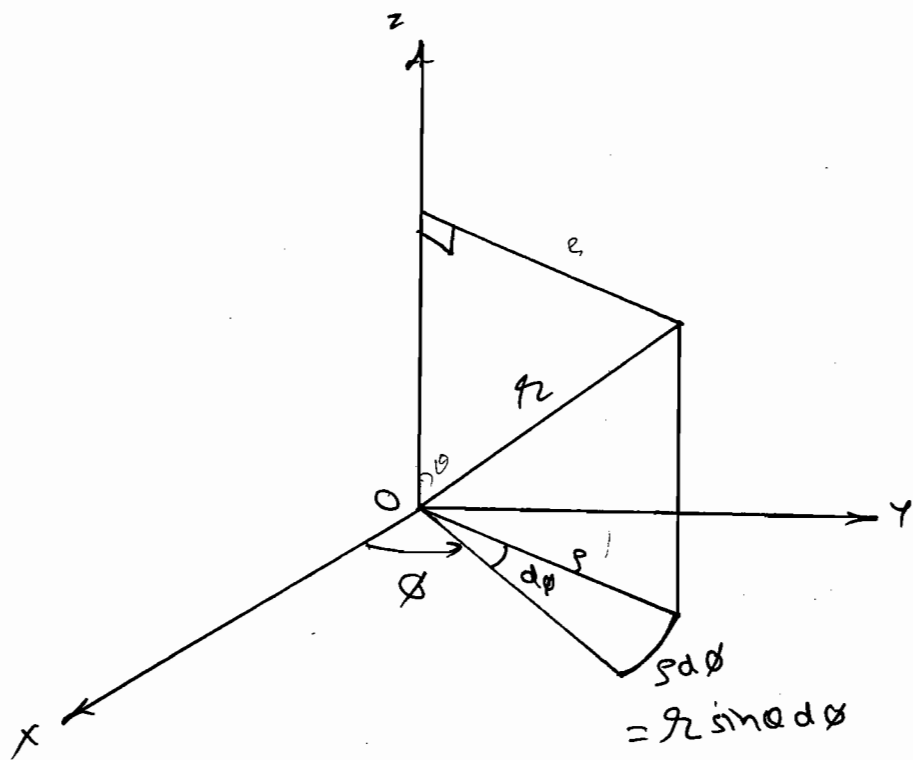
$$\therefore Q = \int_0^{\infty} \rho e^{-10z} dz \times \int_0^{\pi/2} d\phi \times \int_0^{\infty} e^{-z} dz \quad \text{nc.}$$

$$\therefore Q = \int_0^{\infty} \left[ \rho \cdot \frac{e^{-10z}}{-10} + (1) \frac{e^{-10z}}{(10)^2} \right]_0^{\infty} \times \frac{\pi}{2} \times \left[ \frac{e^{-z}}{-1} \right]_0^{\infty}$$

$$\therefore Q = \int_0^{\infty} \left[ 0 + \frac{1}{100} \right] \times \frac{\pi}{2} \times 0 + 1.$$

$$\therefore Q = \frac{+\pi}{20} \quad \text{nc.}$$

\*



$$dS = r d\theta \cdot r \sin\theta \cdot d\phi$$

$$dS = r^2 \sin\theta \cdot d\theta d\phi.$$

$\Rightarrow r = 2m, 0 \leq \theta \leq \pi, 0 \leq \phi \leq 2\pi$

$\Rightarrow$  This represents a sphere of  $2m$  centered at origin.

$ds = r^2 \sin\theta d\theta d\phi$

$\therefore S = \int_0^\pi \int_0^{2\pi} r^2 \sin\theta d\theta d\phi$   
( $\theta$ ) ( $\phi$ )  $r=2m$

$\therefore S = (2)^2 [-\cos\theta]_0^\pi [\phi]_0^{2\pi}$

$\therefore S = 4\pi(2)^2 m^2$

$\therefore S = 16\pi m^2$

Ex-1 Let  $S_u = \frac{4}{3} \frac{\cos^2\theta \cdot \sin^2\theta}{r^2(r^2+1)}$  define for universe.

Find the total charge.

Ans: Universe  $\rightarrow r \rightarrow 0 \text{ to } \infty$   
 $\theta \rightarrow 0 \text{ to } 2\pi$   
 $\phi \rightarrow 0 \text{ to } \pi$

$du = r^2 \sin\theta d\theta d\phi$

$\therefore Q = \int S_u \cdot du$

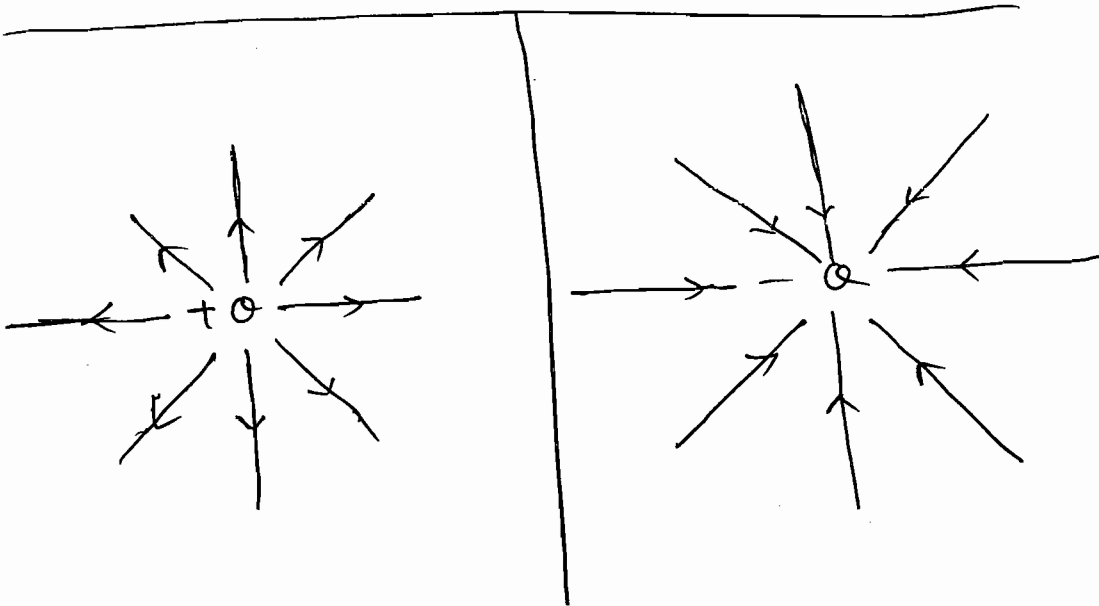
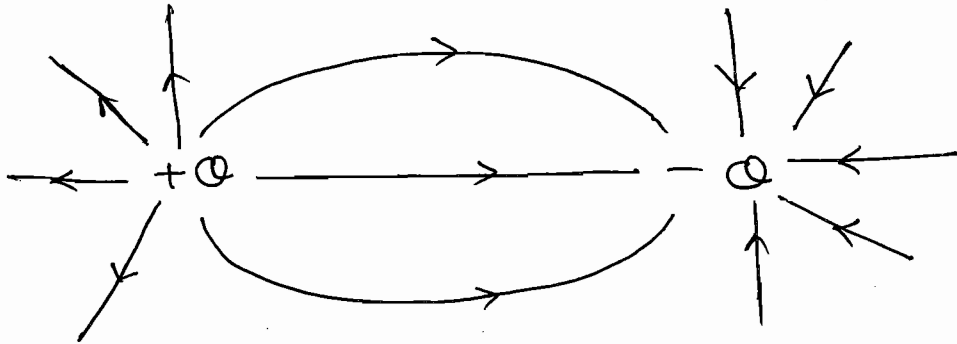
$\therefore Q = \int_0^\infty \int_0^\pi \int_0^{2\pi} \frac{4}{3} \cdot \frac{\cos^2\theta \cdot \sin^2\theta}{r^2(r^2+1)} \times r^2 \sin\theta d\theta d\phi dr$

$$= \frac{4}{3} [\tan^{-1} r]_0^{\infty} \times \left[ -\frac{\cos^3 \theta}{3} \right]_0^{\pi} \times \left[ \frac{\theta}{2} - \frac{\sin 2\theta}{4} \right]_0^{2\pi}$$

$$= \frac{4}{3} \left[ \frac{\pi}{2} \right] \times \left[ \frac{1}{3} + \frac{1}{3} \right] \times [\pi]$$

$$\therefore \boxed{\phi = \frac{4}{9} \pi^2}$$

\* Electric Flux ( $\psi$ ).



→ An Electric flux originates from a +ve charge and ends with a negative charge. In the absence of -ve charge electric flux terminates at infinity.

→ IC of electric charge would result  
 IC of electric flux rather ~~IC of~~  
 → QC of electric charge would result  
 QC of electric flux.

$$\psi = Q C$$

Ex-1 How much Electric flux would result from a non-uniform surface charge density  $\frac{8}{s^2+1}$  nC/m<sup>2</sup> define for  $s \leq 5m$ ,  $z = 4m$ .

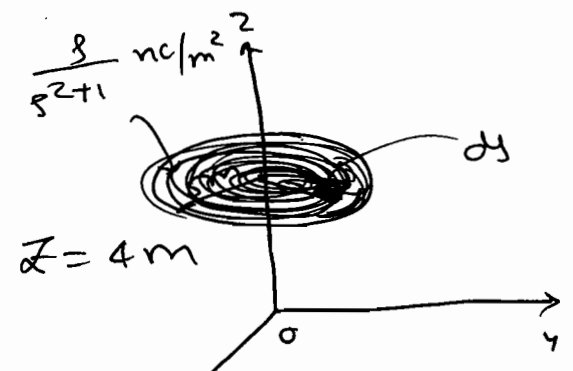
Ans:  $\frac{8}{5}$

$$ds = s ds d\phi$$

$$Q = \int_S \rho_s \cdot ds$$

$$Q = \int_{s=0}^5 \int_{\phi=0}^{2\pi} \frac{8}{s^2+1} s ds d\phi$$

$z = 4m$

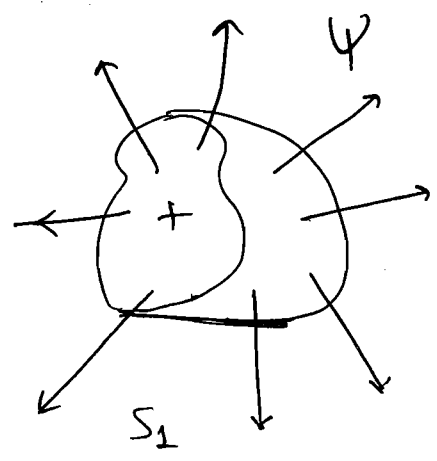


$$\psi = Q = \int_0^5 \frac{(s^2+1)-1}{(s^2+1)} ds \times [\phi]_0^{2\pi}$$

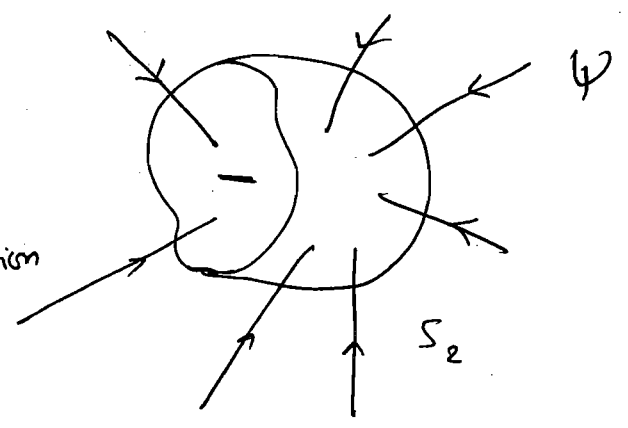
$$\psi = [5] - [\tan^{-1}s]_0^5 \times 2\pi$$

$$\psi = [5 - \tan^{-1}5] \times 2\pi \text{ nC}$$

\*



- (or)  $Q$
- (or)  $S_1$
- (or)  $S_2$
- (or) any combination



$S_1$  &  $S_2$  = arbitrary closed surfaces.

$$\psi_{net} = Q_{enc.}$$

→  $S_1$  &  $S_2$  are two arbitrary closed surfaces. We assume that they enclosed some charge configuration i.e. either  $Q$  (or)  $S_1$  (or)  $S_2$  (or) any combination. Some how we have calculated the total charge within them.

→ Further, we assume that  $S_1$  encloses +ve charge which would result flux leaving surface. The amount of electric flux leaving surface is equal to the charge enclosed within it.

→ Further we assume that  $S_2$  encloses -ve charge. ~~which~~ Therefore, the flux enter the closed surface.

→ Whether the electric flux leaving the surface or entering the surface, the electric flux passing through the closed surfaces.

→ Gauss's Law's state that the net electric flux passing through any closed surface is equal to the charge enclosed by that surface.

→  $\Psi_{net} = Q_{enc.}$

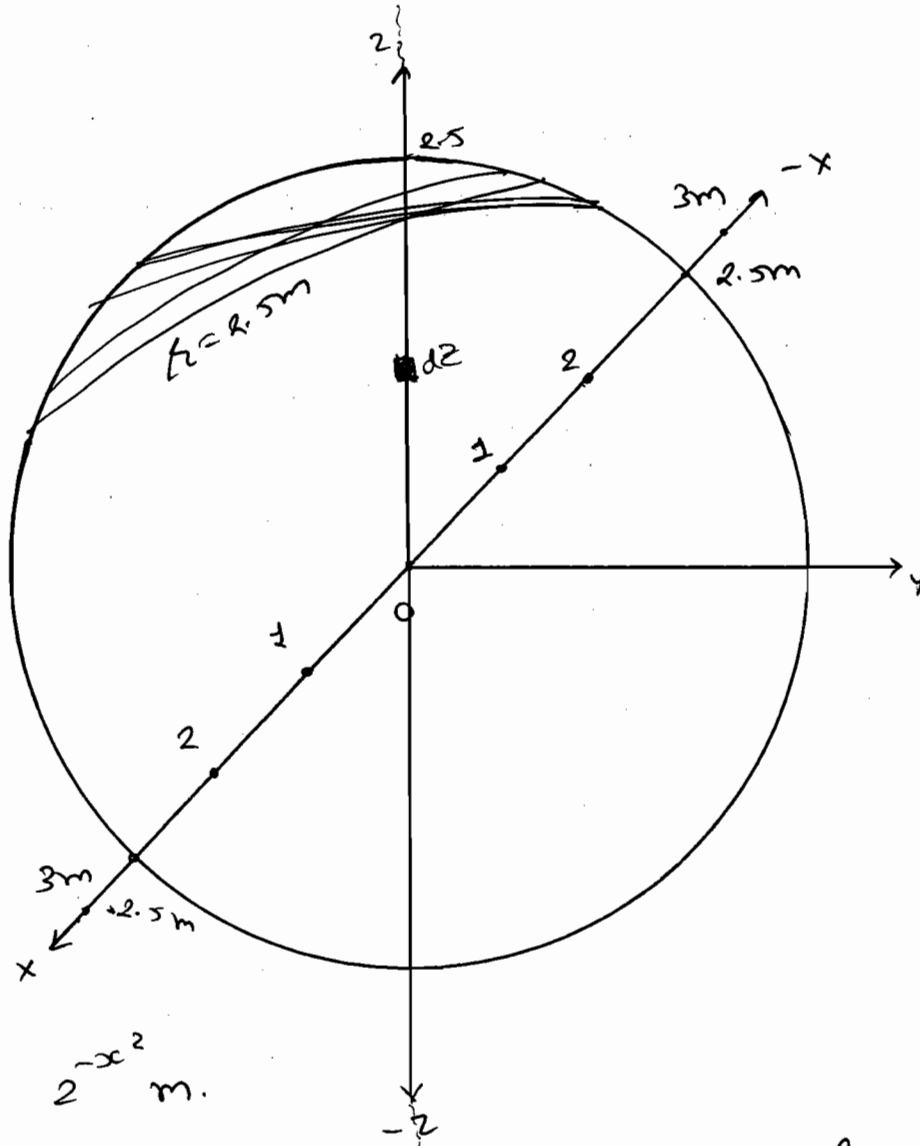
Ex-1/2 What net electric flux passes through a sphere of radius 2.5m centered at the origin. Given the charge configuration.

(1) Point charges of  $q = 2^{-x^2}$  nC, which are located on the x-axis at  $x = 0, \pm 1, \pm 2, \pm 3$  m  
Ans: 2.125 nC

(2) An infinite line with a uniform charge density of  $\frac{1}{z^2+1} = \frac{1}{z^2+1}$  nC/m lies along z-axis.  
Ans: 2.38 nC

(3) A 2m - uniform surface charge density of  $\frac{1}{x^2+y^2+4}$  nC/m<sup>2</sup>, lies in z=0 plane.  
Ans: 2.95 nC.

(4) Uniform line charge density 20nC/m, lies in z=0 plane and are located at  $y = 0, \pm 1, \pm 2, \pm 3$  m.  
Ans: 403 nC.



①  $Q = 2^{-x^2} \text{ m.}$

→ The charges at  $x = \pm 3\text{m}$  are not enclosed by the sphere

$\psi_{\text{net}} = Q_{\text{enc.}}$

$\therefore \psi_{\text{net}} = \frac{-(-3)^2}{2} + \frac{-(-2.5)^2}{2} + \frac{-(-1)^2}{2} + 2 + \frac{-(-1)^2}{2} + \frac{-(-2)^2}{2} + 0$

$\therefore \psi_{\text{net}} = \frac{1}{16} + \frac{1}{2} + 1 + \frac{1}{16} + \frac{1}{2}$

$\psi_{\text{net}} = 2.125 \text{ nC.}$

② Part of the infinite line is enclosed by sphere.

For  $|z| \leq 2.5$  (or)  $-2.5 \leq z \leq 2.5$ .

$\therefore dQ = \lambda dz$

$\therefore \psi_{\text{net}} = Q_{\text{enc.}}$



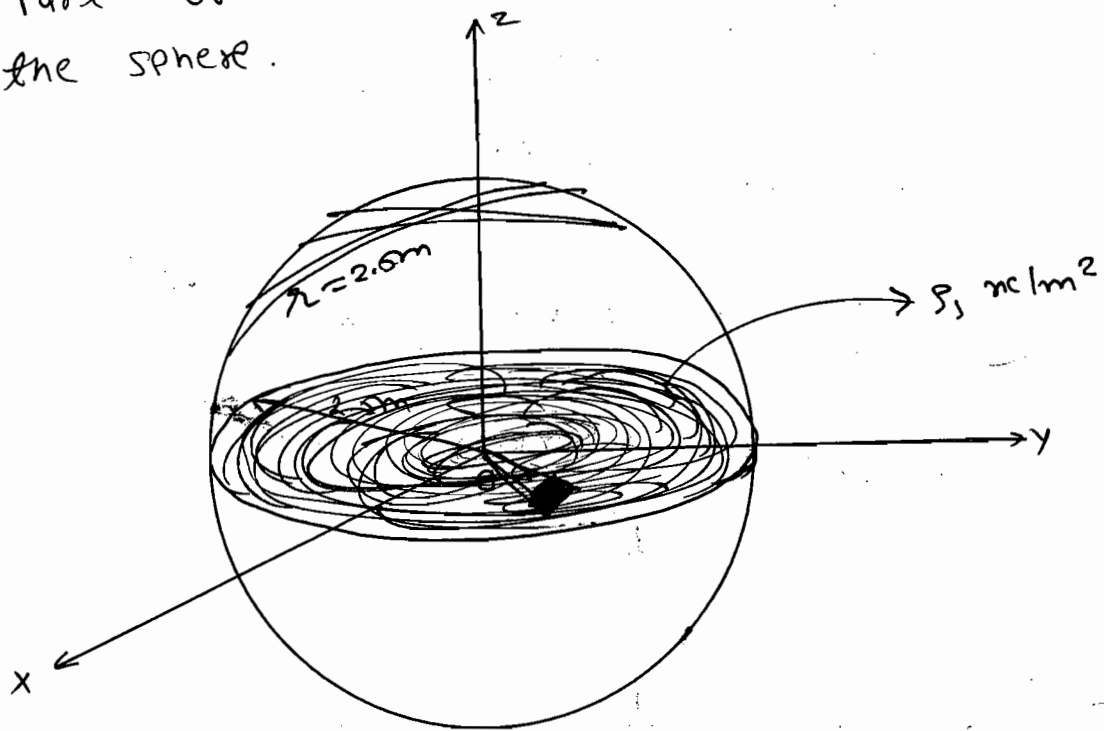
$$\therefore Q_{enc} = \int_{-2.5}^{2.5} \frac{1}{z^2+1} dz.$$

$$= \left[ \tan^{-1} z \right]_{-2.5}^{2.5}$$

keep the calci  
in Radian.

$$\therefore Q_{enc} = 2.38 \text{ nC}$$

(3) Part of the infinite sheet is enclosed by the sphere.



→ Sphere encloses a circular disk of radius 2.5m centered at origin and it located in  $z=0$  plane.

$$S_s = \frac{1}{x^2+y^2+z^2} \text{ nC/m}^2.$$

here,  $\rho \leq 2.5 \text{ m}$  ;  $z=0$

Put  $x = \rho \cos \phi$  ,  $y = \rho \sin \phi$

$$\therefore S_s = \frac{1}{\rho^2+4} \text{ nC/m}^2$$

$$\Phi = \int \rho ds d\theta$$

$$\therefore d\Phi = \rho_s ds$$

$$\therefore \Phi_{net} = Q_{enclosed}$$

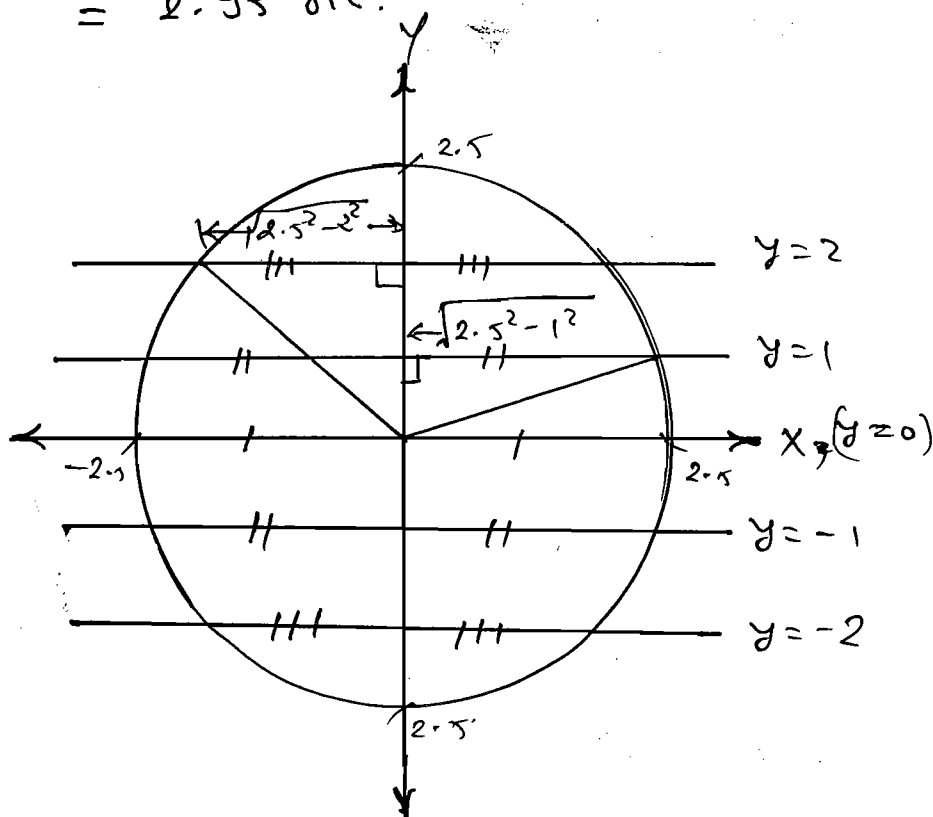
$$= \int \rho ds d\theta$$

$$= \int_{\theta=0}^{2\pi} \int_{s=0}^{2.5} \frac{\rho ds d\theta}{(s^2+4)}$$

$$= \frac{1}{2} \left[ \ln(s^2+4) \right]_0^{2.5} \times [\theta]_0^{2\pi}$$

$$= 2.95 \text{ nC.}$$

(2)

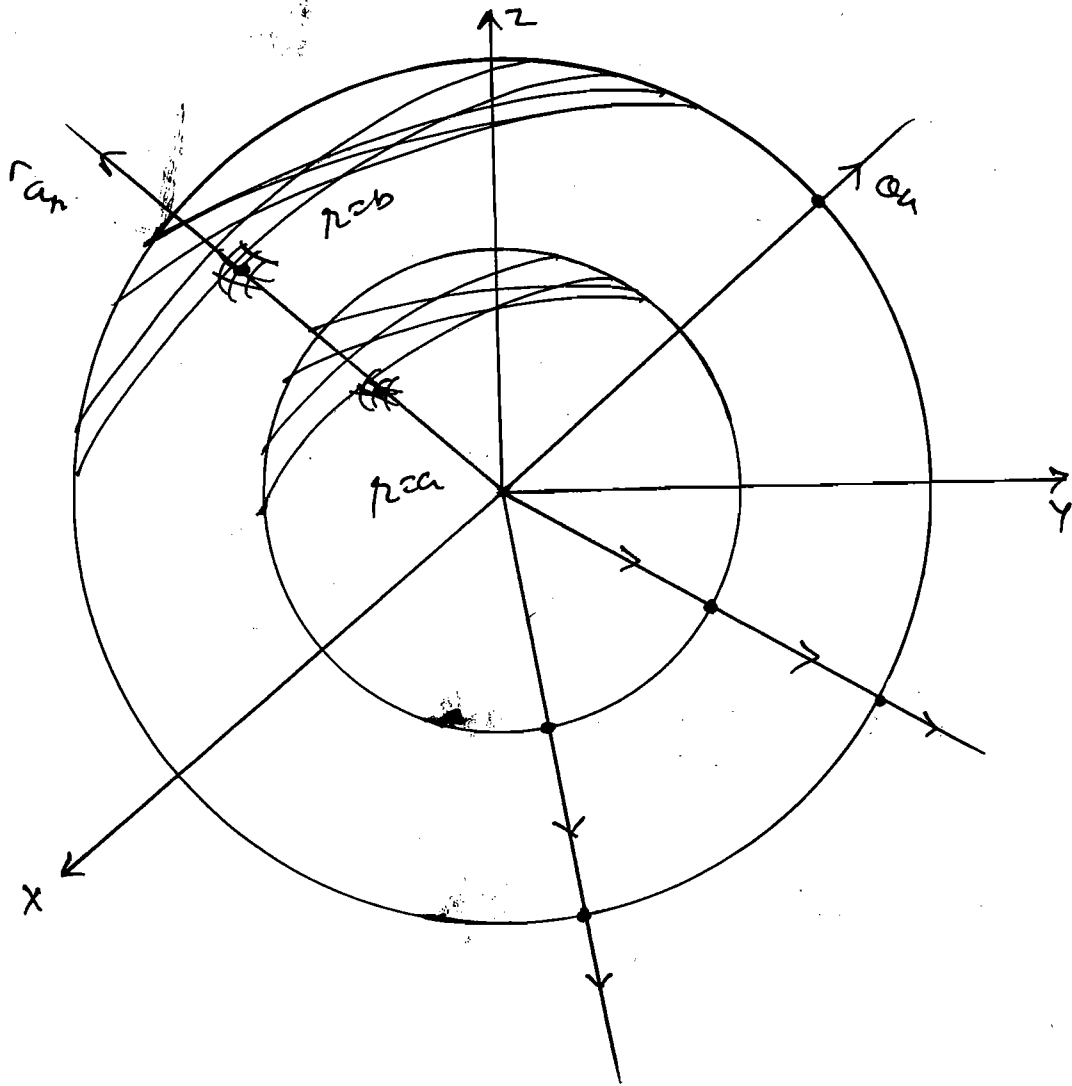


$$\rightarrow \Phi_{net} = Q_{enc.} = 20 \times 10^{-9} \left[ 4 \sqrt{2.5^2 - 2^2} + 4 \sqrt{2.5^2 - 1^2} \right]$$

$$+ 5 \times 20 \times 10^{-9}$$

$$= 403 \text{ nC.}$$

\* Electric Flux Density [ $\bar{D}$  C/m<sup>2</sup>]



→ Flux per unit Area = Electric Flux Density

→ Through  $r = a$

$$\Psi_{\text{net}} = Q_{\text{enc}} = q$$

$$\text{Surface area of Sphere} = 4\pi a^2$$

$$\therefore \text{Flux Density} = \frac{q}{4\pi a^2} \text{ C/m}^2.$$

Through  $r = b$ .

$$\text{Flux density} = \frac{q}{4\pi b^2} \text{ C/m}^2.$$

→ In general, the magnitude of the flux density through sphere of radius  $r$  m ( $r > 0$ )

$$|\bar{D}| = \frac{Q}{4\pi r^2} \text{ C/m}^2$$

→ As shown, the flux density is changing its value along radial direction ( $\hat{a}_r$ )

∴ we write

$$\bar{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

$\bar{E}$  due to  $Q$  located at the origin is given by

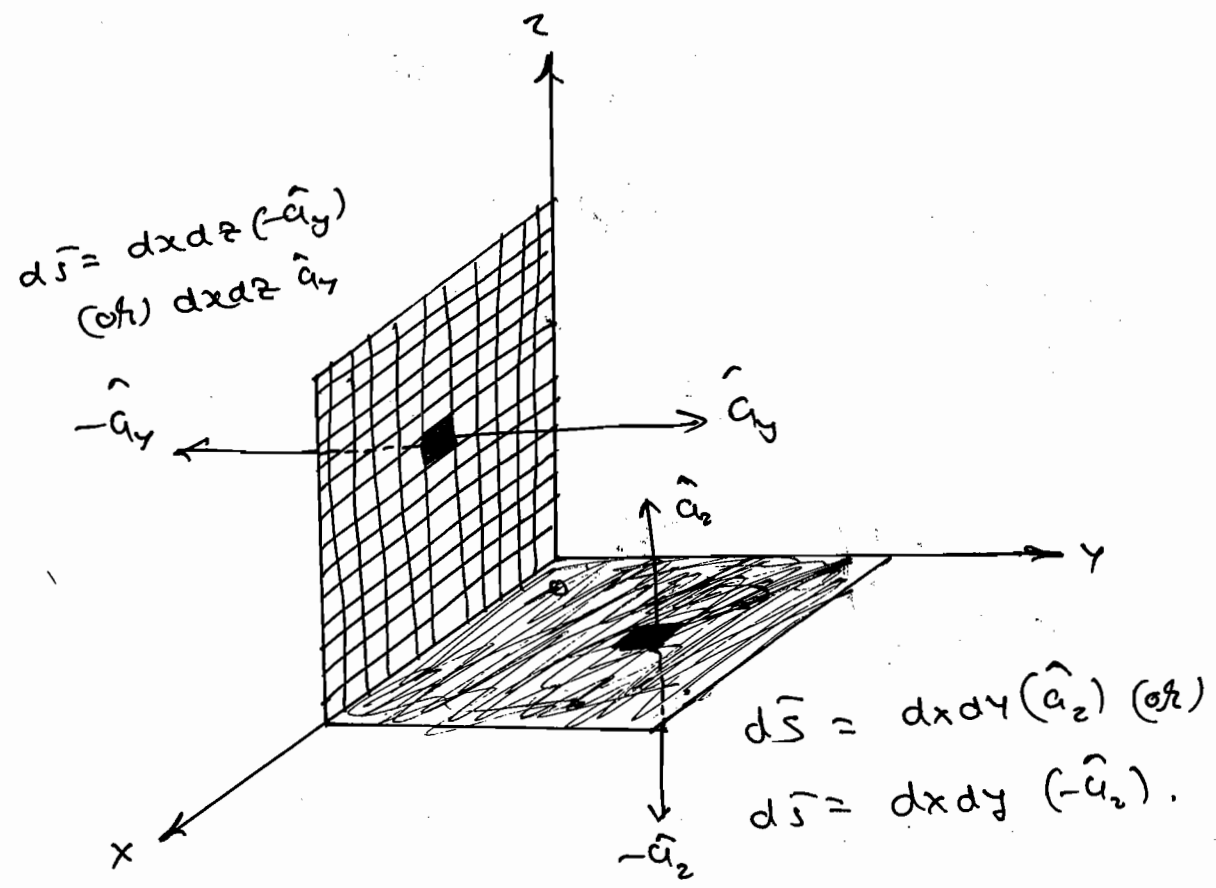
$$\bar{E} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{a}_r$$

$$\therefore \bar{D} = \epsilon \bar{E}$$

Procedure for the calculation of  $\bar{D}$  and  $\bar{E}$  are identically same.

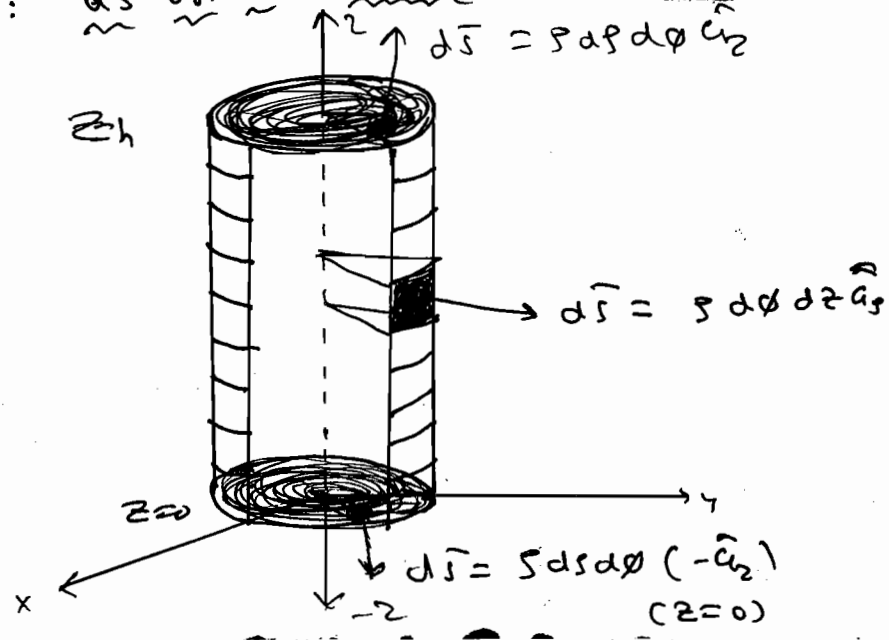
\* Vector differential surface element:  $d\vec{s}$

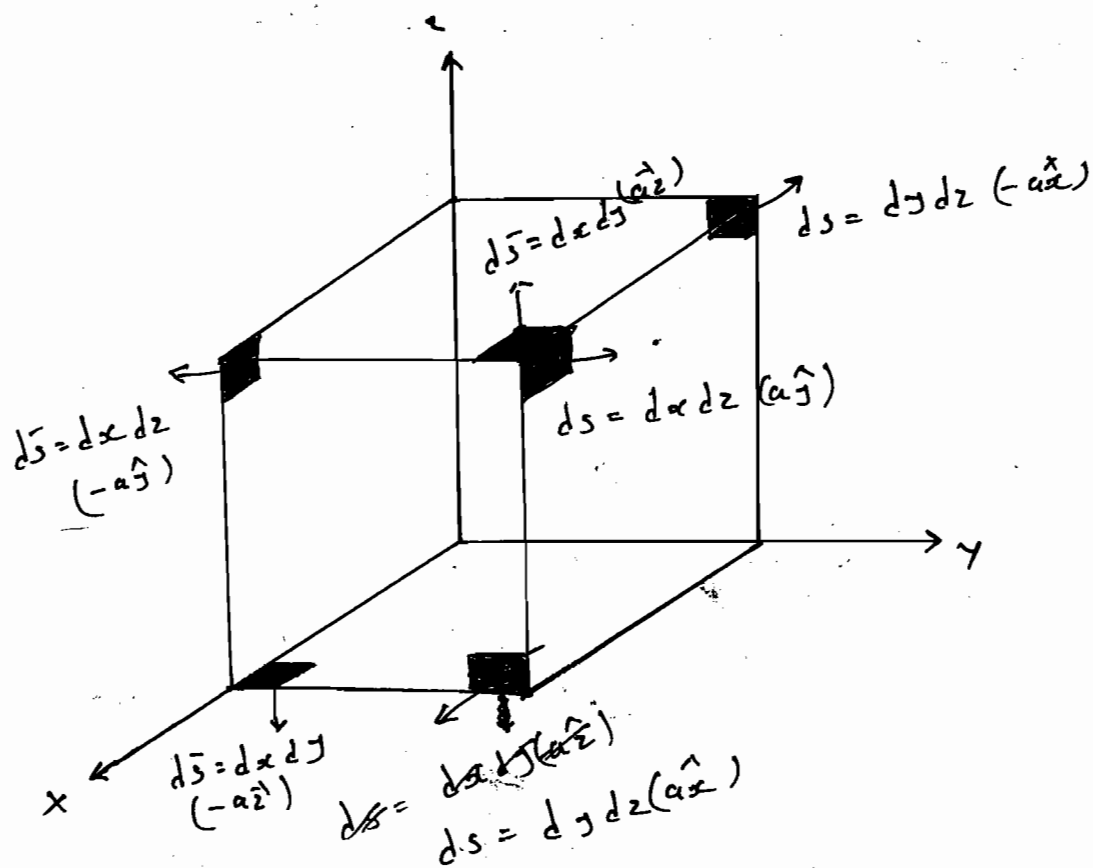
\* Case-1: open plane (or) open surface.



→ The vector differential surface element  $d\vec{s}$  at any point on the open plane would be projecting normal to the surface.

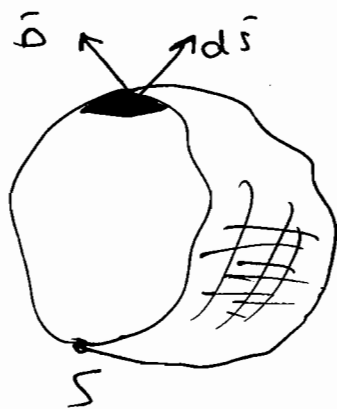
\* Case-2:  $d\vec{s}$  on a closed surface:





→ At any point on the closed surface  $d\vec{s}$  could be projecting outward normal to the surface.

\* Integral form of Gauss's Law:



→ Figure shows an arbitrary closed surface (S) at any point, on this surface  $d\vec{s}$  would be projecting outward normal to the surface.

enclosing some charge configurations. Somehow we have calculated  $\vec{D}$  at any point on the closed surface

for e.g.  $\vec{D}$  makes an angle  $\alpha$  with  $d\vec{s}$

✓ The direction of  $\vec{D}$  at any point on the closed surface will solely depend upon the charge configuration within the closed surface. Whereas direction of  $d\vec{s}$  at any point on the closed surface would be projecting outward normal to the surface.

→  $\alpha$  making any possible value bet<sup>n</sup> 0 to 180°.

→ The differential amount of flux passing through  $d\vec{s}$  i.e. in a direction normal to the surface at that point is the projection of  $\vec{D}$  on to the  $d\vec{s}$ .

→ Mathematicaly,

$$d\phi = |\vec{D}| \cdot |d\vec{s}| \cos \alpha \\ = \vec{D} \cdot d\vec{s} \quad \text{if } \alpha$$

if  $\alpha = 0$  or  $180^\circ$  max. amount of flux passes through  $d\vec{s}$

→ If  $\alpha = 90^\circ$ , zero flux passes through  $d\vec{s}$ .

→ We write Gauss Law's Integral form.

$$\therefore \Psi_{\text{net}} = \oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enc.}}$$

→ We assume that the closed surface is enclosing a volume charge density of  $\rho_v \text{ C/m}^3$ .

$$\therefore Q_{\text{enc}} = \int_V \rho_v dV$$

$$\therefore \oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dV. \quad \text{--- (1)}$$

Now, using Divergence theorem.

$$\therefore \oint_S \vec{D} \cdot d\vec{s} = \int_V \nabla \cdot \vec{D} dV. \quad \text{--- (2)}$$

∴ Comparing (1) & (2)

$$\boxed{\nabla \cdot \vec{D} = \rho_v}$$

→ This is a point form of Gauss Law.

(or) Gauss Divergence theorem.

$$\rightarrow \nabla \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$



$$\rightarrow \nabla \cdot \vec{D} = \frac{1}{r} \frac{\partial}{\partial r} (r D_r) + \frac{1}{r} \frac{\partial D_\theta}{\partial \theta} + \frac{\partial D_z}{\partial z}$$

$$\rightarrow \nabla \cdot \vec{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_\theta) + \frac{1}{r \sin \theta} \frac{\partial D_z}{\partial z}$$

Ex-1 In a region the electric flux density is given by  $\vec{D} = (2x \hat{a}_x + 3y \hat{a}_y - kz \hat{a}_z) \text{ C/m}^2$ .

Assume charge free region then find the value of  $k$ .

Ans: Charge free region  $\rho_v = 0$

$$\therefore \nabla \cdot \vec{D} = \rho_v = 0$$

$$\therefore \frac{\partial}{\partial x} D_x + \frac{\partial}{\partial y} D_y + \frac{\partial}{\partial z} D_z = 0$$

$$\therefore 2 + 3 - k = 0$$

$$\boxed{k = 5}$$

$$\therefore -kz = \text{C/m}^2$$

$$\therefore +kz = \frac{5}{z} \text{ C/m}^2$$

$$\boxed{k = 5 \text{ C/m}^3}$$

(a) 5 C/m<sup>2</sup>

(b) 5 C/m

(c) 5 C-m.

✓ (d) 5 C/m<sup>3</sup>

Ex-2 The magnitude of the Electric flux density is proportional to  $r^k$  where  $k$  is constant.  $r \rightarrow$  spherical coordinate. The  $\vec{D}$  is projecting in the radial direction. Choose the value of  $k$  such that electric flux density has zero divergence.

Ans: (a) -2 (b) -4 (c) -8 (d) -16.

$\rightarrow |\vec{D}| \propto r^k$   
 $\therefore \vec{D} = C_1 r^k \cdot \hat{a}_r = D_0 r^k \hat{a}_r$

$\therefore \nabla \cdot \vec{D} = 0$

$\therefore \frac{1}{r^2} \left( r^2 \frac{\partial D_r}{\partial r} \right) = 0$

$\therefore \frac{1}{r^2} r^2 \times C_1 r^k$

$\therefore \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) = 0$

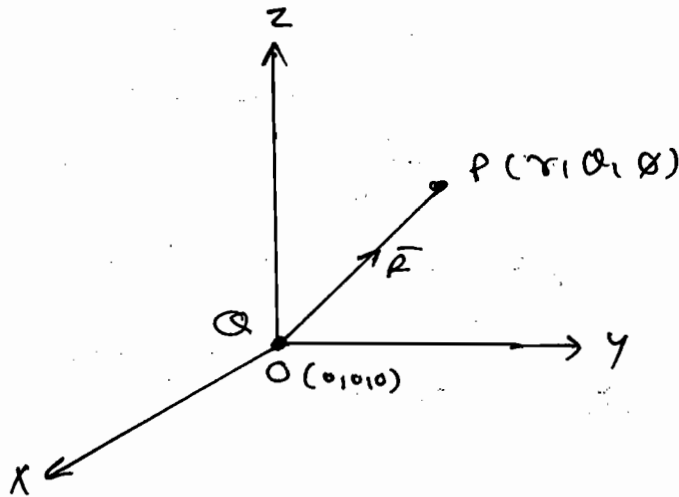
$\therefore \frac{\partial}{\partial r} (C_1 r^{k+2}) = 0$

$\therefore (k+2) r^{k+1} = 0$

$\boxed{k = -2}$

Ex-3 A point charge of  $Q$  is located at origin. If no other charge is present what is the value  $\nabla \cdot \bar{D}$  at any point other than the origin.

Ans:  $\nabla \cdot \bar{D} = 0$



$$\text{at } P \quad \bar{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

$$\bar{D} = D_r \hat{a}_r$$

$$\begin{aligned} \therefore \nabla \cdot \bar{D} &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \dots \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \cdot \frac{Q}{4\pi r^2} \right) \end{aligned}$$

$$\therefore \nabla \cdot \bar{D} = 0$$

Ex-4 Let  $\bar{D} = (4x^3 \hat{a}_x + x^2 z \hat{a}_y + 2xy \hat{a}_z) \text{ nC/m}^2$   
 $0 \leq x, y, z \leq 1$ . find the amount of  $\bar{D}$  passing through closed surface defined by  $0 \leq x, y, z \leq 1$ . and also find the amount of charge enclosed within it. also indicate whether the flux entering a close surface or

Ans:

$$\Phi_{\text{net}} = \oint_S \bar{D} \cdot d\bar{S} = \dots = Q_{\text{enclosed}}$$

$$\rightarrow \Phi_{net} = Q_{enc} = \oint_{dS} \vec{D} \cdot d\vec{S} = \int_{x=0} \vec{D} \cdot d\vec{S} + \int_{x=1} \vec{D} \cdot d\vec{S}$$

$$+ \int_{y=0} \vec{D} \cdot d\vec{S} + \int_{y=1} \vec{D} \cdot d\vec{S} + \int_{z=0} \vec{D} \cdot d\vec{S} + \int_{z=1} \vec{D} \cdot d\vec{S}$$

Surface is at	$d\vec{S}$	Surface limit	$\vec{D} \cdot d\vec{S}$	$\vec{D} \cdot d\vec{S}$ on the surface	$\int \vec{D} \cdot d\vec{S}$
$x=0$	$dydz (-\hat{a}_x)$	$0 \leq y, z \leq 1$	$-4x^3 dydz$	$-4(0)^3 dydz$	$-4 \int_0^1 \int_0^1 (0)^3 dydz = 0$
$x=1$	$dydz (\hat{a}_x)$	$0 \leq y, z \leq 1$	$+4x^3 dydz$	$+4(1)^3 dydz$	$-4 \int_0^1 \int_0^1 dydz = -4$
$y=0$	$dx dz (-\hat{a}_y)$	$0 \leq x, z \leq 1$	$-x^2 z dx dz$	$-x^2 z dx dz$	$-\int_0^1 \int_0^1 -x^2 z dx dz = -1/8$
$y=1$	$dx dz (\hat{a}_y)$	$0 \leq x, z \leq 1$	$+x^2 z dx dz$	$+x^2 z dx dz$	$+\int_0^1 \int_0^1 x^2 z dx dz = 1/8$
$z=0$	$dx dy (-\hat{a}_z)$	$0 \leq x, y \leq 1$	$-2xy dx dy$	$-2xy dx dy$	$-2 \int_0^1 \int_0^1 xy dx dy = -1/2$
$z=1$	$dx dy (\hat{a}_z)$	$0 \leq x, y \leq 1$	$2xy dx dy$	$2xy dx dy$	$+2 \int_0^1 \int_0^1 xy dx dy = 1/2$

$$Q_{enc} = 4nC$$

$\rightarrow Q_{enc} = +4nC$   
 $\rightarrow$  The enclosed charge is +ve therefore, the electric flux ~~is~~ leaving the closed surface.

$$\rightarrow \nabla \cdot \vec{D} = 12x^2 + 0 + 0 = \rho_v$$

$$\rho_v = 12x^2$$

$$\therefore Q_{enclosed} = \int_V \rho_v dV = \int_0^1 \int_0^1 \int_0^1 12x^2 dx dy dz$$

$$\therefore Q_{enc} = 12 \times \left[ \frac{y^3}{3} \right]_0^4 \left[ z \right]_0^7$$

$$= \frac{12}{3}$$

$$\therefore Q_{enc} = 4 \text{ nC.}$$

Ex-5  
 → Let,  $\vec{D} = 12x^2yz \hat{a}_x + 2xy \hat{a}_y + 3x^2z \hat{a}_z$   $\frac{\text{nC}}{\text{m}^2}$ .  
 find the amount of Electric flux passing through a surface define by  $x=1, 0 \leq y, z \leq 2$ .  
 $\hat{a}_x$  direction.

Ans:  $\vec{D} = 12x^2yz \hat{a}_x + 2xy \hat{a}_y + 3x^2z \hat{a}_z$

$$d\vec{S} = dydz \hat{a}_x$$

$$\therefore Q_{en1} = \int_0^2 \int_0^2 12yz \, dy \, dz$$

$$\vec{D} \cdot d\vec{S} = 12x^2yz$$

at  $x=1$

$$\vec{D} \cdot d\vec{S} = 12yz$$

$$= \frac{12}{4} [y^2]_0^2 [z^2]_0^2$$

$$= \frac{12}{4} \times 4 \times 4$$

$$\therefore Q_{enc} = 48 \text{ nC}$$

$$\therefore \psi_{net} = Q_{enc} = 48 \text{ nC}$$

Ex-6 Let,  $\vec{D} = \frac{r}{3} \hat{a}_r$   $\frac{\text{nC}}{\text{m}^2}$  where  $r$  is a Spherical Co-ordinate,  $\hat{a}_r$  is a unit vector in the radial direction. find  $\oint \vec{D} \cdot d\vec{S}$ , amount of electric flux passing through a sphere of radius 1m. centered at the origin. also indicate the surface of entrance.

Ans:  $\oint \vec{D} \cdot d\vec{S} = \nabla \cdot \vec{D}$

$$\begin{aligned}
 \therefore \rho_v &= \nabla \cdot \vec{D} \\
 &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \cdot D_r) \\
 &= \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \cdot \frac{\rho}{3} \right) \\
 &= \frac{3 \rho}{3 r^2}
 \end{aligned}$$

$$\boxed{\rho_v = \frac{1}{3} \rho \text{ nC/m}^3}$$

$$\begin{aligned}
 \therefore Q_{\text{enclosed}} &= \int_V \rho_v \, dV \\
 &= \int_0^1 \int_0^{2\pi} \int_0^\pi \rho_v \cdot r^2 \sin\theta \cdot dr \, d\alpha \, d\theta \\
 &= \int_0^1 \int_0^{2\pi} \int_0^\pi \frac{1}{3} \rho \cdot \sin\theta \cdot dr \, d\alpha \, d\theta \\
 &= \frac{1}{3} \times 2\pi \times [-\cos\theta]_0^\pi
 \end{aligned}$$

$$\boxed{Q_{\text{enclosed}} = \frac{4\pi}{3} \rho = Q_{\text{net}} = \rho \cdot V}$$

$$\therefore Q_{\text{enclosed}} = \oint_S \vec{D} \cdot d\vec{S}$$

$$d\vec{S} = r^2 \sin\theta \cdot d\alpha \, d\theta \cdot \hat{e}_r$$

$$\therefore \vec{D} \cdot d\vec{S} = \frac{\rho r^3}{3} \sin\theta \cdot d\alpha \, d\theta$$

$$\therefore Q_{\text{enclosed}} = \int_0^\pi \int_0^{2\pi} \frac{\rho r^3}{3} \sin\theta \cdot d\alpha \, d\theta$$

$r = 1 \text{ m}$

$$= \frac{1}{3} [2\pi] [-\cos 0] \pi$$

$$= \frac{1}{3} \times 2\pi \times 2$$

$$\therefore \mathcal{Q}_{\text{enclosed}} = \frac{4\pi}{3} \rho c = \psi_{\text{net}}$$

→ <sup>flux</sup> Leaving the sphere as  $\rho$  is +ve.

Ex-6 Let,  $\vec{D} = -\frac{20}{r^2} [\sin^2 \theta \hat{a}_r + \sin 2\theta \hat{a}_\theta] \text{ nC/m}^2$

find the amount of electric flux passing through a closed region define by  $1 \leq r \leq 2$ ,

$$0 \leq \theta \leq \frac{\pi}{2}, \quad 0 \leq z \leq 1.$$

Ans:

$$\vec{D} = -\frac{20}{r^2} [\sin^2 \theta \hat{a}_r + \sin 2\theta \hat{a}_\theta] \text{ nC/m}^2.$$

$$\begin{aligned} \therefore \nabla \cdot \vec{D} &= \frac{1}{r} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (D_\theta \sin \theta) \\ &= \frac{1}{r} \cdot \frac{\partial}{\partial r} \left( -\frac{20}{r} \sin^2 \theta \right) + \frac{1}{r \sin \theta} \left[ \frac{\partial}{\partial \theta} \left( -\frac{20}{r^2} \sin 2\theta \right) \right] \end{aligned}$$

$$\nabla \cdot \vec{D} = \frac{+20 \sin^2 \theta}{r^3} + \left( -\frac{40}{r^3} \cos 2\theta \right)$$

$$\therefore \rho_v = \frac{20 \sin^2 \theta}{r^3} - \frac{40}{r^3} \cos 2\theta = \frac{20}{r^3} \left[ \frac{1}{2} - \frac{\cos 2\theta}{2} - 2 \cos 2\theta \right]$$

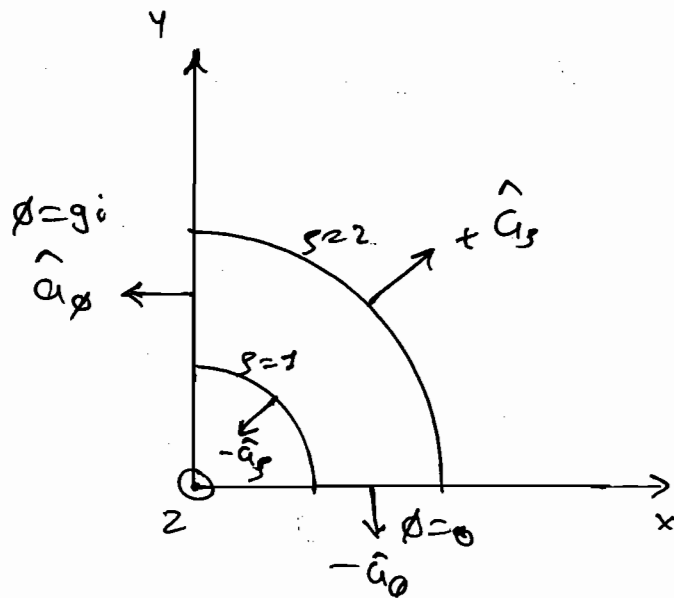
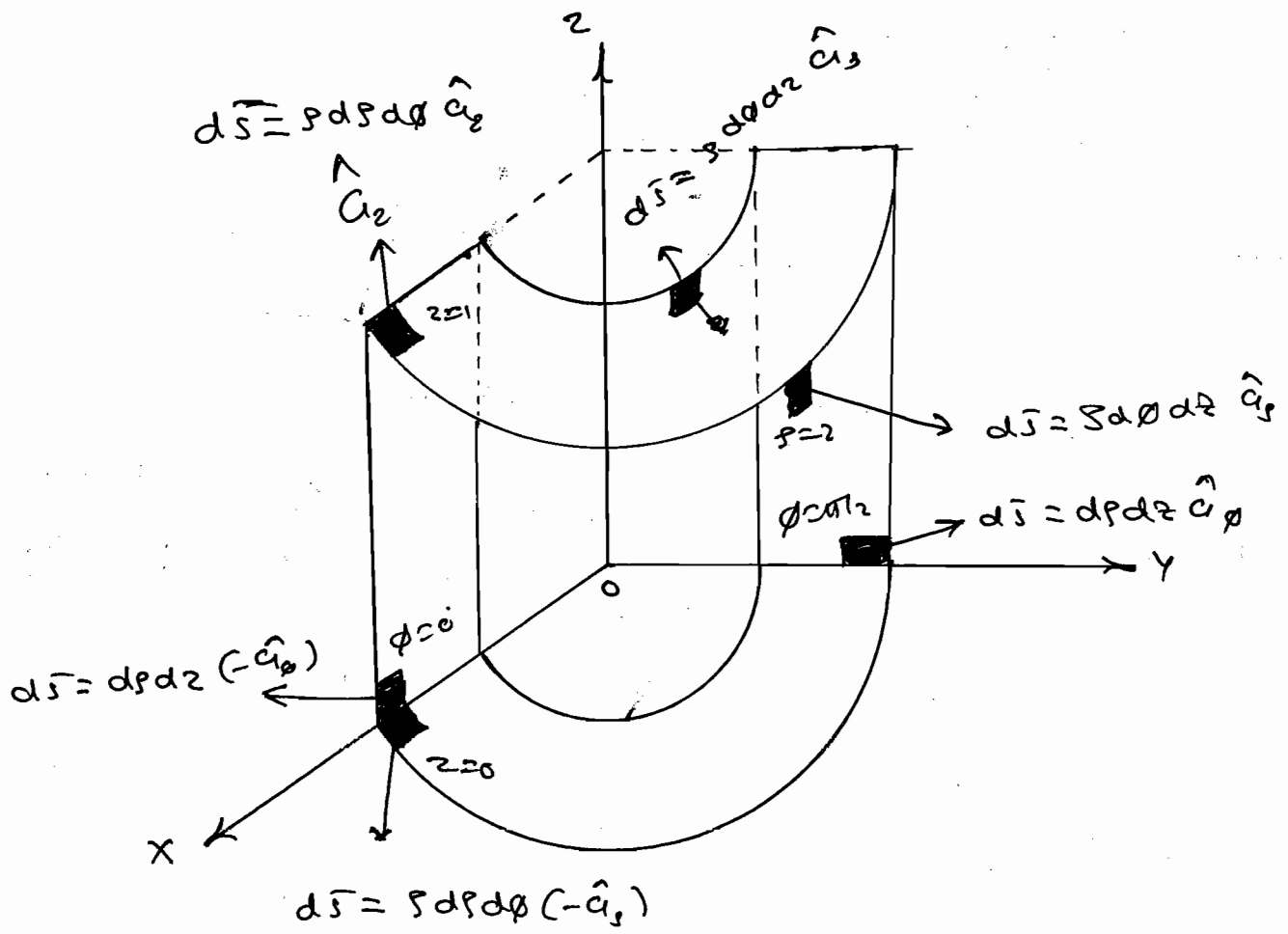
$$\rho_v = \frac{20}{r^3} \left[ \frac{1}{2} - \frac{5}{2} \cos 2\theta \right]$$

$$\therefore \mathcal{Q}_{\text{enclosed}} = \psi_{\text{net}} = \int_V \rho_v dV$$

$$= \int_1^2 \int_0^{\pi/2} \int_0^{2\pi} \frac{20 \sin^2 \theta}{r^3} \cdot r^2 dr d\theta dz$$

$$= 20 \left[ -\frac{1}{r} \right]_1^2 \times \left[ \frac{\theta}{2} + \frac{\sin 2\theta}{4} \right]_0^{\pi/2} \times \pi$$

$$= \frac{+10 \times \pi}{2} = +2.5 \pi \text{ nC}$$





\* Work:

→ Work is defined as a force acting over distance.

→ Work done in moving a charge of  $q$  Coloumbs from an initial point to the final point in the vicinity of electric field is given by

$$W = -q \int_{\text{initial}}^{\text{final}} \vec{E} \cdot d\vec{r} \quad \text{Joules.}$$

Ex-1 find a w.o. in moving a 5  $\mu\text{C}$  Charge from the origin to  $(2, -1, 4)$  m through the field  $(2xyz \hat{a}_x + x^2z \hat{a}_y + x^2y \hat{a}_z)$  V/m. via the path  $(0, 0, 0)$  to  $(2, 0, 0)$  to  $(2, -1, 0)$  to  $(2, -1, 4)$ .

Ans:  $d\vec{r} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$ .

$$\vec{E} \cdot d\vec{r} = 2xyz dx + x^2z dy + x^2y dz$$

$$W.O. = -q \int_{\text{initial}}^{\text{final}} 2xyz dx + x^2z dy + x^2y dz$$

→  $d\vec{r} = dr \hat{a}_r + r d\theta \hat{a}_\theta + dz \hat{a}_z$   
 $d\vec{r} = dx \hat{a}_x + r d\phi \hat{a}_\phi + r \sin\alpha d\theta \hat{a}_\theta$

$$W.D. = -q \left[ \int_1 \vec{E} \cdot d\vec{r} + \int_2 \vec{E} \cdot d\vec{r} + \int_3 \vec{E} \cdot d\vec{r} \right]$$

∴ ① Path-1 (0, 0, 0) to (2, 0, 0).

$$x \rightarrow 0 \text{ to } 2$$

$$y = 0 \Rightarrow dy = 0 \quad x = 2$$

$$z = 0 \Rightarrow dz = 0$$

$$\therefore I_1 = \int_0^2 \vec{E} \cdot d\vec{r} = \int_0^2 0 \cdot dz = 0$$

② Path-2: (2, 0, 0) to (2, -1, 0)

$$\therefore x = 2 \Rightarrow dx = dz = 0$$

$$y = 0 \text{ to } -1$$

$$z = 0$$

$$\therefore I_2 = \int_0^{-1} 4y \, dy = 0$$

③ Path-3: (2, -1, 0) to (2, -1, 4)

$$x = 2 \Rightarrow dx = 0$$

$$y = -1 \Rightarrow dy = 0$$

$$z = 0 \text{ to } 4$$

$$I_3 = \int_0^4 -4 \cdot dz$$

$$I_3 = -16$$

$$\therefore W.D. = -q [ I_1 + I_2 + I_3 ]$$

$$= -5 \times 10^{-6} [-16]$$

$$\therefore \boxed{W.D. = 80 \mu J}$$

Ex. 2 Repeat the above example ~~with~~ the ~~same~~  $z$

Path  $x = -2y, z = 2x.$

Ans:  $d\vec{r} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z.$  (0,0,0) to (2,-1,4).

$\therefore \vec{E} \cdot d\vec{r} = 2xy z^{ax} + x^2 z dz + x^2 y dz.$

$W = -q \int_{initial}^{final} \vec{E} \cdot d\vec{r} = -5 \times 10^{-6} \left[ \int_0^2 xy z dx + \int_0^{-1} x^2 z dy + \int_0^4 x^2 y dz \right].$

$= -5 \times 10^{-6} \left[ \int_0^2 -x^3 dx + \int_0^{-1} 2x^3 dx + \int_0^4 -x^3 dz \right].$

$= -5 \times 10^{-6} \left[ -2 \left[ \frac{1}{4} \right] - \left[ \frac{1}{2} \right] - \left[ \frac{1}{256} \right] \right].$

$= -5 \times 10^{-6} \left[ \frac{1}{8} + 1 + \frac{1}{256} \right].$

$W = -5 \times 10^{-6} \left[ 2 \int_0^2 -x^3 dx + \int_0^{-1} 8y^3 dy + \int_0^4 -\frac{z^3}{8} dz \right].$

$\therefore W = -5 \times 10^{-6} \left[ -\frac{1}{8} + \frac{8^2}{4} - \frac{648}{8} \right]$

$= -5 \times 10^{-6} \left[ -6 - \frac{1}{8} \right].$

$W = \frac{49 \times 5}{8} \times 10^{-6} \text{ J.}$

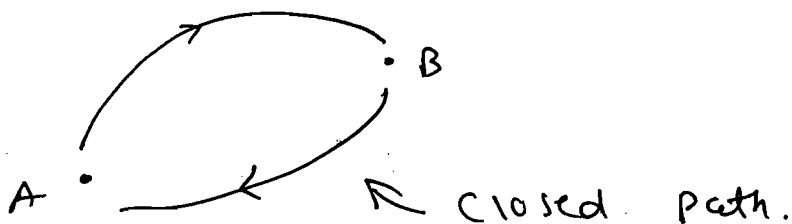
→  $(x_1, y_1, z_1)$  to  $(x_2, y_2, z_2)$ .

$(x_1, y_1)$  to  $(x_2, y_2)$        $(x_1, z_1)$ ,  $(x_2, z_2)$ .

$$\therefore \frac{y-y_1}{y_2-y_1} = \frac{x-x_1}{x_2-x_1}$$

$$\frac{z-z_1}{z_2-z_1} = \frac{x-x_1}{x_2-x_1}$$

\*\*



→  $\oint \vec{E} \cdot d\vec{r} = 0 \Rightarrow$  '0' can't be zero.

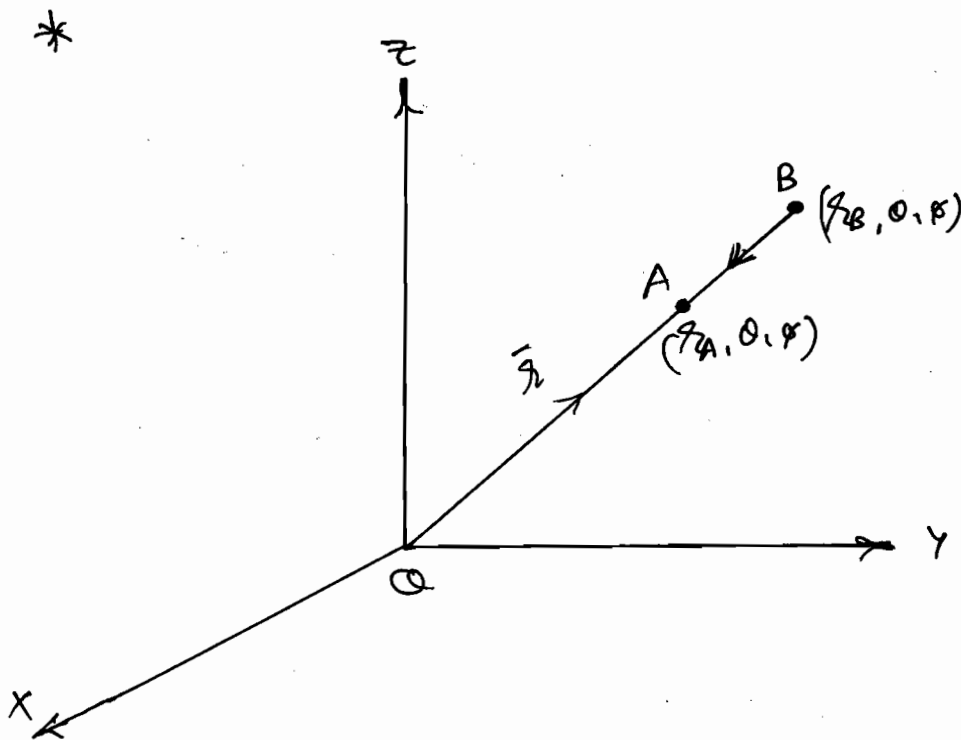
$\oint \vec{E} \cdot d\vec{r} = 0 \Rightarrow$  Work done over a closed path is ZERO.

## \* Potential:

$$\rightarrow W = -q \int_B^A \vec{E} \cdot d\vec{l} \quad \text{J}$$

We define the potential at 'A' with ref. to 'B' is given by,

$$V_{AB} = \frac{W}{q} = - \int_B^A \vec{E} \cdot d\vec{l} \quad \text{J/C (or) Volts.}$$



$$\rightarrow \vec{E} = \frac{q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

From B to A  $d\vec{l} = dr \hat{a}_r$ .

$$\therefore \vec{E} \cdot d\vec{l} = \frac{q}{4\pi\epsilon_0 r^2} \cdot dr$$

$$V_{AB} = - \int_{r_B}^{r_A} \frac{q}{4\pi\epsilon_0 r^2} dr$$

$$\therefore V_{AB} = \frac{q}{4\pi\epsilon} \left[ \frac{1}{r_A} - \frac{1}{r_B} \right].$$

if  $r_B$  is chosen at infinity,

$$r_B \rightarrow \infty$$

$$\frac{1}{r_B} = 0.$$

Then,

$$V_{AB} = \frac{q}{4\pi\epsilon r_A} = V_A.$$

In general

$$V_p = \frac{q}{4\pi\epsilon (r)} + C.$$

$V_p$  is the potential at P due to 'q'.  $r$  is the distance b/w the charge 'q' and the observation point 'P'.

$C=0$  if the ref. point is chosen at infinity.

### \* Potential Function:

→ Potentials is a functions of space

$$\text{Co-ordinates } V(x, y, z) \quad (\text{or})$$

$$V(r, \theta, z) \quad (\text{or})$$

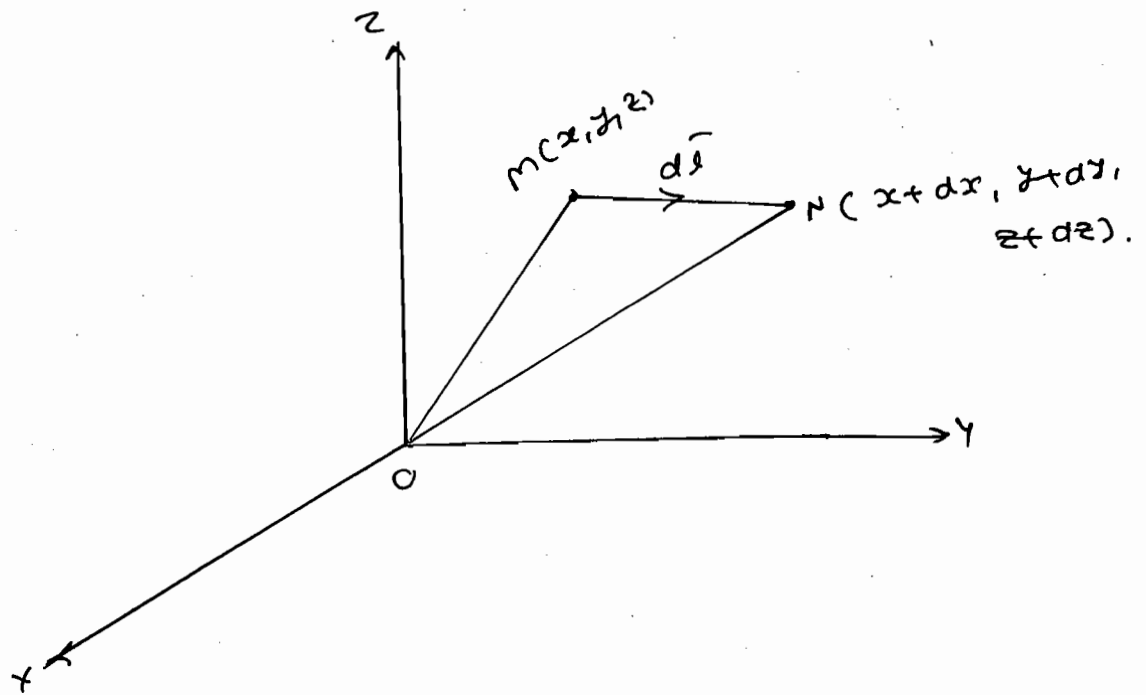
$$V(r, \theta, \phi).$$

\* Relation b/w Potential gradient and Electric field: 87

→ We assume that two neighborhood points  $M, N$  because of some charge configuration we have known the potential function  $V(x, y, z)$ .

→ Further, we assume that potential at  $M$  is different from potential at  $N$  and there exist a potential difference of  $dV$  volts.

→



→ (1)  $d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$ .

$V(x, y, z)$  is known.

(2)  $dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$ .

• We introduce  $\nabla$  (or) Del (or) gradient operator

→ gradient of scalar function in vector.

(3)  $\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$ .

(2) in terms of (1) & (3).

$$dV = \nabla V \cdot d\vec{l} \quad - (4)$$

$$\therefore V = - \int \vec{E} \cdot d\vec{l}$$

$$\therefore dV = - \vec{E} \cdot d\vec{l} \quad - (5)$$

From (4) & (5)

$$\therefore - \vec{E} \cdot d\vec{l} = \nabla V \cdot d\vec{l}$$

suppressing  $d\vec{l}$  on both sides.

$$\boxed{\vec{E} = - \nabla V.}$$

(I) Electric field is the gradient of the scalar electric potential functions.

(II) (a) From eq (5) we can conclude that electric field points normal to an equipotential surface.

(b)  $\vec{E}$  would be project from a higher potential surface to towards lower potential surface.

\* Equipotential surface:

→ It is that surface on which the potential difference bet<sup>n</sup> any two points is 0.

→ we assume that the points m and n lies on equipotential surface.

(c) From eq (4) we can conclude that Potential can vary its value normal to an equipotential surface.



$$\rightarrow \nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \rightarrow V(x, y, z)$$

$$\rightarrow \nabla \cdot V = \frac{\partial V}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{a}_\theta + \frac{\partial V}{\partial z} \hat{a}_z \rightarrow V(r, \theta, z)$$

$$\rightarrow \nabla \cdot V = \frac{\partial V}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \hat{a}_\phi \rightarrow V(r, \theta, \phi)$$

Ex: 1  
~~→~~ ~~→~~ ~~→~~ ✓

In a certain region the potential field distribution is given by  $V(r) = 100\sqrt{r}$  volts where,  $r$  is spherical coordinates assume

medium to be free space. Find  $\vec{E}$ ,  $\vec{D}$  & amount of flux passing through a sphere of radius 5m. centered at origin. also <sup>find</sup> ~~indicate~~ charge enclosed and also indicate the flux entering <sup>the surface</sup> or <sup>the</sup> ~~the~~ <sup>surface</sup> ~~surface~~.

Ans:  $V(r) = 100(r)^{1/2}$

$$\therefore \vec{E} = -\nabla \cdot V$$

$$\therefore \vec{E} = -\frac{d}{dr} (100r^{1/2})$$

$$= -100 \times \frac{1}{2\sqrt{r}} \hat{a}_r$$

$$\therefore \vec{E} = \frac{-50}{\sqrt{r}} \hat{a}_r \text{ V/m.}$$

$$\therefore \vec{D} = \epsilon \vec{E}$$

$$\therefore \vec{D} = \frac{-50 \epsilon_0}{\sqrt{r}} \hat{a}_r \text{ V/m. C/m}^2$$

$$\therefore Q = \oint_S \vec{D} \cdot d\vec{S} = \oint_S \dots$$

$$\therefore Q = \int \dots d\theta$$

$$\therefore \nabla \cdot \vec{D} = + \frac{50}{2} \epsilon_0 r^{-3/2}$$

$$\therefore Q_{\text{enclosed}} = \int_0^5 \int_0^\pi \int_0^{2\pi} \epsilon_0 r^2 \sin\theta \cdot dr d\theta d\phi$$

$$= [2\pi] [-\cos\theta]_0^\pi \times 25 \times \int_0^5 (r^2)^{1/2} \cdot dr$$

$$= 100\pi \times \frac{2}{3} (5)^{3/2}$$

$$\vec{D} \cdot d\vec{J} = -50 \epsilon_0 r^{3/2} \sin\theta \cdot d\theta d\phi$$

at  $r=5m$

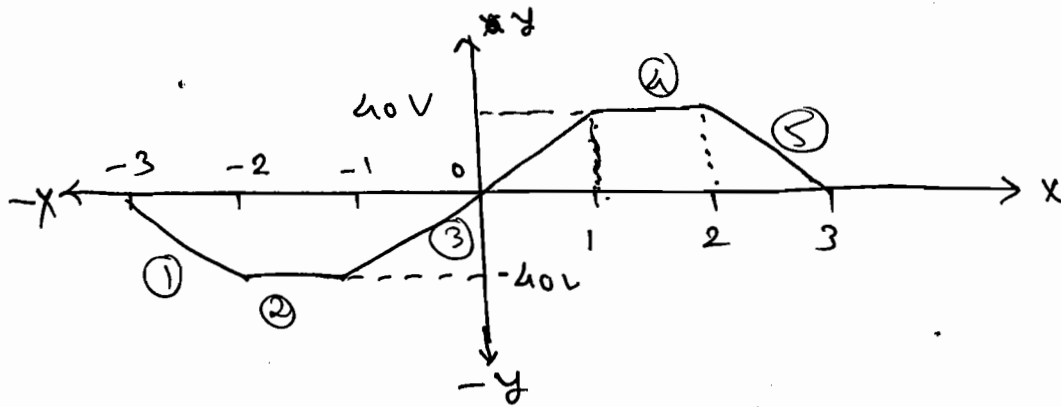
$$\vec{D} \cdot d\vec{J} = -50 \epsilon_0 (5)^{3/2} \sin\theta \cdot d\theta d\phi$$

$$\begin{aligned} \therefore \psi_{\text{net}} = Q_{\text{enc}} &= \oint \vec{D} \cdot d\vec{J} \\ &= -50 \epsilon_0 (5)^{3/2} \int_0^\pi \int_0^{2\pi} \sin\theta \cdot d\theta d\phi \end{aligned}$$

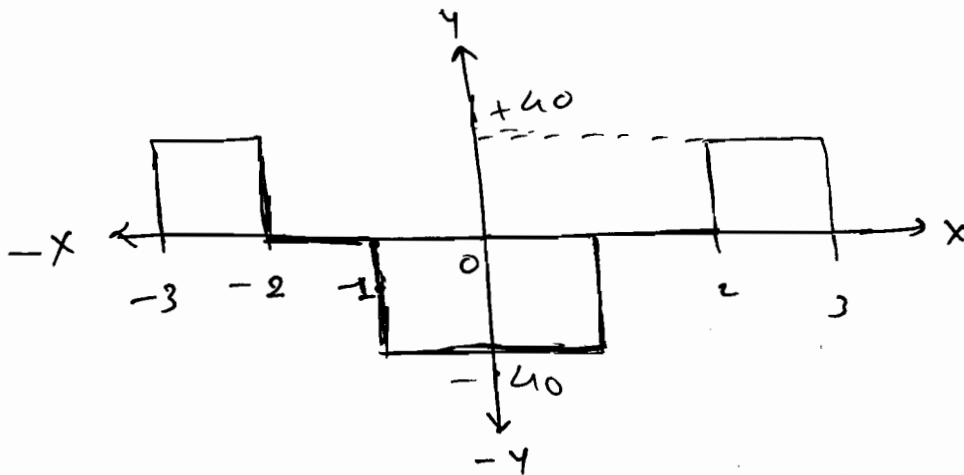
$$\psi_{\text{net}} = Q_{\text{enc}} = -50 \epsilon_0 (5)^{3/2} (4\pi) C$$

$\therefore -\psi'$  is entering to the closed surface.

Ex-2 In certain region the potential field  $\phi$  is given by the following sketch plot the corresponding electric field.



Ans:



→

seg-②

$$-2 < x < -1.$$

$$V(x) = -40V$$

$$E_x = -\frac{dV}{dx} = 0$$

seg-③  $-1 < x < 1.$

$$(-1, -40), (1, 40)$$

$$\Delta V = 40$$

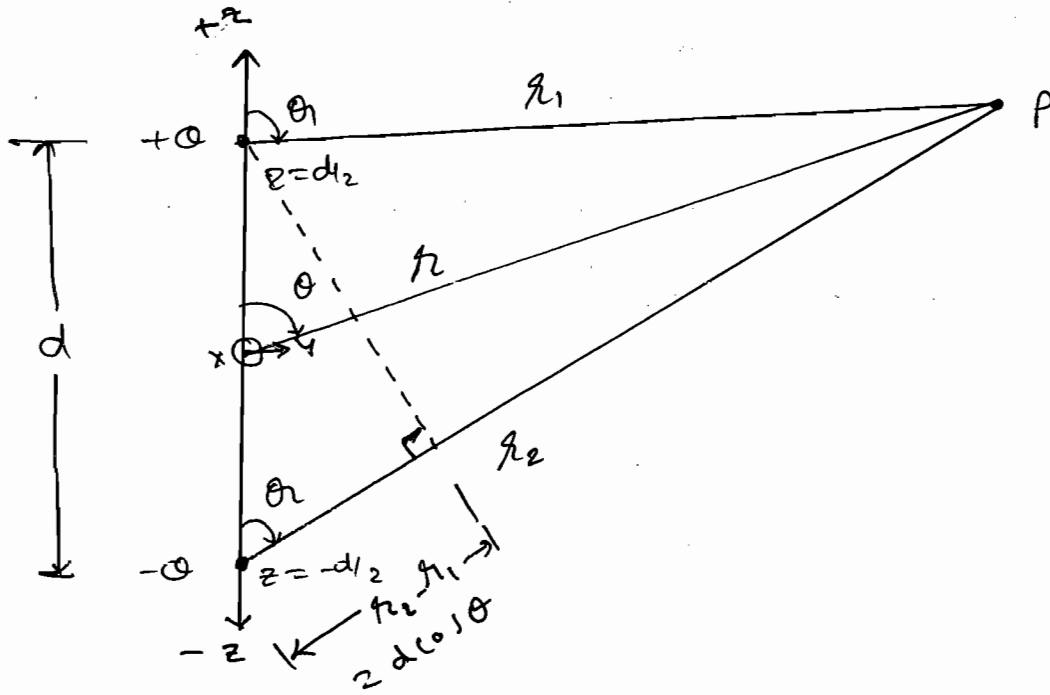
$$V(x) + 40 = 40(x + 1).$$

$$\therefore V(x) = 40x.$$

$$\therefore E_x = -\frac{\partial V}{\partial x}.$$

$$\therefore \boxed{E_x = -40 \text{ V/m}}$$

# \* Dipole:



$$\rightarrow V_P = \frac{q}{4\pi\epsilon} \left[ \frac{1}{r_1} - \frac{1}{r_2} \right]$$

$$V_P = \frac{q}{4\pi\epsilon} \left[ \frac{r_2 - r_1}{r_1 \cdot r_2} \right]$$

$$\therefore r \gg d$$

$$\Rightarrow \theta_1 \approx \theta_2 \approx \theta$$

$$\therefore r_2 - r_1 = d \cos \theta$$

$$\frac{1}{r_1 \cdot r_2} = \frac{1}{r^2}$$

$$\therefore V_P = \frac{q}{4\pi\epsilon} \times \frac{d \cos \theta}{r^2}$$

$$\therefore \boxed{V_P = \frac{q d \cos \theta}{4\pi\epsilon r^2}}$$

$$\therefore \boxed{V_P \propto \frac{1}{r^2}}$$

Ans:  $\vec{E} = -\nabla V$

$$\therefore \vec{E} = -\frac{\partial V}{\partial r} \hat{a}_r - \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{a}_\theta$$

$$\vec{E} = \left( \frac{qd \cos \theta}{2\pi \epsilon r^2} \hat{a}_r + \frac{qd \sin \theta}{4\pi \epsilon r^2} \hat{a}_\theta \right) \frac{1}{m}$$

$$\therefore \vec{E} = \left( \frac{qd \cos \theta}{2\pi \epsilon r^2} \hat{a}_r + \frac{qd \sin \theta}{4\pi \epsilon r^2} \hat{a}_\theta \right) \frac{1}{m}$$

✓

So, for the quantities  $\vec{E}$ ,  $\psi$ ,  $\vec{D}$  &  $V$  have been analyzed. From the knowledge of given charge configuration, there are no procedure available for the measurement of this charge configuration but there are procedures available for the measurement of potentials at the given points.

→ From the known potentials if we are able to develop potential function i.e.  $V(x, y, z)$  or  $V(r, \theta, z)$  or  $V(r, \theta, \phi)$  then

$$\begin{aligned} \vec{E} &= -\nabla V \\ \vec{D} &= \epsilon \vec{E} \\ \oint_S \vec{D} \cdot d\vec{s} &= Q_{enc} = \psi_{net} \\ \nabla \cdot \vec{D} &= \rho_v \end{aligned}$$

→ For developing this potential Poisson's eq<sup>n</sup> and Laplace eq<sup>n</sup> are used.

\* Poisson's and Laplacian's Eq<sup>n</sup>:

$$\nabla \cdot \bar{D} = \rho_v$$

$$\nabla \cdot (\epsilon \bar{E}) = \rho_v$$

(Homogeneous medium).

$$\epsilon \nabla \cdot \bar{E} = \rho_v$$

$$\therefore \nabla \cdot \bar{E} = \frac{\rho_v}{\epsilon}$$

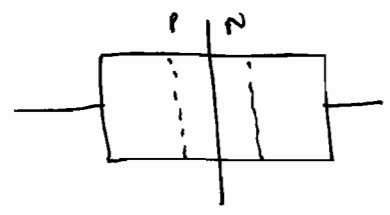
$$\therefore \nabla \cdot (-\nabla V) = \frac{\rho_v}{\epsilon}$$

$$\therefore \boxed{\nabla^2 V = -\frac{\rho_v}{\epsilon}} \rightarrow \text{Poisson Eq<sup>n</sup>}$$

in a region of interest if  $\rho_v = 0$

then  $\boxed{\nabla^2 V = 0}$   $\rightarrow$  Laplacian Eq<sup>n</sup>.

$\rightarrow$  For analysing junction characteristics of a PN diode one dimensional Poisson's Eq<sup>n</sup> is used because junction has a charge i.e. it is an ionic region.

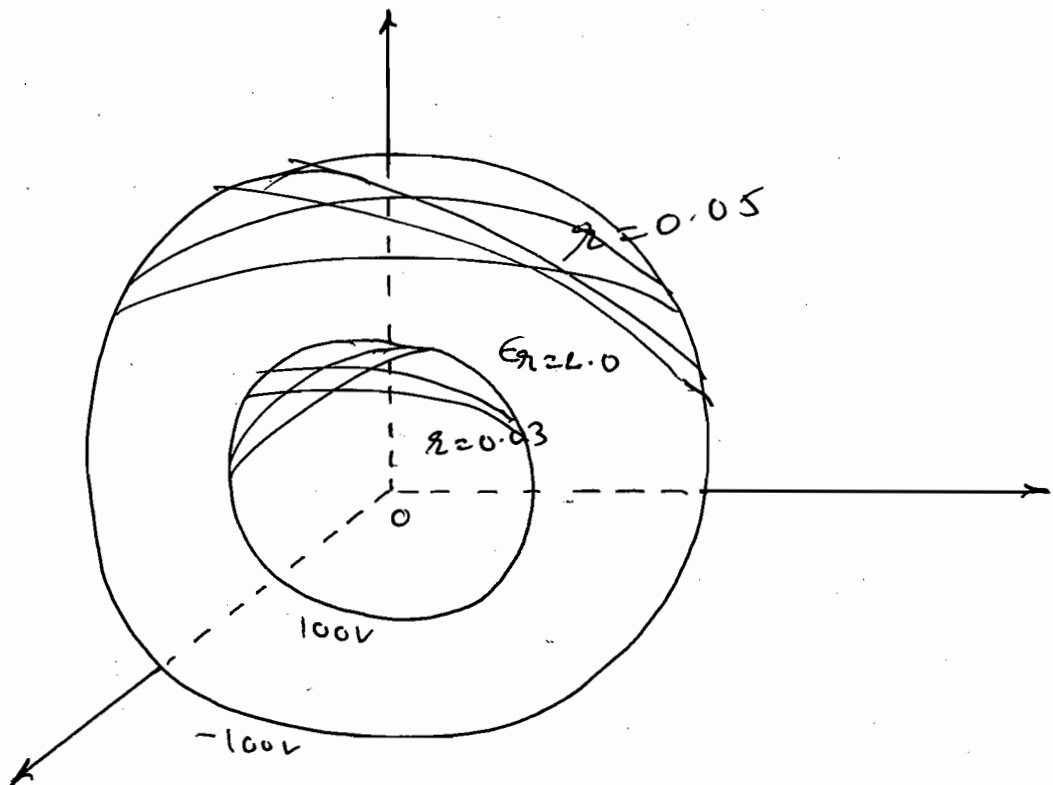


$$\frac{d^2V}{dx^2} = -\frac{\rho}{\epsilon} \text{ (PE)}$$

Ex-1 Two concentric conducting spheres of radii 3 cm and 5 cm are centered at origin. The potential on the inner sphere is 100 V, while the outer sphere is yet -100 V. The region bet<sup>n</sup> them is filled with a homogeneous dielectric having  $\epsilon_r$  relative permittivity 2.0. Find

- ① potential function.
- ② potential mid way bet<sup>n</sup> the conducting sphere.
- ③ The value of  $r$  at which  $V=0$ .
- ④ Find the expression for electric field.

Ans:



→ as shown in figure, there exists equipotential surfaces at  $r = \text{constant}$ . We know that potential varies normal to equipotential surface.

→ Therefore, Potential  $V$  must be a  $r$  alone.  
 Since  $\rho_v$  is not mention bet<sup>n</sup> the sphere.  
 We assume  $\rho_v = 0$ . Therefore, Laplacian eq<sup>n</sup>  
 reduces to

$$\nabla^2 V = 0$$

$$\therefore \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial V}{\partial r} \right) = 0.$$

∴ Cross multiply and integrate,

$$\therefore r^2 \frac{\partial V}{\partial r} = C_1$$

$$\therefore \frac{dV}{dr} = \frac{C_1}{r^2}$$

∴ integrate again

$$\therefore V = -\frac{C_1}{r} + C_2$$

$$V \text{ (at } r = 0.03) = 100 = -\frac{C_1}{0.03} + C_2$$

$$V \text{ (at } r = 0.005) = -100 = -\frac{C_1}{0.05} + C_2$$

Solve  $C_1$  and  $C_2$ .

$$\therefore C_1 = -15, C_2 = -400$$

$$V(r) = \left( \frac{15}{r} - 400 \right) \text{ Volts.}$$

$$(1) V(r) = \left( \frac{15}{r} - 400 \right) \text{ V.}$$

$$(2) V \text{ (at } r = 0.04 \text{ m)}$$

$$V(0.04) = \left( \frac{15}{0.04} - 400 \right)$$



(3)  $0 = \frac{15}{r} - 400$

$\therefore V=0$  at  $r = \frac{15}{400}$  m.

$\therefore r = 3.75 \text{ cm}$

(4)  $\vec{E} = -\nabla \cdot V$

$= -\frac{\partial V}{\partial r} \hat{a}_r$

$\therefore \vec{E} = +\frac{15}{r^2} \hat{a}_r \text{ V/m.}$

→ The obtained  $\vec{E}$  is projecting along  $\hat{a}_r$  direction and it is projecting from a higher potential surface to towards lower potential.

\* Current: (I).

→ It is a rate of charge.

→  $J = \rho_v \cdot v = \sigma \vec{E}$

$\vec{J}_c = \rho_v \vec{v}_d \text{ A/m}^2$

$\vec{J}_c = \sigma \vec{E} \text{ A/m}^2$

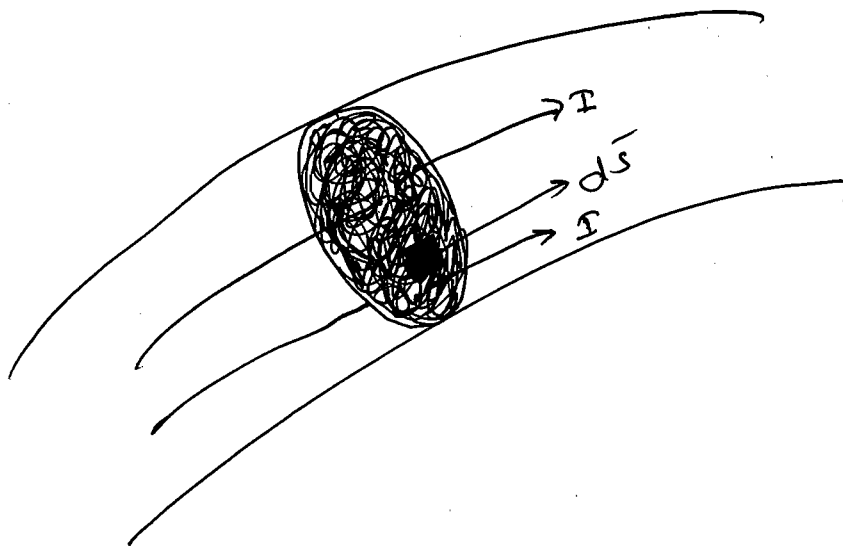
$\vec{J}_c$  : Conduction current density (A/m<sup>2</sup>)

$\rho_v$  : Volume charge density (C/m<sup>3</sup>).

$\sigma$  : Conductivity (V/m).

$\vec{v}_d$  : drift velocity (m/s).

$\vec{E}$  = Applied Electric field.



→ Across, 'S', we know the Conduction current density ( $\vec{J}_c$   $\text{A/m}^2$ )

→ The diff. amount of current  $dI$  passing length  $d\vec{s}$  is given by

$$dI = \vec{J}_c \cdot d\vec{s}$$

$$\therefore I = \int_S \vec{J}_c \cdot d\vec{s}$$

Ex-1 In certain region the conduction current density is given by  $-10^5 \nabla V$   $\text{A/m}^2$  where  $V = 10 e^{-x} \sin y$  volts. scalar electric potential function. Find

- ① Conductivity of medium.
- ② Amount of current passing through  $x=1, 0 \leq y \leq 1$  in  $\hat{u}_x$  direction.

Ans: ①  $\vec{J}_c = \sigma \vec{E}$ .

$\vec{J}_c = \sigma (-\nabla V)$ .

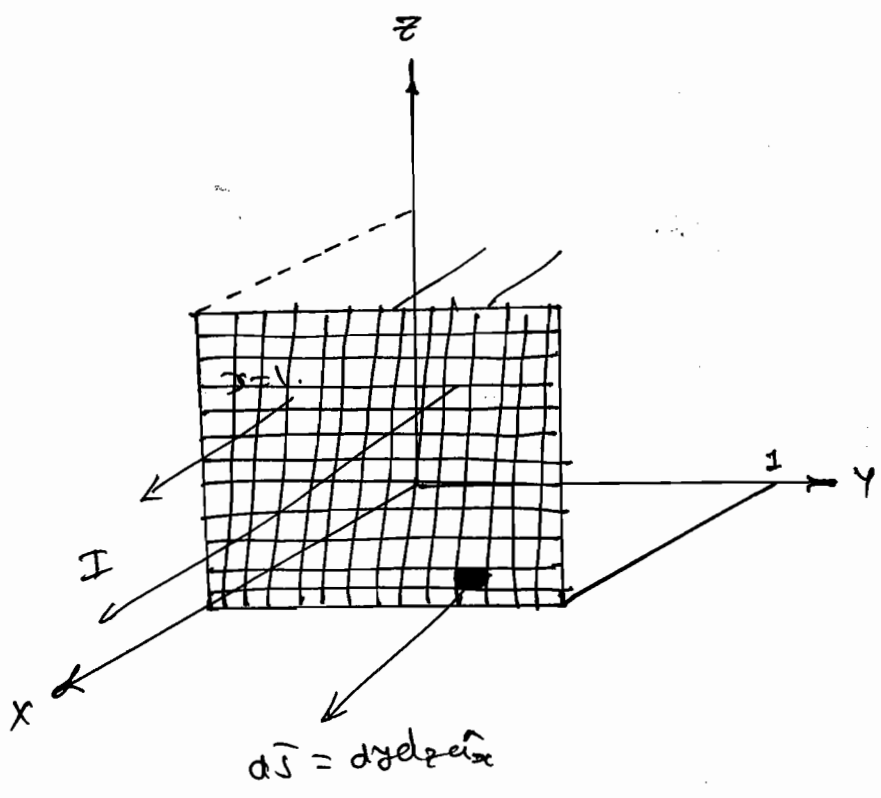
$\therefore \vec{J}_c = 10^5 (-\nabla V)$ .

$\vec{J}_c \therefore \sigma = 10^5 \text{ cm}^{-1}$ .

②  $\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y$ .

$\nabla V = (10^6 e^{-x} \cos y \hat{a}_x - 10^6 e^{-x} \sin y \hat{a}_y)$

$\therefore \vec{J}_c = 10^6 e^{-x} \sin y \hat{a}_x - 10^6 e^{-x} \cos y \hat{a}_y$ .



$\rightarrow \vec{J}_c \cdot d\vec{S} = 10^6 e^{-x} \sin y \, dy \, dz$ .

$\vec{J}_c \cdot d\vec{S} = 10^6 e^{-1} \sin y \, dy \, dz$ .

At  $x=1$

$I = \int_S \vec{J}_c \cdot d\vec{S} = 10^6 e^{-1} \int_0^1 \int_0^1 \sin y \, dy \, dz$

$$= 10^6 e^{-1} [1 - \cos 13] A.$$

↑ keep the calci in Red.

$$\therefore \boxed{I = 169 \text{ KA}}$$

\* Continuity of a Current Equation:

$$\rightarrow \oint_S \vec{J}_c \cdot d\vec{S} = - \frac{dq}{dt} = - \frac{d}{dt} \int_V \rho_v dV.$$

$$(oh) \quad \oint_S \vec{J}_c \cdot d\vec{S} = - \frac{\partial}{\partial t} \int_V \rho_v dV. \quad - (1)$$

Using divergence theorem.

$$\oint_S \vec{J}_c \cdot d\vec{S} = \int_V \nabla \cdot \vec{J}_c \cdot dV. \quad (2)$$

$$\therefore \therefore \boxed{\nabla \cdot \vec{J} = - \frac{\partial \rho_v}{\partial t}}$$

Point form.

$$\begin{aligned} \rightarrow \vec{J} &= \sigma \cdot \vec{E} \\ \nabla \cdot \vec{J} &= \sigma \cdot \nabla \cdot \vec{E} \\ \nabla \cdot \vec{J} &= \sigma \cdot \nabla \cdot \left( \frac{\vec{D}}{\epsilon} \right) \\ \therefore \nabla \cdot \vec{J} &= \frac{\sigma}{\epsilon} \cdot \nabla \cdot \vec{D} \\ \therefore \nabla \cdot \vec{J} &= \frac{\sigma}{\epsilon} \rho_v \\ \therefore \frac{\sigma}{\epsilon} \rho_v &= - \frac{d\rho_v}{dt} \end{aligned}$$

$$\therefore \frac{d\rho_e}{dt} + \frac{\sigma}{\epsilon} \rho_e = 0$$

$$\therefore m + \frac{\sigma}{\epsilon} = 0$$

$$\therefore m = -\frac{\sigma}{\epsilon}$$

$$\therefore \rho_e = C_1 e^{-\frac{\sigma}{\epsilon} t}$$

$$\therefore \rho_e = C_1 e^{-t/\tau}$$

where,  $\tau = \epsilon/\sigma$ .

$\tau =$  Relaxation time.

→ We conclude that as the time progresses the charge density inside a conductor decays exponentially. The rate at which it decays exponentially depends upon conductivity of the conductor. If a conductor having infinite conductivity the density inside a conductor tends to zero within no time. In other words, for a transient time there may be some non zero charge inside a conductor.

→ Further we can conclude that if any charge is present in any conductor it resides on the surface of the conductor only.

Ex-1 Find the relaxation time for a copper conductor whose conductivity is  $56 \text{ MS/m}$ .  
 assume  $\epsilon = \epsilon_0$ . also find % of charge density after 1 relaxation time and after  $5$  relaxation time.

→  $\tau = \frac{\epsilon_0}{\sigma}$

$\therefore \tau = \frac{8.85 \times 10^{-12}}{56 \times 10^6}$

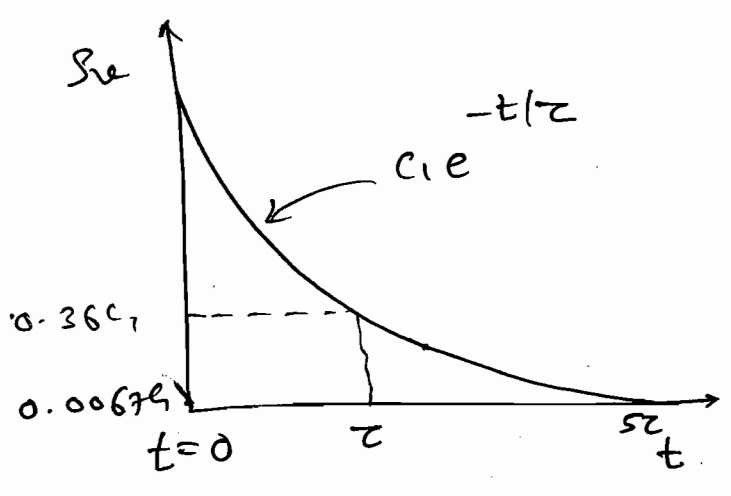
$\therefore \tau = 1.6 \times 10^{-19} \text{ s}$

→  $\rho_e \text{ (at } t = \tau) = C_1 e^{-\tau/\tau} = C_1/e = 0.36 C_1$

$\rho_e \text{ (at } t = \tau) = 36.1.06 C_1$

$\rho_e \text{ (at } t = 5\tau) = C_1 e^{-5\tau/\tau} = C_1/e^5 = 0.0067 C_1$

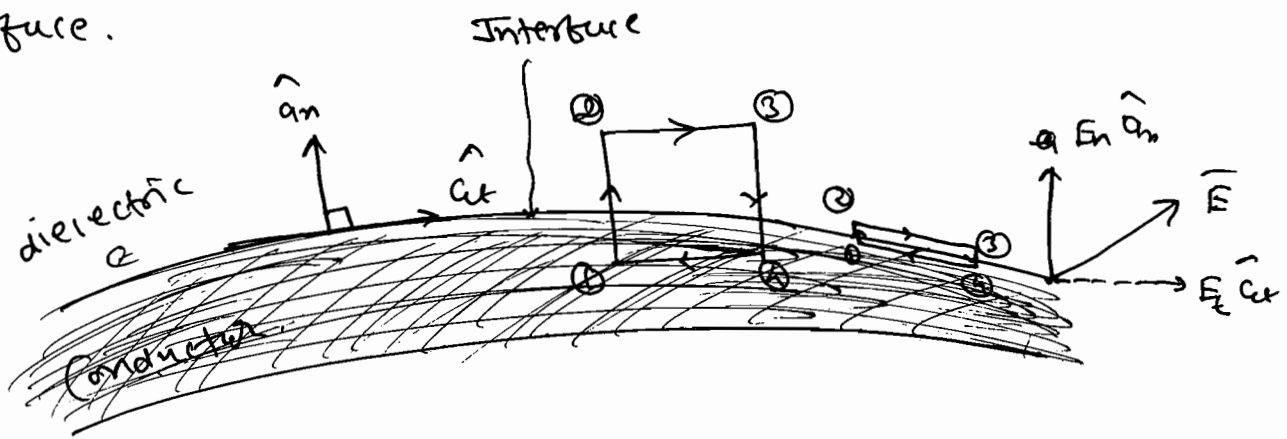
$\therefore \rho_e \text{ (at } t = 5\tau) = 0.67.1.06 C_1$



\* Boundary Conditions:

\* Case-1: Conductor interface. (OR) Conductor to dielectric interface.

→ An interface is a plane like structure where two mediums are interacting. In this case we assume conductor interface (OR) Conductor to dielectric interface. we have to investigate behaviour of electric field and electric flux density across the interface.



→  $\hat{n}$ : Normal unit vector directed from conductor to dielectric.

→  $\hat{t}$ : Unit vector tangential to the interface.

→  $\oint \vec{E} \cdot d\vec{l} = 0.$

$\Rightarrow \int_{1-2} \vec{E} \cdot d\vec{l} + \int_{2-3} \vec{E} \cdot d\vec{l} + \int_{3-4} \vec{E} \cdot d\vec{l} + \int_{4-1} \vec{E} \cdot d\vec{l} = 0.$

*(Note: The integral from 4-1 is circled and labeled as zero because it is inside the conductor.)*

→ The  $\int_{4-1}$  has to be computed inside a conductor.

→ The charge is zero inside a conductor.

Therefore, Electric field is zero inside a conductor and hence this integral vanishes.

→ We are interested to investigate behaviour of electric field across interface. To accomplish this we choose path like 1-2 and 3-4 so small such that the path 2-3 is grazing the interface, which would result the  $\int_{1-2}$  and  $\int_{3-4}$  vanishing.

$$\rightarrow \int_{2-3} \vec{E} \cdot d\vec{l} = 0.$$

→ For path (2-3)  $\Rightarrow d\vec{l} = dl \hat{a}_t$

$$\text{Let } \vec{E} = E_n \hat{a}_n + E_t \hat{a}_t$$

This is assumed across the interface.

$$\therefore \vec{E} \cdot d\vec{l} = E_n \hat{a}_n \cdot dl \hat{a}_t + E_t \hat{a}_t \cdot dl \hat{a}_t$$

$$\therefore \vec{E} \cdot d\vec{l} = E_t dl$$

$$\therefore \Rightarrow \int E_t \cdot dl = 0.$$

$\therefore$   $E_t$  can't be zero.

$$\therefore \boxed{E_t = 0}$$

→ Tangential components of electric field across a conductor to dielectric interface vanishing.



→ Across a Conductor interface identify the correct one from the following: where  $\bar{E}$  is the electric field across the interface

$\hat{a}_t$  : unit vector tangential to interface.

$\hat{a}_n$  : the unit vector normal to interface.

(i)  $\bar{E} \cdot \hat{a}_t = 0$

(v)  $\bar{D} \cdot \hat{a}_n = \rho_s$

(ii)  $\bar{E} \times \hat{a}_n = 0$

(vi)  $\bar{D} \cdot \hat{a}_t = 0$

(iii)  $\hat{a}_n \times \bar{E} = 0$

(vii)  $\hat{a}_n \cdot \bar{D} = \rho_s$

(iv) All the above.

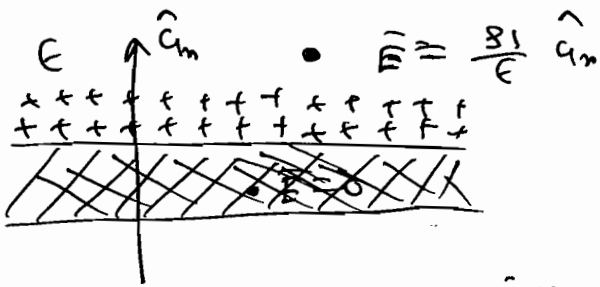
⇒ We assume that the interface has a non-zero surface charge density of  $\rho_s \text{ C/m}^2$ . By using Gauss Law we can show that normal components of Electric flux densities are equal to surface charge density. By expression

$$D_n = \rho_s \quad (\text{or})$$

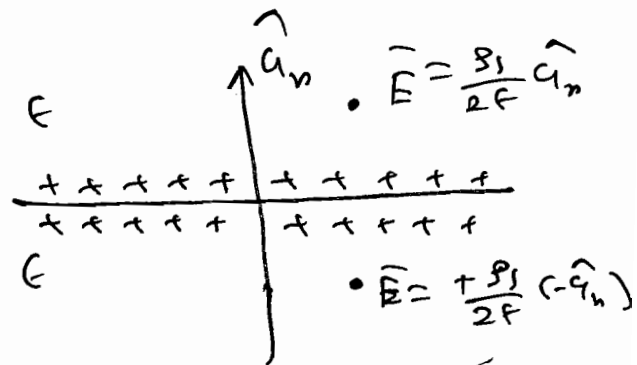
$$\bar{D} = \rho_s \hat{a}_n \quad \text{and}$$

$$\therefore \bar{E} = \frac{\rho_s}{\epsilon} \hat{a}_n$$

Imp  
\*



→ The entire charge lies on the top of the conductor surface.



→ The charge is distributed on both sides of conductor sheet.

Ex-1 A charge density of  $1 \text{ nC/m}^2$  is placed on a conductor surface. Assume interface is free space. Find the magnitude of the electric field.

Ans: 
$$\vec{E} = \frac{\rho_s}{\epsilon} \hat{a}_n = \frac{1 \times 10^{-9}}{36\pi \times 10^9} \hat{a}_n$$

$$\therefore |\vec{E}| = 36\pi \text{ V/m.}$$

Ex-2 A positive charge is distributed on a conductor surface. Assume the interface is free space. Given that  $\vec{D}$  at across interface is equal to  $\vec{D} = 2(\hat{a}_x + \sqrt{3}\hat{a}_y)$   $\text{nC/m}^2$ .

find the value of charge density across the interface.

Ans: 
$$\vec{E} = \frac{\rho_s}{\epsilon} \hat{a}_n$$

$$\therefore \vec{D} = \rho_s \hat{a}_n$$

$$\hat{a}_n = \frac{2\hat{a}_x + 2\sqrt{3}\hat{a}_y}{\sqrt{4+12}}$$

$$\hat{a}_n = \frac{\hat{a}_x}{2} + \frac{\sqrt{3}}{2}\hat{a}_y$$

$$\therefore |\vec{D}| = \rho_s$$

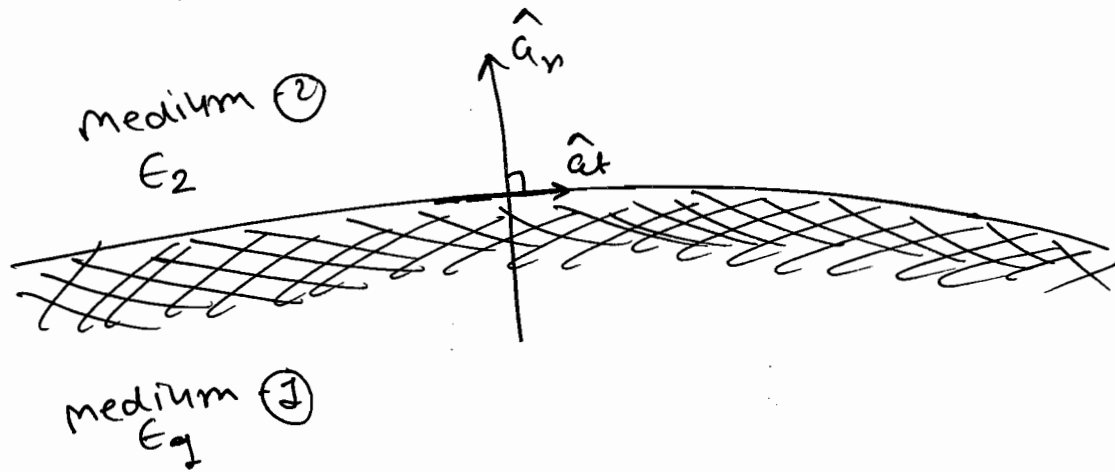
$$|\vec{D}| = \sqrt{2^2 + 2^2(3)} = 4$$

$$\therefore \vec{D} = 4 \left\{ \frac{2\hat{a}_x + 2\sqrt{3}\hat{a}_y}{4} \right\}$$

$$\vec{D} = \rho_s \hat{a}_n$$

$$\therefore \rho_s = 4 \text{ nC/m}^2$$

Case-2: Dielectric to Dielectric interface:



- $\hat{a}_n$ : Normal unit vector directed in from ① to ②
- $\hat{a}_t$ : Tangential unit vector tangential to the interface.

We can show that

$$\boxed{(1) E_{t1} = E_{t2}}$$

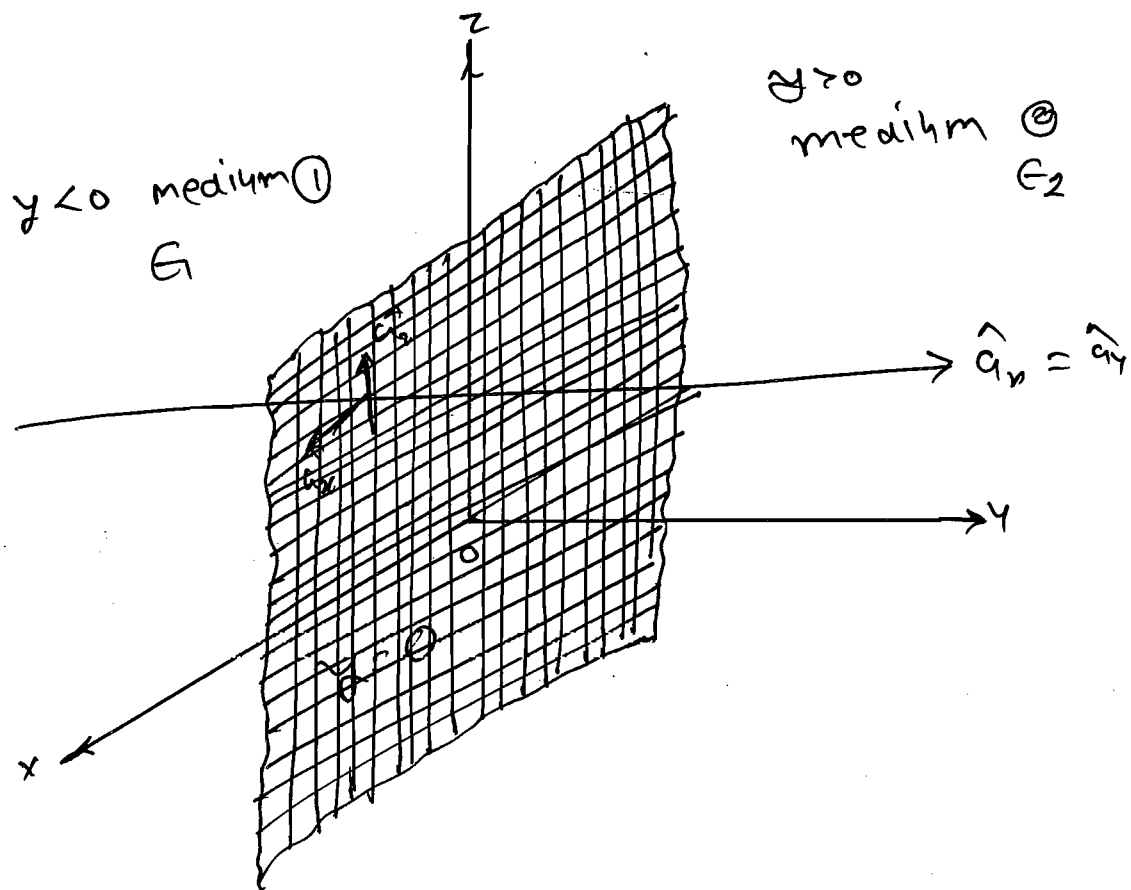
Tangential components of E-fields are continuous across a dielectric to dielectric interface.

$$(2) (a) \boxed{D_{n2} - D_{n1} = \rho_s}$$

→ The normal components of electric flux densities are discontinuous by an amount of surface charge density.

(b) if  $\rho_s = 0$  (charge free interface).

→ The normal components of electric flux densities are continuous across a charge free interface.



→ figure shows that interface is defined by  $y=0$ . Medium -1 is defined for  $y < 0$  and is characterised by  $\epsilon_1$ .

→ Medium -2 is defined for  $y > 0$  and is characterised by  $\epsilon_2$ . To this interface the normal unit vector is  $\hat{n} = \hat{a}_y$  and the unit vectors tangential to interface are  $\hat{a}_x$  and  $\hat{a}_z$ .

Ex-1  
 → With reference to the figure shown above let,  $\epsilon_1 = 2\epsilon_0$ ,  $\epsilon_2 = 3\epsilon_0$  and given that

$$\vec{E}_1 = (4\hat{a}_x + 5\hat{a}_y + 6\hat{a}_z) \text{ V/m.}$$

Find  $\bar{D}_1$ ,  $\bar{D}_2$  and  $E_2$ . and assume that the interface is charge free: (i.e)  $S_f = 0$  across  $z=0$ .

Ans:  $\bar{E}_1 = \underbrace{4\hat{a}_x + 6\hat{a}_z}_{E_{t1}} + \underbrace{5\hat{a}_y}_{E_{n1}}$

$$\therefore \bar{E}_1 = E_{t1}\hat{a}_t + E_{n1}\hat{a}_n$$

→ (i.e) Any field vector across the interface can be represented as a vectorial sum of tangential and normal components.

$$\bar{E}_1 = 4\hat{a}_x + 6\hat{a}_z + 5\hat{a}_y$$

$$\bar{D}_1 = \bar{E}_1 \epsilon_1$$

$$\therefore \bar{D}_1 = 4\epsilon_1\hat{a}_x + 6\epsilon_1\hat{a}_z + 5\epsilon_1\hat{a}_y$$

$$E_{t1} = E_{t2}$$

$$\therefore \bar{E}_2 = 4\hat{a}_x + 6\hat{a}_z + E_{y2}\hat{a}_y$$

$$\therefore D_{n1} = D_{n2} \quad (\because S_f = 0)$$

$$\therefore \bar{D}_2 = D_{x2}\hat{a}_x + D_{z2}\hat{a}_z + 5\epsilon_2\hat{a}_y$$

$$\therefore \bar{D}_2 = \epsilon_2 \bar{E}_2$$

$$\therefore D_{x2}\hat{a}_x + D_{z2}\hat{a}_z + 5\epsilon_2\hat{a}_y = 4\epsilon_2\hat{a}_x + 6\epsilon_2\hat{a}_z + E_{y2}\epsilon_2\hat{a}_y$$

$$\therefore \left. \begin{array}{l} D_{x2} = 4\epsilon_2 \text{ C/m}^2 \\ D_{z2} = 6\epsilon_2 \text{ C/m}^2 \end{array} \right| E_{y2} = \frac{5\epsilon_2}{\epsilon_2} \text{ V/m}$$

Ex-2 Repeat the above problem if the interface has a non-zero surface charge density of  $\rho_s$  C/m<sup>2</sup>.

Ans:

$$\text{let, } \vec{D}_2 = D_{x2} \hat{a}_x + D_{z2} \hat{a}_z + D_{y2} \hat{a}_y$$

$$\therefore D_{n2} - D_{n1} = \rho_s$$

$$D_{y2} - 0 = \rho_s$$

$$\therefore D_{y2} = \rho_s + 5\epsilon_1$$

$$\therefore D_2 = D_{x2} \hat{a}_x + D_{z2} \hat{a}_z + (\rho_s + 5\epsilon_1) \hat{a}_y$$

$$\therefore D_2 = \epsilon_2 \vec{E}_2$$

$$\therefore D_{x2} = 4\epsilon_2 \text{ C/m}^2$$

$$D_{z2} = 6\epsilon_2 \text{ C/m}^2$$

$$\therefore E_{y2} = \frac{\rho_s + 5\epsilon_1}{\epsilon_2} \text{ V/m.}$$

Ex-3 Repeat above 2 example by assuming the interface at  $z=0$ .  $z < 0$  is medium 1 and is characterized by  $\epsilon_1$  whereas  $z > 0$  is medium 2 and is characterized by  $\epsilon_2$ .

Ans:

$$\vec{E} = \underbrace{4\hat{a}_x + 5\hat{a}_y}_{E_{\text{ref}}} + \underbrace{6\hat{a}_z}_{E_{\text{ref}}}$$

$$\therefore \vec{E} = \vec{E}_{n1} + \vec{E}_{t1}$$

$$\therefore \vec{E}_{\text{ref}} = 4\hat{a}_x + 5\hat{a}_y$$

$$\vec{E}_{\text{ref}} = \vec{E}_{n1} = 6\hat{a}_z$$

is directed in  $\hat{a}_z$  direction. unit vector  $\hat{a}_z$  is  
 $\hat{a}_z$  & unit vector tangential to interface  
 are  $\hat{a}_x$  and  $\hat{a}_y$ .

$$\vec{E}_{t2} = \vec{E}_{t1}$$

$$\therefore \vec{E}_{t2} = 4\hat{a}_x + 5\hat{a}_y$$

$$\therefore \vec{E}_2 = \vec{E}_{t2} + \vec{E}_{n2}$$

$$\therefore \vec{D}_{n2} = \vec{D}_{n1}$$

$$\therefore \epsilon_2 \vec{E}_{n2} = \epsilon_1 \vec{E}_{n1}$$

$$\therefore \vec{E}_{n2} = \frac{\epsilon_1}{\epsilon_2} \vec{E}_{n1}$$

$$\therefore \vec{E}_{n2} = \frac{2}{3} \times 6\hat{a}_z = 4\hat{a}_z$$

$$\therefore \vec{E}_2 = 4\hat{a}_x + 5\hat{a}_y + 4\hat{a}_z$$

$$\therefore \vec{D}_1 = \epsilon_1 \vec{E}_1$$

$$\vec{D}_1 = \epsilon_0 (8\hat{a}_x + 10\hat{a}_y + 12\hat{a}_z)$$

$$\therefore \vec{D}_2 = \epsilon_2 \vec{E}_2$$

$$\vec{D}_2 = \epsilon_0 [12\hat{a}_x + 15\hat{a}_y + 12\hat{a}_z]$$

Now, these are normal components of  $\vec{D}$  that are discontinuous by surface charge density  $\rho_s$  C/m<sup>2</sup>.

$$\therefore D_{n2} - D_{n1} = \rho_s \text{ C/m}^2$$

$$\therefore \epsilon_2 E_{n2} - \epsilon_1 E_{n1} = \rho_s$$

$$\epsilon_2 E_{n2} = \epsilon_1 E_{n1} + \beta_1$$

$$E_{n2} = \frac{\epsilon_1 E_{n1} + \beta_1}{\epsilon_2}$$

$$E_{n2} = \frac{6\epsilon_1 + \beta_1}{\epsilon_2}$$

$$\vec{E}_2 = 4\hat{a}_x + 5\hat{a}_y + \left(\frac{6\epsilon_1 + \beta_1}{\epsilon_2}\right)\hat{a}_z$$

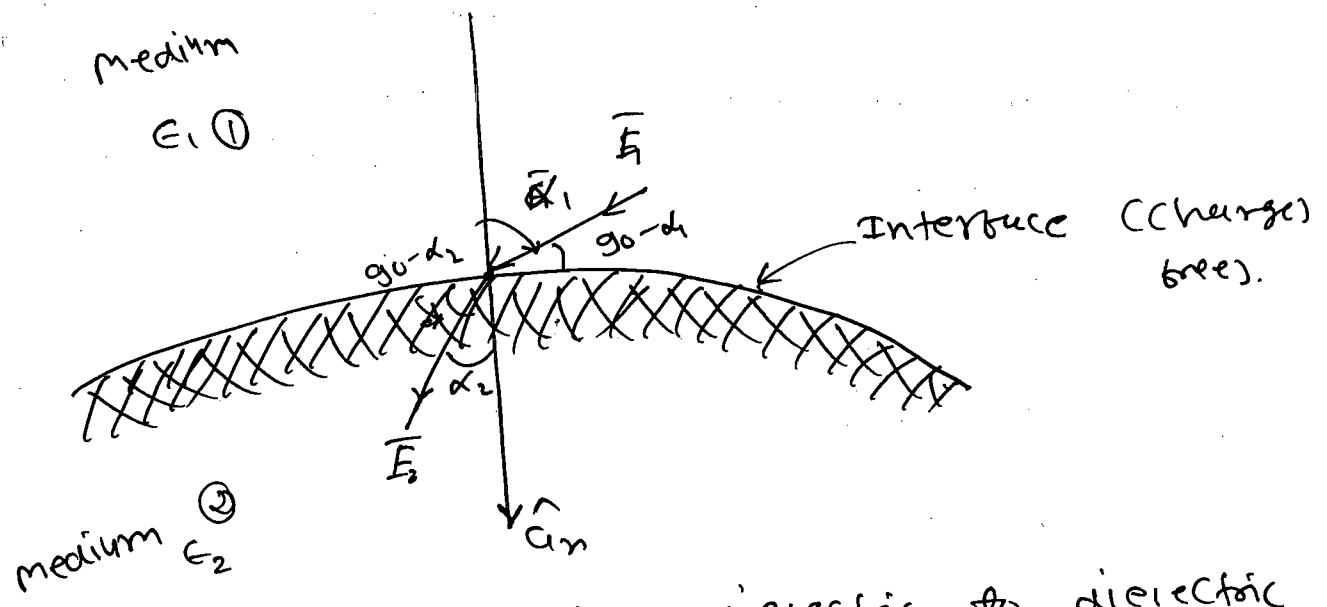
$$\vec{D}_2 = 4\epsilon_2\hat{a}_x + 5\epsilon_2\hat{a}_y + (6\epsilon_1 + \beta_1)\hat{a}_z$$

$$\vec{D}_1 = \epsilon_1 \vec{E}_1$$

$$\vec{D}_1 = \epsilon_0 (8\hat{a}_x + 10\hat{a}_y + 12\hat{a}_z)$$



Ex 3



→ Fig. Shows charge free dielectric to dielectric interface. Further it is shown normal unit vector directed in from medium ① to medium ② of P. Relate an expression  $\alpha_1, \alpha_2, \epsilon_1, \epsilon_2$ .

Ans::

$$|\vec{E}_{t1}| = |\vec{E}_{t2}|$$

$$\therefore E_2 \cos(90 - \alpha_2) = E_1 \cos(90 - \alpha_1)$$

$$\therefore E_2 \sin \alpha_2 = E_1 \sin \alpha_1$$

$$\therefore \epsilon_1 |\vec{E}_{n1}| = \epsilon_2 |\vec{E}_{n2}|$$

$$\therefore \frac{E_1 \cos \alpha_1}{\sin \alpha_1} = \frac{E_2 \cos \alpha_2}{\sin \alpha_2}$$

$$\boxed{\epsilon_1 \tan \alpha_1 = \epsilon_2 \tan \alpha_2}$$

$$D_{n1} - D_{n2} = \rho_s$$

But  $\rho_s = 0$

$$D_{n1} = D_{n2}$$

$$\therefore \epsilon_1 |\vec{E}_1| \cos \alpha_1 = \epsilon_2 |\vec{E}_2| \cos \alpha_2$$

$$\therefore \frac{\tan \alpha_1}{\epsilon_1} = \frac{\tan \alpha_2}{\epsilon_2}$$

$$\boxed{\frac{\tan \alpha_1}{\tan \alpha_2} = \frac{\epsilon_1}{\epsilon_2}}$$

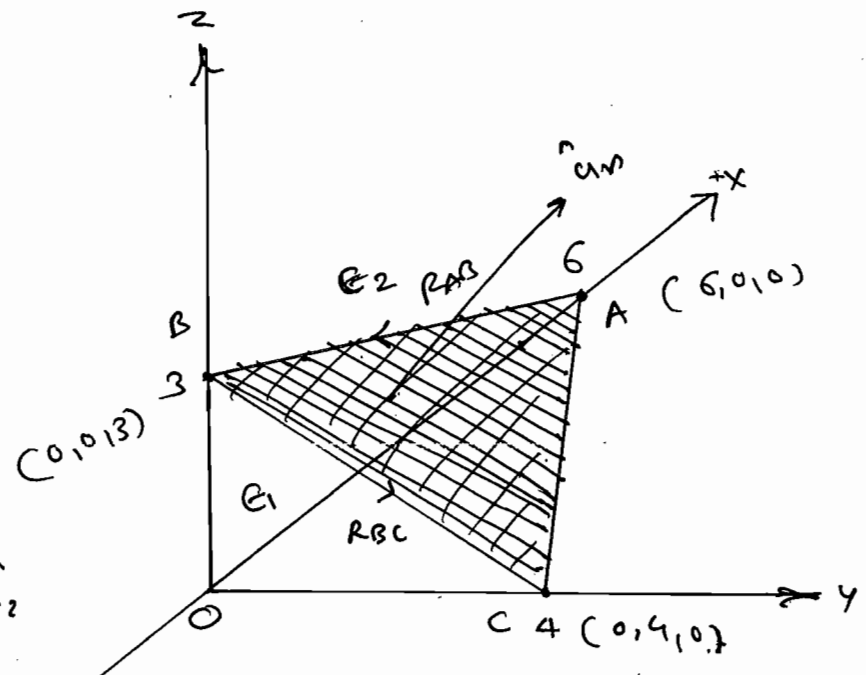
Ex-1 An interface is defined by  $2x + 3y + 4z = 12$ .  
 origin side of the interface is medium (1) and is characterised by  $\epsilon_1 = 2\epsilon_0$ . Other side of the interface is medium (2) and is characterised by free space. Let, the electric field in the medium (2) is given by  $\vec{E}_1 = 5\hat{a}_x + 6\hat{a}_y + 7\hat{a}_z$  V/m. Assume charge free interface. Find  $\vec{D}_1$ ,  $\vec{E}_2$ ,  $\vec{D}_2$ .

Ans:  $2x + 3y + 4z = 12$   
 $\therefore \frac{x}{6} + \frac{y}{4} + \frac{z}{3} = 1$

$\vec{r}_{AB} \times \vec{r}_{BC}$

$\vec{r}_{AB} = -6\hat{a}_x + 3\hat{a}_z$   
 $\vec{r}_{BC} = 4\hat{a}_y - 3\hat{a}_z$

$\vec{r}_{AB} \times \vec{r}_{BC}$   
 $= \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ -6 & 0 & 3 \\ 0 & 4 & -3 \end{vmatrix}$   
 $= -12\hat{a}_x - 18\hat{a}_y - 24\hat{a}_z$   
 $\hat{a}_n = -3[4\hat{a}_x + 6\hat{a}_y + 8\hat{a}_z]$   
 $\vec{r}_n = -6(2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z)$



$\hat{a}_n = \frac{-6(2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z)}{36.31}$       $\hat{a}_n = \frac{2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z}{\sqrt{2^2 + 3^2 + 4^2}}$   
 $\therefore \hat{a}_n = -\frac{(2\hat{a}_x + 3\hat{a}_y + 4\hat{a}_z)}{5.385}$

$$\rightarrow \vec{E}_1 = E_{n1} \hat{a}_n + E_{t2} \hat{a}_t$$

$$\vec{E}_2 = E_{n2} \hat{a}_n + E_{t2} \hat{a}_t$$

$$\rightarrow \vec{E}_1 \cdot \hat{a}_n = E_{n1} \hat{a}_n \cdot \hat{a}_n + E_{t2} \hat{a}_t \cdot \hat{a}_n$$

$$\boxed{E_{n1} = \vec{E}_1 \cdot \hat{a}_n} \rightarrow (1)$$

$$\boxed{\vec{E}_{n1} = E_{n1} \hat{a}_n} \rightarrow (2)$$

$$\boxed{\vec{E}_{t2} = \vec{E} - \vec{E}_{n1}} \rightarrow (3)$$

∴ NOW, tangential components are continuous.

So,  $\vec{E}_{t1} = \vec{E}_{t2}$

$$\boxed{\vec{E}_{t2} = \vec{E}_{t1}} \rightarrow (4)$$

∴ NOW,  $D_{n1} = \epsilon_1 E_{n1}$

$$\therefore \vec{E}_{n2} = \frac{\vec{D}_{n2}}{\epsilon_2} =$$

normal components at  $\bar{0}$  are continuous  
∵ charge free  
so  $\rho_s = 0$ .

$$\boxed{\vec{D}_{n1} = \vec{D}_{n2}} \rightarrow (5)$$

$$\vec{D}_{n1} = \epsilon_1 \vec{E}_{n1}$$

$$\boxed{\vec{D}_{n2} = \epsilon_1 \vec{E}_{n1}} \rightarrow (6)$$

$$\vec{E}_{n2} = \frac{\vec{D}_{n2}}{\epsilon_2} = \frac{\epsilon_1}{\epsilon_2} \vec{E}_{n1}$$

$$\boxed{\vec{E}_{n2} = \frac{\epsilon_1}{\epsilon_2} \vec{E}_{n1}} \rightarrow (7)$$

$$\text{So, } \boxed{\bar{E}_2 = \bar{E}_{t2} + \bar{E}_{n2}} \rightarrow \textcircled{8}$$

$$\therefore \bar{D}_1 = \bar{D}_{n1} + \bar{D}_{t1}$$

$$\boxed{\bar{D}_1 = \epsilon_1 \bar{E}_1} \rightarrow \textcircled{10}$$

$$\boxed{\bar{D}_2 = \epsilon_2 \bar{E}_2} \rightarrow \textcircled{9}$$

$$\rightarrow \bar{E}_1 = 5\hat{a}_x + 6\hat{a}_y + 7\hat{a}_z$$

$$\therefore \hat{a}_m = \frac{5\hat{a}_x + 6\hat{a}_y + 7\hat{a}_z}{10.49}$$

$$\hat{a}_m \cdot \bar{E}_1 = E_{n1} \hat{a}_m$$

$$\Rightarrow E_{n1} = \bar{E}_1 \cdot \hat{a}_m$$

$$\therefore E_{n1} = \frac{25 + 36 + 49}{10.49}$$

$$\boxed{E_{n1} = 10.49}$$

$$\therefore \bar{E}_{n1} = E_{n1} \hat{a}_m$$

$$\therefore \bar{E}_{n1} = 5\hat{a}_x + 6\hat{a}_y + 7\hat{a}_z$$

$$\therefore \bar{E}_{t1} = 0$$

$$\therefore \bar{E}_{t2} = 0$$

$$\therefore \bar{D}_{n1} = \bar{D}_{t2}$$

$$\therefore \epsilon_2 \bar{E}_{n2} = \epsilon_1 \bar{E}_{n1}$$

$$\therefore \bar{E}_{n2} = \frac{\epsilon_1}{\epsilon_2} (5\hat{a}_x + 6\hat{a}_y + 7\hat{a}_z)$$

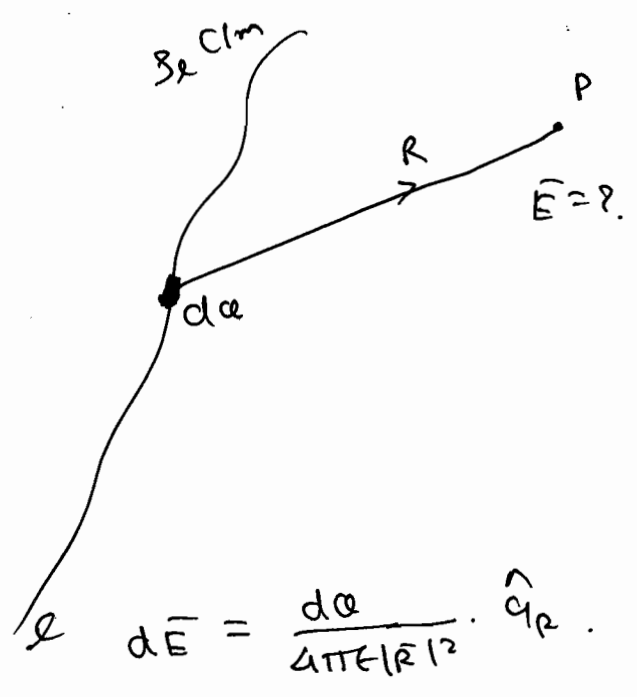
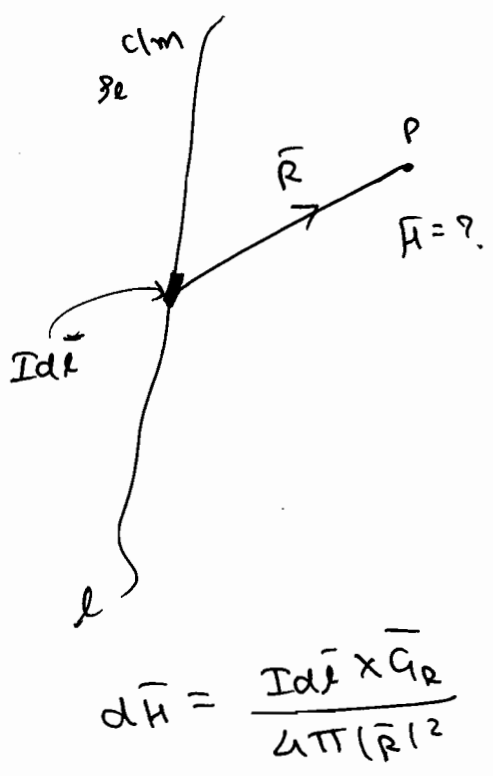
$$\therefore \bar{E}_{n2} = \frac{10}{3} \hat{a}_x + 4\hat{a}_y + \frac{14}{3} \hat{a}_z$$

$$\therefore \bar{E}_2 = \bar{E}_{n2} + \bar{E}_{t2}$$

$$\therefore \bar{E}_2 = \frac{10}{3} \hat{a}_x + 4\hat{a}_y + \frac{14}{3} \hat{a}_z$$

# Magnetic Fields (Steady)

Fields R Independent of time.



## Current Element = $I d\vec{l}$

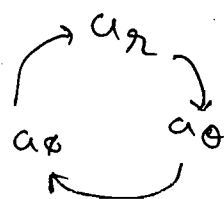
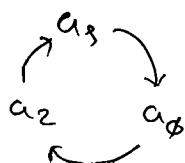
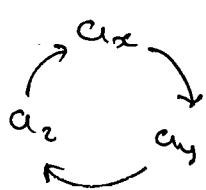
- Current multiplied vector dist. length
- This is vector quantity.
- Source of magnetic field.

- There exists a similarity bet<sup>n</sup> electric and magnetic fields.
- Both fields are proportional to the corresponding sources.
- Both fields are inversely proportional to square of distance from their corresponding sources.

→ Both fields are vector fields.

⇒ Bio Savart's Law:

$$\vec{H} = \int \frac{I d\vec{l} \times \hat{r}}{4\pi |\vec{r}|^2} \quad \text{A/m.}$$



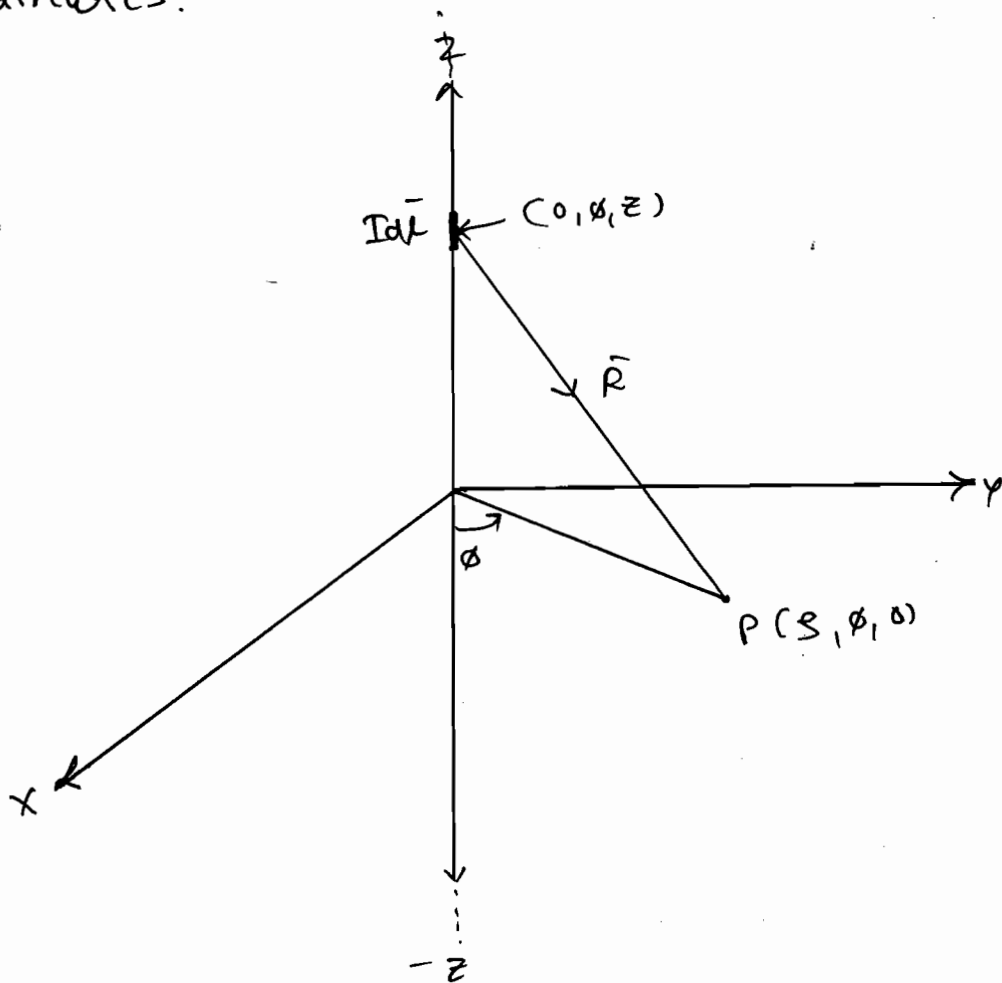
Ex-1 Find an expression for the magnetic field intensity due to a long straight infinite filamentary conductor which carries a direct current of  $I$  A. Show that the magnitude of the  $\vec{H}$  magnetic field intensity is inversely proportional to the distance between infinite current filament and the observation point.

Ans: We assume that the infinite current filament lies along  $z$  axis and is extending from  $-\infty$  to  $+\infty$ . We find the magnetic field intensity at some

Point on the x-y plane.

→ Say at a point  $P(s, \phi, 0)$ .

for the convenience we circular cylindrical co-ordinates.



→  $d\vec{l} = dz \hat{a}_z$

∴  $I d\vec{l} = I dz \hat{a}_z$

→  $\vec{R} = s \hat{a}_s - z \hat{a}_z$        $\hat{a}_R = \frac{s \hat{a}_s - z \hat{a}_z}{\sqrt{s^2 + z^2}}$

∴  $I d\vec{l} \times \hat{a}_R = \frac{I s dz}{\sqrt{s^2 + z^2}} \cdot \hat{a}_\phi$

so,  $d\vec{H} = \frac{I d\vec{l} \times \hat{a}_R}{4\pi |\vec{R}|^2}$

$$d\vec{H} = \frac{I dz \hat{a}_\phi}{4\pi (s^2 + z^2)^{3/2}} \cdot \hat{a}_\phi$$

$$\therefore \vec{H} = \frac{I}{4\pi} \int_{-\infty}^{\infty} \frac{s}{(s^2 + z^2)^{3/2}} dz \cdot \hat{a}_\phi$$

Now, let  $z = s \tan \theta$

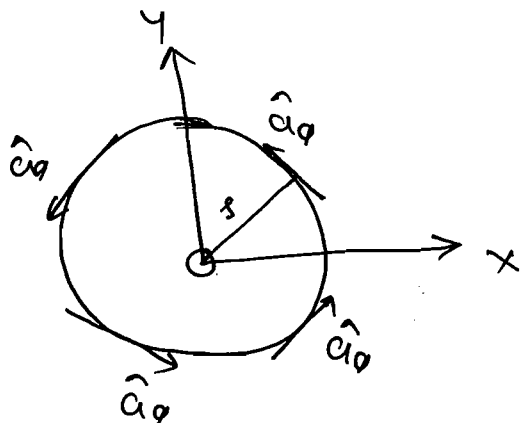
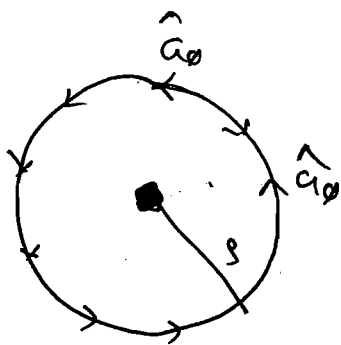
$$\therefore dz = s \sec^2 \theta$$

$$z \in (-\infty, \infty) \Rightarrow (-\pi/2, \pi/2)$$

$$\vec{H} = \frac{I}{4\pi} \int_{-\pi/2}^{\pi/2} \frac{s^2 \sec^2 \theta}{s^3 \sec^3 \theta} \cdot d\theta \cdot \hat{a}_\phi$$

$$\therefore \boxed{\vec{H} = \frac{I}{2\pi s} \cdot \hat{a}_\phi}$$

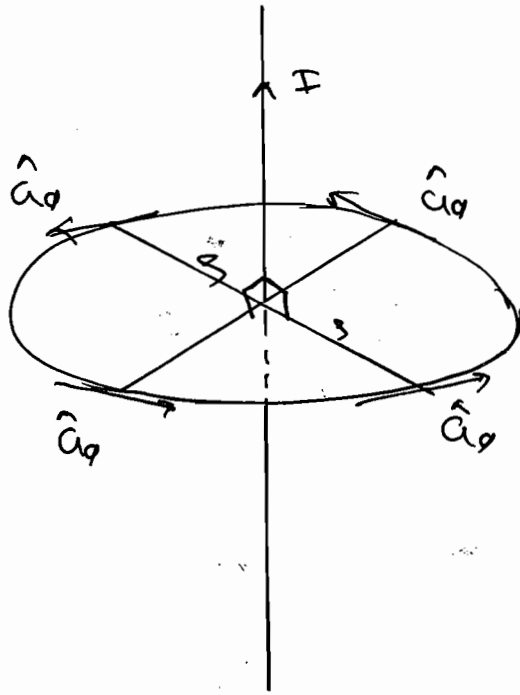
$$\therefore \boxed{|\vec{H}| \propto \frac{1}{s}}$$



→ Magnitude of magnetic field intensity is inversely proportional to the distance bet<sup>n</sup> the infinite current filament and the observation point. The direction of the magnetic field is around the conductor.

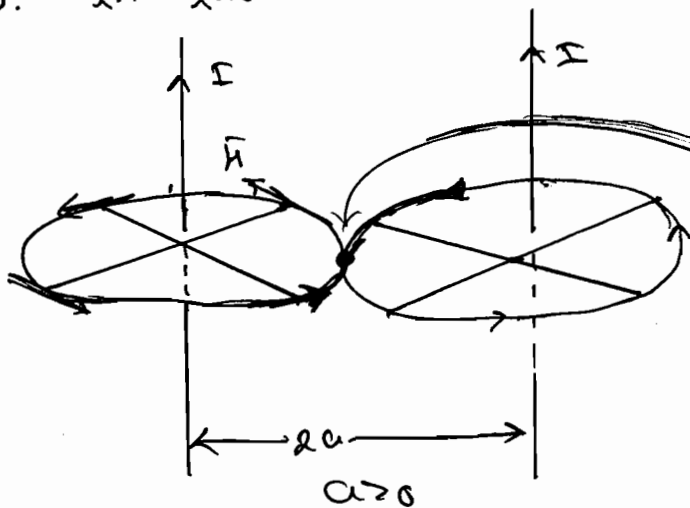


it encircles the conductor.



⇒ Two infinite current filaments are parallel: Case-1: currents are in same direction:

→ They are separated by  $2a$  m. ( $a > 0$ ) - They carry equal current of  $I$  amp. In same direction. find the magnitude of the ~~at the middle point~~ magnetic field intensity at the middle point bet<sup>n</sup> this two infinite current filaments. Assume that this conductor's carry equal currents of  $I$  amps. in the same direction.

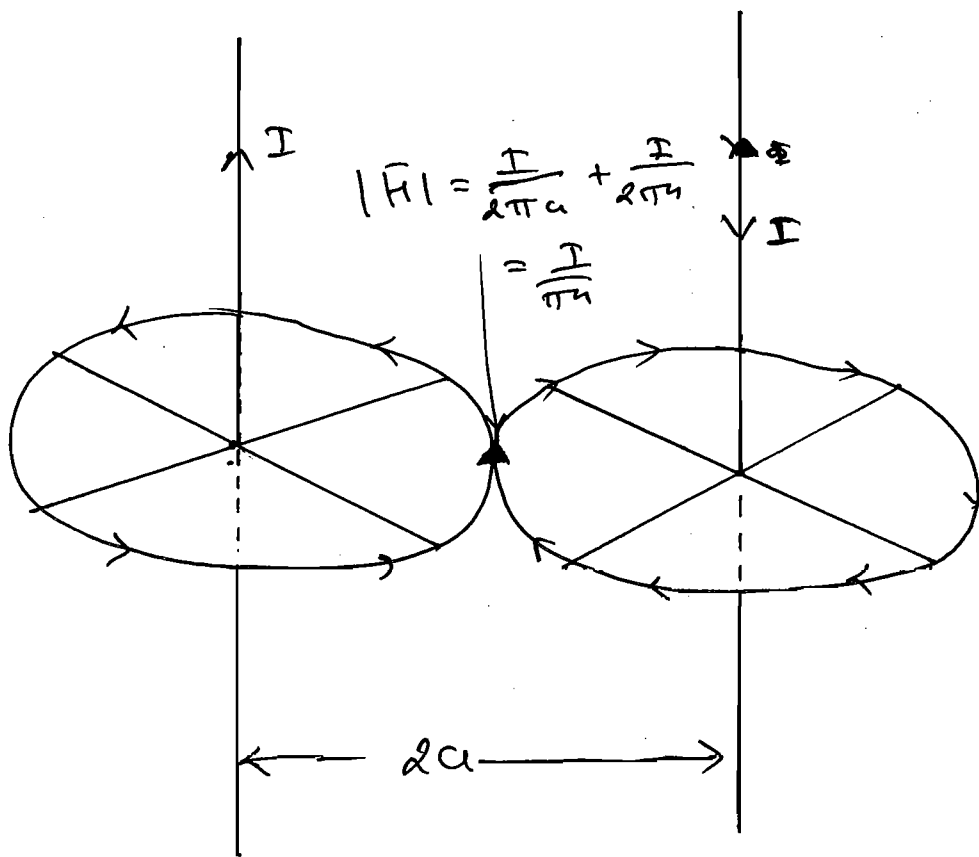


$H = 0$

The fields add in out of phase

∴  $|H| = 0$

Case-2: Currents are in opposite direction.



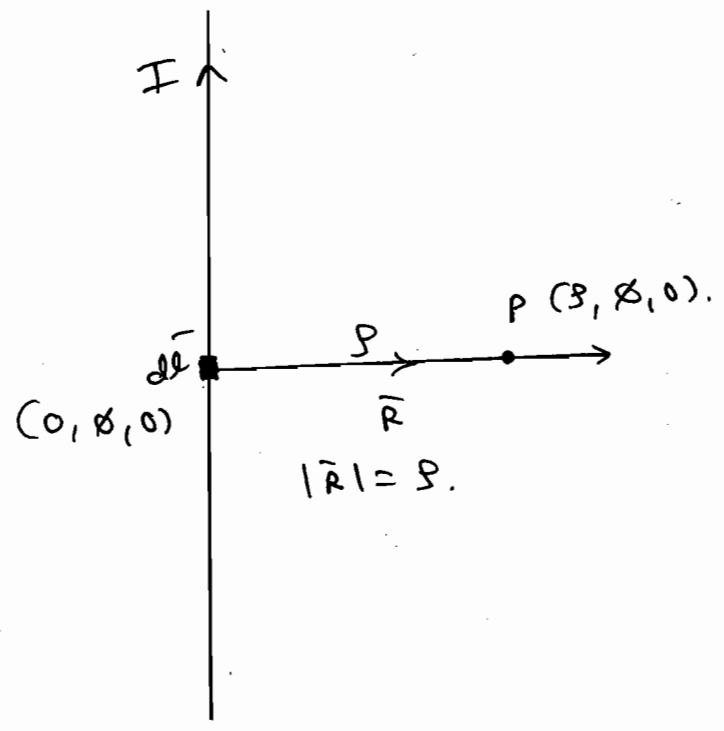
$$|\vec{H}| = \frac{I}{2\pi a} + \frac{I}{2\pi a}$$
$$= \frac{I}{\pi a}$$

$$\rightarrow |\vec{H}| = \frac{I}{2\pi a} + \frac{I}{2\pi a} = \frac{I}{\pi a}$$

The fields are added in phase.

\* General Expression for the Magnetic Field Intensity due to an infinite current filament.

⇒



→  $dl = dz \hat{a}_z$   
 $\therefore \vec{R} = \beta \hat{a}_\beta$   
 $\hat{a}_R = \hat{a}_\beta$

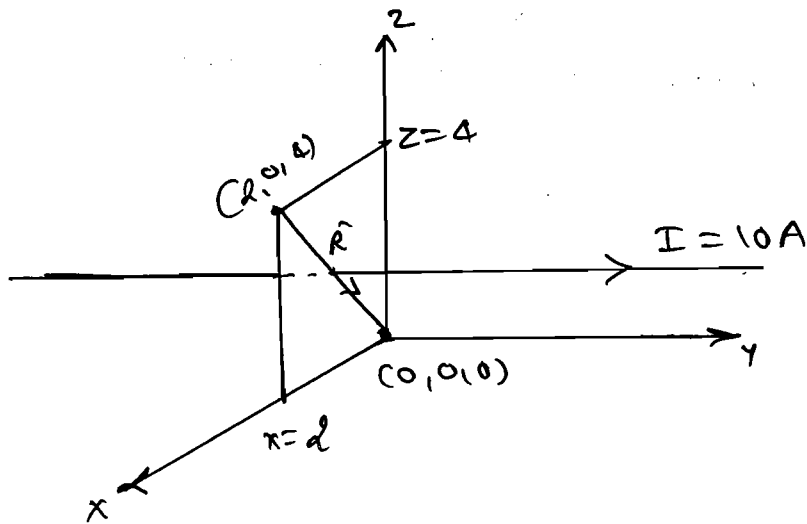
$\therefore dl \times \hat{a}_R = \hat{a}_\phi dz$   
 The unit vector of  $dl \times \hat{a}_R = \hat{a}_\phi$

→  $\vec{H} = \frac{I}{2\pi |\vec{R}|}$  Unit vector of  $(dl \times \hat{a}_R)$ .

Short-cut formula.

Ex 1 → An infinite current filament is lies at  $x=2, y=2, z=4m$  it carries a current of  $10A$  along +ve  $z$  direction. Find  $H$  at the origin?

Ans:



$$\Rightarrow \vec{R} = -2\hat{a}_x - 4\hat{a}_z, \quad d\vec{l} = dy\hat{a}_y$$
$$|\vec{R}| = \frac{-2\hat{a}_x - 4\hat{a}_z}{\sqrt{20}} \cdot \sqrt{20}$$

$$\therefore \hat{a}_R = \frac{-2\hat{a}_x - 4\hat{a}_z}{\sqrt{20}}, \quad d\vec{l} = dy\hat{a}_y$$

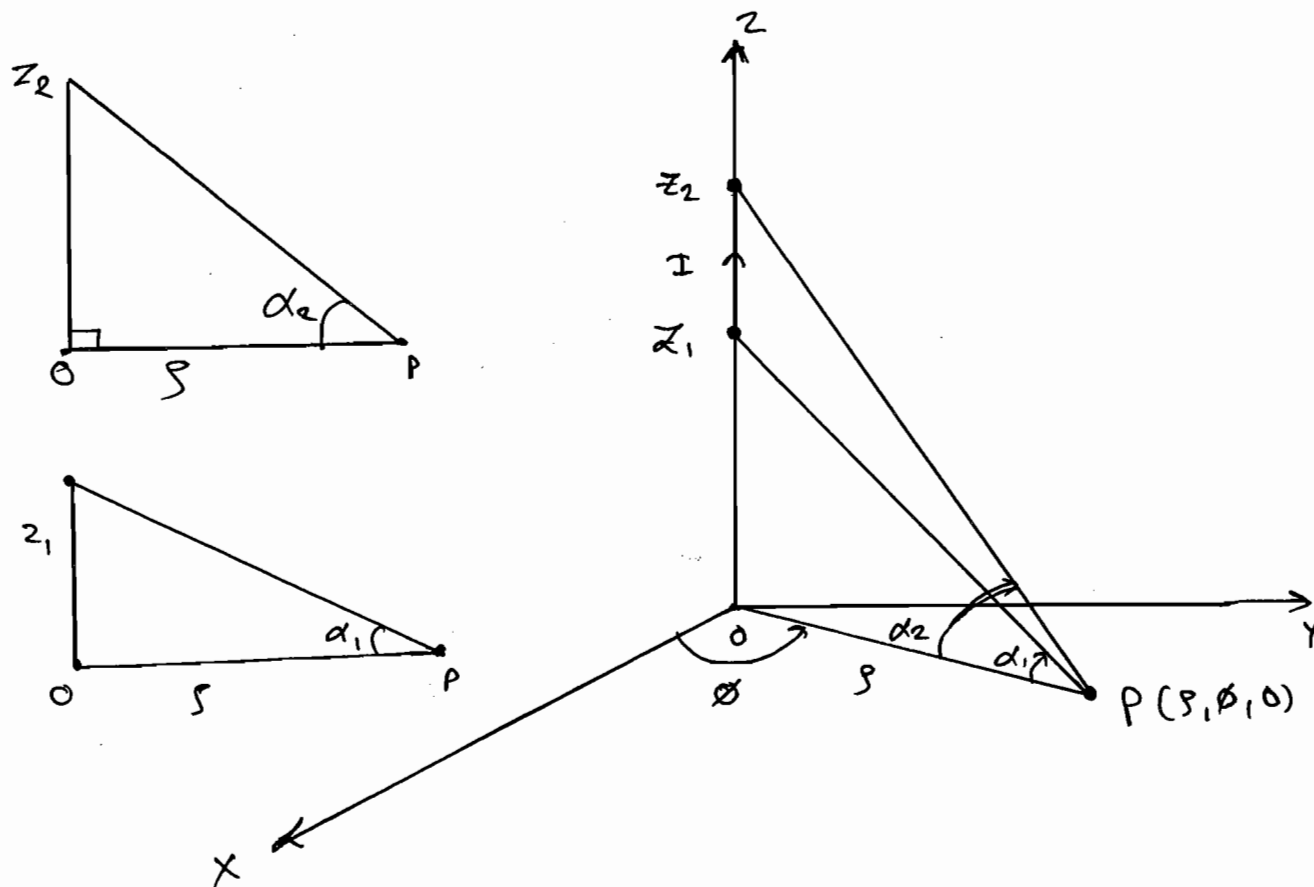
$$\therefore d\vec{l} \times \hat{a}_R = \frac{2\hat{a}_z - 4\hat{a}_x}{\sqrt{20}} dy$$

$$\text{Unit vector of } (d\vec{l} \times \hat{a}_R) = \frac{2\hat{a}_z - 4\hat{a}_x}{\sqrt{20}}$$

$$\therefore H = \frac{I}{2\pi\sqrt{20}} \cdot \frac{2\hat{a}_z - 4\hat{a}_x}{\sqrt{20}}$$

$$\therefore \boxed{H = \frac{I ( \hat{a}_z - 2\hat{a}_x )}{20\pi} \text{ Alm.}}$$

\*



→ Figure shows a finite length current filament lies along  $z$ -axis. It carries a current of  $I$  A.

→ find the magnetic field intensity at  $P(s, 0, 0)$  in terms of  $\alpha_1$  &  $\alpha_2$ .

→ We know that for infinitesimal

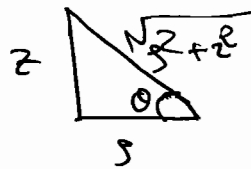
$$d\vec{H} = \frac{I ds dz}{4\pi (s^2 + z^2)^{3/2}} \cdot \hat{a}_\phi$$

∴ Now, for finite length ( $z_1$  to  $z_2$ ).

$$\therefore \vec{H} = \int_{z_1}^{z_2} \frac{I ds dz}{4\pi (s^2 + z^2)^{3/2}} \hat{a}_\phi$$

$$\therefore \vec{H} = \frac{I}{4\pi} \hat{a}_\phi \int_{z_1}^{z_2} \frac{s dz}{(s^2 + z^2)}$$

Put  $z = \rho \tan \theta$   
 $\therefore dz = \rho \sec^2 \theta$



$$\therefore \bar{H} = \frac{I}{4\pi\rho} \int_{z_1}^{z_2} \frac{\rho^2 \sec^2 \theta \cdot d\theta}{\rho^3 \sec^3 \theta} \hat{a}_\phi$$

$$\sin \theta = \frac{z}{\sqrt{z^2 + \rho^2}}$$

$$\cos \theta = \frac{\rho}{\sqrt{z^2 + \rho^2}}$$

$$\bar{H} = \frac{I}{4\pi\rho} \cdot [\sin \theta]_{z_1}^{z_2}$$

$$\bar{H} = \frac{I}{4\pi\rho} \left[ \frac{z}{(z^2 + \rho^2)^{1/2}} \right]_{z_1}^{z_2} \hat{a}_\phi$$

$$\bar{H} = \frac{I}{4\pi\rho} \left[ \frac{z_2}{(z_2^2 + \rho^2)^{1/2}} - \frac{z_1}{\sqrt{z_1^2 + \rho^2}} \right] \hat{a}_\phi$$

$$\therefore \bar{H} = \frac{I}{4\pi\rho} [\sin \alpha_2 - \sin \alpha_1] \hat{a}_\phi \quad \text{AIm.}$$

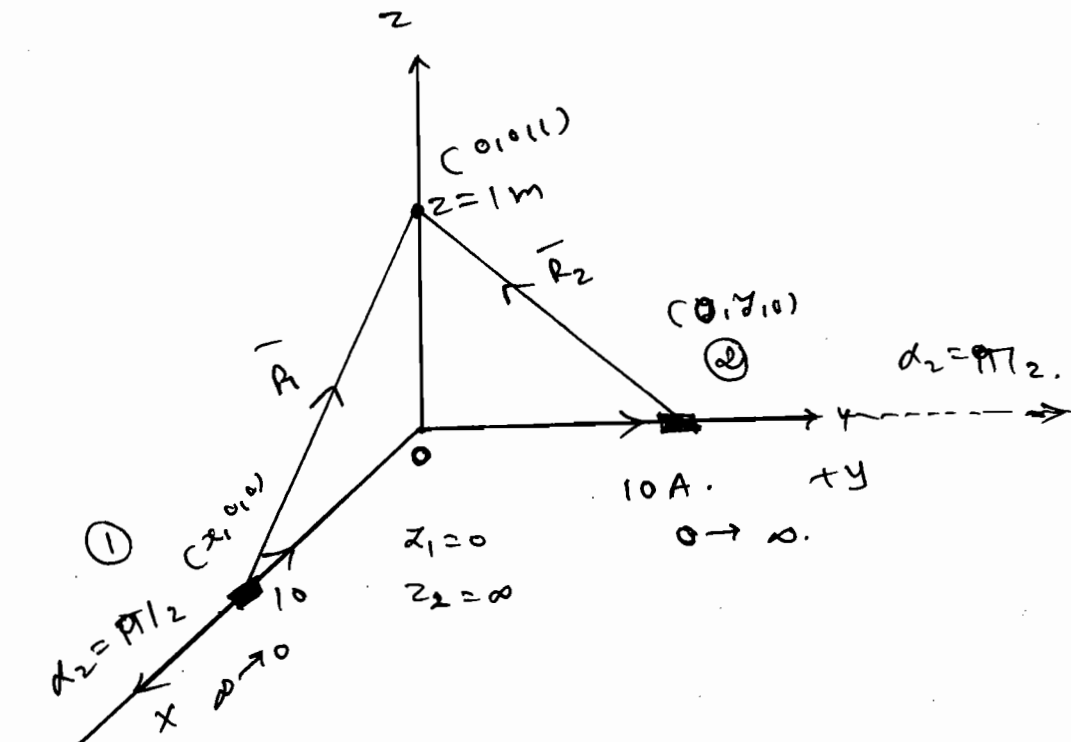
$$\rightarrow \text{If } z_2 \rightarrow \infty \Rightarrow \alpha_2 = \frac{\pi}{2} \Rightarrow \sin \frac{\pi}{2} = 1$$

$$\rightarrow \text{If } z_1 \rightarrow -\infty \Rightarrow \alpha_1 = -\frac{\pi}{2} \Rightarrow \sin \frac{\pi}{2} = -1$$

$$\therefore \bar{H} = \frac{I}{4\pi\rho} [1 - (-1)] \hat{a}_\phi$$

$$\therefore \bar{H} = \frac{I}{2\pi\rho} \hat{a}_\phi$$

\* A current of 10A is directed in from infinity towards origin on the positive x-axis and then and then map to  $\infty$  on the +ve y-axis find magnitude of magnetic field intensity on the z-axis. at  $z=1m$ .



$$\vec{H}_e = \frac{I d\vec{l} \times \hat{r}_e}{4\pi |\vec{R}|^3}$$

$$\vec{H} = \frac{I}{4\pi |\vec{R}|} \cdot \text{Unit vector of } (\hat{r}_e \times d\vec{l})$$

$$\textcircled{1} \quad d\vec{l}_1 = dx \hat{a}_x$$

$$\vec{R}_1 = -x \hat{a}_x + \hat{a}_z$$

$$|\vec{R}_1| = \sqrt{x^2 + 1}$$

$$\hat{r}_{R1} = \frac{-x \hat{a}_x + \hat{a}_z}{\sqrt{x^2 + 1}}$$

$$\hat{a}_{R1} \times d\vec{l}_1 = \frac{-dx}{\sqrt{x^2 + 1}} \hat{a}_y$$

$$\textcircled{2} \quad d\vec{l}_2 = dy \hat{a}_y$$

$$\vec{R}_2 = \frac{-y \hat{a}_y + \hat{a}_z}{\sqrt{1 + y^2}}$$

$$|\vec{R}_2| = \sqrt{1 + y^2}$$

$$\hat{r}_{R2} = \frac{-y \hat{a}_y + \hat{a}_z}{\sqrt{1 + y^2}}$$

$$\hat{a}_{R2} \times d\vec{l}_2 = \frac{dy}{\sqrt{1 + y^2}} \hat{a}_x$$

$$\therefore d\vec{H} = \frac{I dy}{4\pi (y^2+1)^{3/2}} \hat{a}_x - \frac{I dx}{4\pi (x^2+1)^{3/2}} \hat{a}_y.$$

$$\therefore \vec{H} = \frac{I}{4\pi} \left[ \int_0^\infty \hat{a}_x \frac{dy}{(y^2+1)^{3/2}} - \hat{a}_y \int_\infty^0 \frac{dx}{(x^2+1)^{3/2}} \right]$$

$$\therefore \vec{H} = \frac{I}{4\pi} [\hat{a}_x + \hat{a}_y].$$

$$\therefore \int_{-\infty}^{\infty} \frac{1}{\sqrt{x^2+1}} dx = 1$$

$$\int_0^\infty \frac{dy}{\sqrt{y^2+1}} = 1.$$

$$\boxed{\vec{H} = \frac{I}{4\pi} [\hat{a}_x + \hat{a}_y].}$$

Ex-2 Find the magnetic field intensity on the axis of a circular current loop of radius  $a$  which carries a direct current of  $I$ . Also find the magnetic field intensity at the center of the circular current loop.

→ we assume that the circular current loop is located in  $z=0$  plane and centered at origin. Therefore  $z$  axis would become axis of the circular current loop on the  $z$ .

$$\therefore I d\vec{l} = I a d\theta \hat{a}_\phi$$

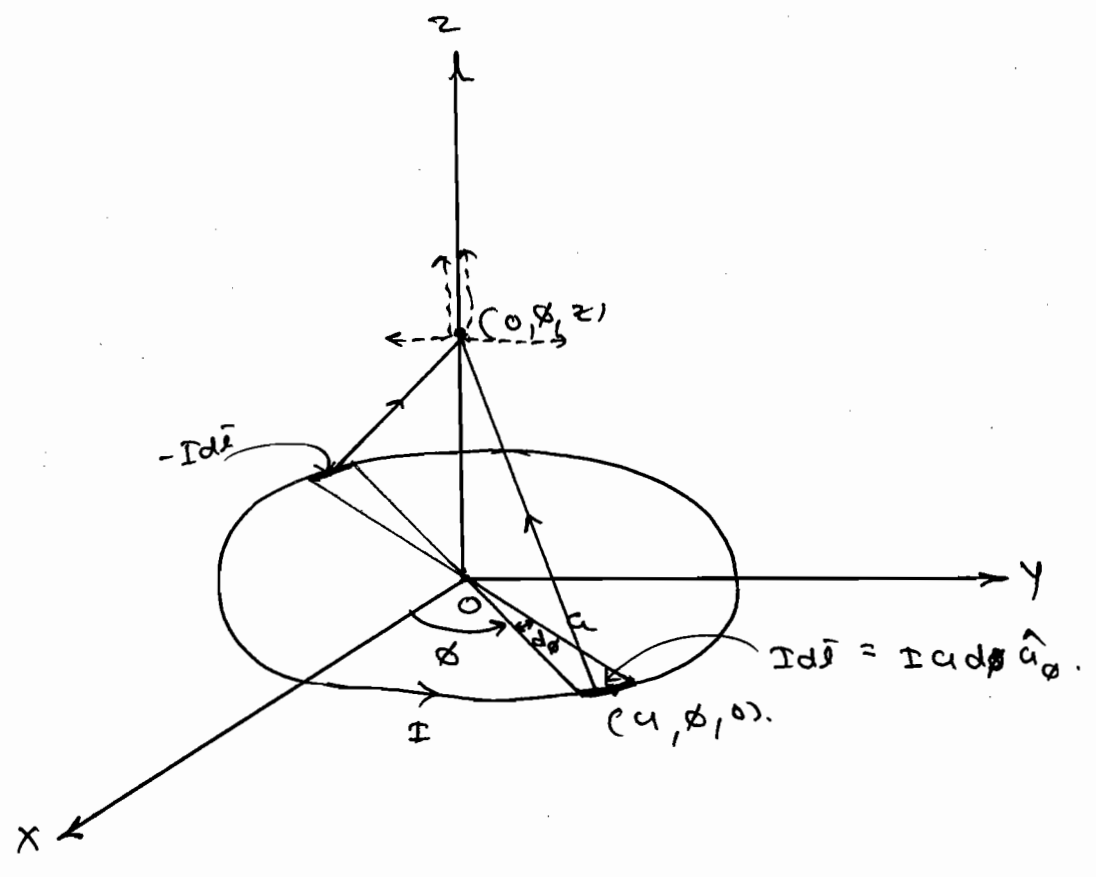
$$\vec{R} = -a \hat{a}_y + z \hat{a}_z$$

$$\hat{a}_R = \frac{-a \hat{a}_y + z \hat{a}_z}{\sqrt{a^2 + z^2}}$$

$$I d\vec{l} \times \hat{a}_R$$

$$= \frac{I a^2 d\theta \hat{a}_z + I a z d\theta \hat{a}_y}{\sqrt{a^2 + z^2}}$$





→ As shown in the figure for every differential current filament on the circular current loop, there exists an another differential current filament diametrically opposite side which results in cancellation of a horizontal field components and the resultant field would be along  $\hat{a}_z$  direction only.

→ Ignoring  $\hat{a}_z$  components the total field is given by

$$d\vec{H} = \frac{I d\vec{l} \times \hat{a}_r}{4\pi r^2}$$

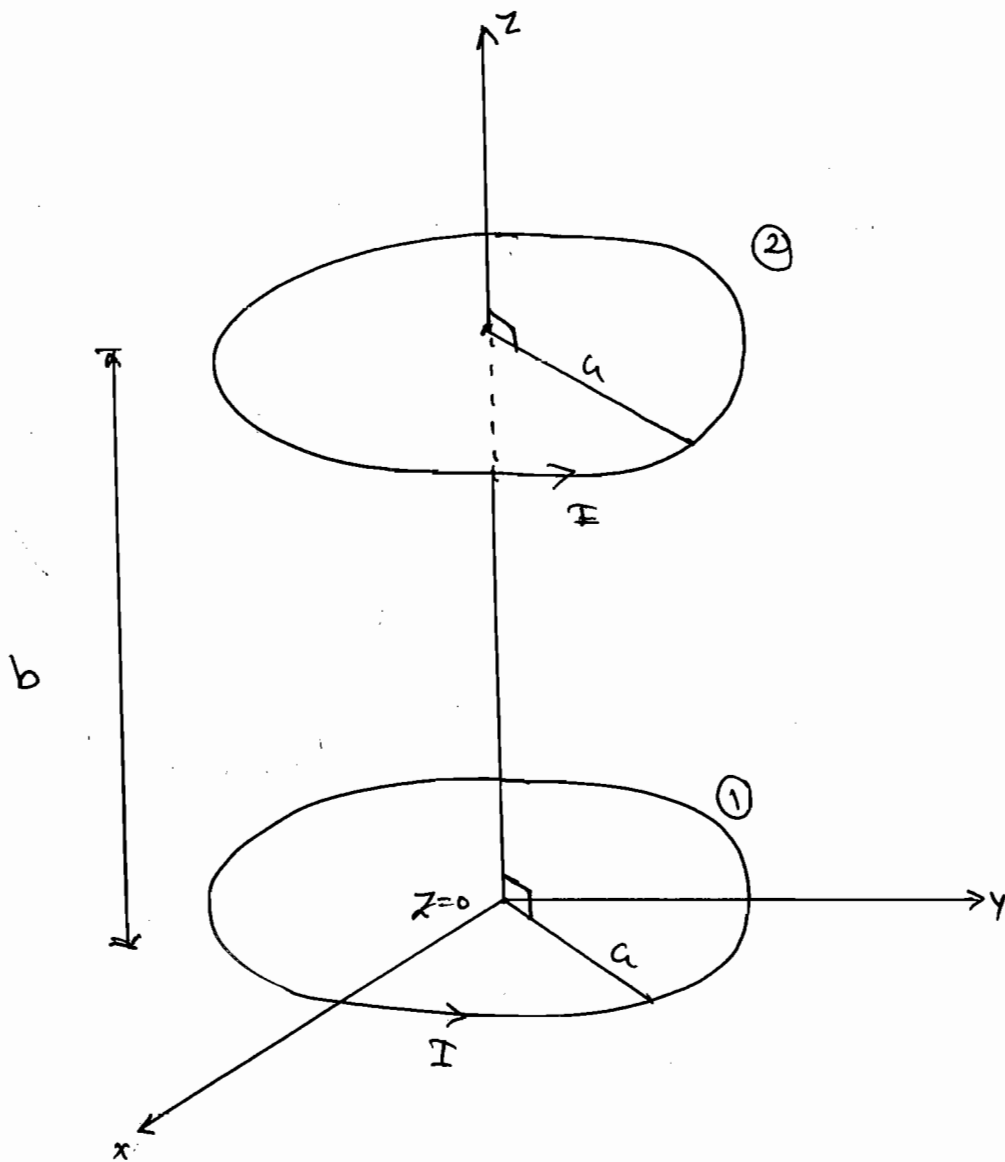
$$\therefore d\vec{H} = \frac{I a^2 \hat{a}_z + I a b \hat{a}_\phi}{4\pi (a^2 + b^2)^{3/2}}$$

$$\vec{H} = \frac{Ia^2}{4\pi (a^2 + b^2)^{3/2}} \int_0^{2\pi} d\theta.$$

$$\therefore \vec{H} = \frac{Ia^2}{2(a^2 + b^2)^{3/2}} \hat{C}_2 \text{ Alm.}$$

→ At the centre of the loop (put  $b=0$ ), the expression for magnetic field intensity is given by

$$\vec{H} = \frac{I}{2a} \hat{C}_2 \text{ Alm.}$$



→ Figure shows parallel circular current loops ① & ② find  $\vec{H}$  at  $z=b$  at the centre of loop ②.

$$\vec{H}_1 = \frac{Ia^2}{2(a^2+b^2)^{3/2}} \hat{a}_2$$

$$\vec{H}_2 = \frac{I}{2a} \hat{a}_2$$

$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

$$\vec{H} = \left( \frac{Ia^2}{2(a^2+b^2)^{3/2}} + \frac{I}{2a} \right) \hat{a}_2$$

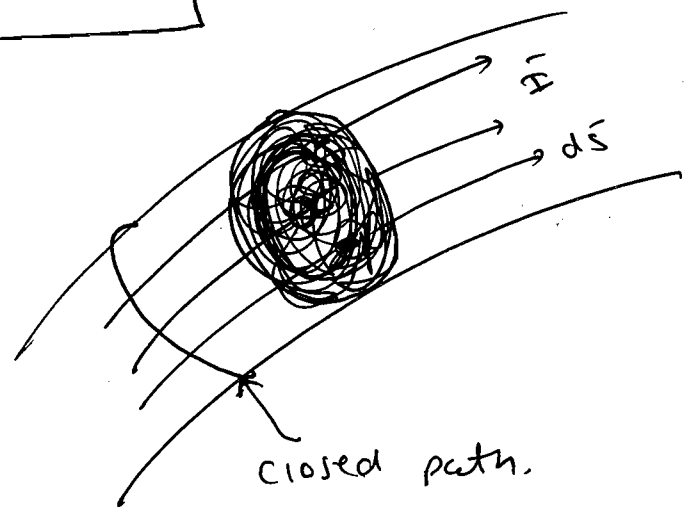
\* Ampere's Law:

→ The line Integral of Magnetic field Intensity around a closed path is equal to current enclosed by the path.

$$\oint_L \vec{H} \cdot d\vec{l} = I_{enc.}$$

$$\therefore I = \int_S \vec{J}_c \cdot d\vec{s}$$

$$\therefore \oint_L \vec{H} \cdot d\vec{l} = \int_S \vec{J}_c \cdot d\vec{s}$$



Now, By Stokes' theorem.

$$\therefore \oint_L \vec{H} \cdot d\vec{l} = \int_S (\nabla \times \vec{H}) \cdot d\vec{s} = \int_S \vec{J}_c \cdot d\vec{s}$$

$$\nabla \times \vec{H} = \vec{J}_c$$

point form of Ampere's Law.

→ The closed path is touching the conductor

∴ the total current enclosed by the path  $I_{enc} = I$ .

$$\nabla \times \vec{H} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ H_x & H_y & H_z \end{vmatrix}$$

$$\nabla \times \vec{H} = \frac{1}{r} \begin{vmatrix} \hat{a}_r & r\hat{a}_\phi & \hat{a}_z \\ \partial/\partial r & \partial/\partial \phi & \partial/\partial z \\ H_r & rH_\phi & H_z \end{vmatrix}$$

$$\nabla \times \vec{H} = \frac{1}{r \sin \theta} \begin{vmatrix} \hat{a}_r & r\hat{a}_\theta & r \sin \theta \hat{a}_\phi \\ \partial/\partial r & \partial/\partial \theta & \partial/\partial \phi \\ H_r & rH_\theta & r \sin \theta H_\phi \end{vmatrix}$$

Ex-1 Let,  $\vec{H} = -y(x^2+y^2)\hat{a}_x + x(x^2+y^2)\hat{a}_y$  Alm. 133

Find the amount of current passing through  $z=0$ ,  $-1 \leq x \leq 1$ ,  $-2 \leq y \leq 2$  in  $\hat{a}_z$  direction.

Ans:

$$\nabla \times \vec{H} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ -y(x^2+y^2) & x(x^2+y^2) & 0 \end{vmatrix}$$

$$\therefore \nabla \times \vec{H} = 0 - 0 + \hat{a}_z (2x^2+y^2) + (x^2+3y^2)\hat{a}_z$$

$$\therefore \nabla \times \vec{H} = 4(x^2+y^2)\hat{a}_z \text{ Alm.}$$

$$\therefore \vec{J}_c \cdot d\vec{s} = (4(x^2+y^2)\hat{a}_z) (dx dy \hat{a}_z)$$

$$\therefore \vec{J}_c \cdot d\vec{s} = 4(x^2+y^2) dx dy$$

$$\therefore I = \int \vec{J}_c \cdot d\vec{s} = 4 \int_{-1}^1 \int_{-2}^2 (x^2+y^2) dx dy$$

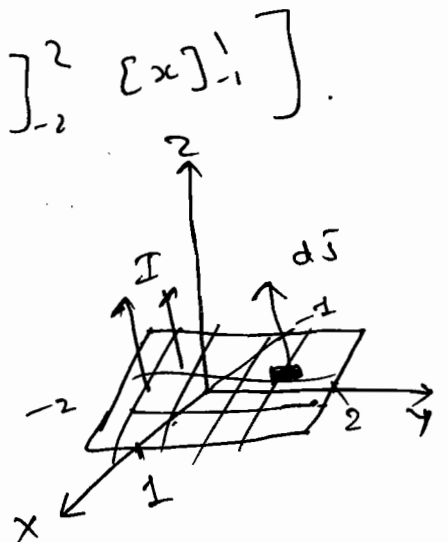
$$= 4 \left[ \int_{-2}^2 \int_{-1}^1 x^2 dx dy + \int_{-1}^1 \int_{-2}^2 y^2 dx dy \right]$$

$$= 4 \left[ \left[ \frac{x^3}{3} \right]_{-1}^1 [y]_{-2}^2 + \left[ \frac{y^3}{3} \right]_{-2}^2 [x]_{-1}^1 \right]$$

$$I = 4 \left[ \left( \frac{2}{3} \times 4 \right) + \frac{16}{3} \times 2 \right]$$

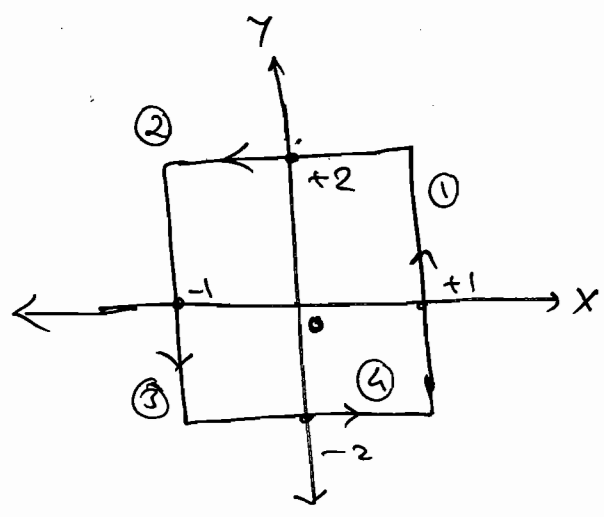
$$= 4 \left[ \frac{8}{3} + \frac{32}{3} \right]$$

$$\therefore I = 160 \text{ (A)}$$



→ Method 2: by Integral form

$$I_{enc} = \oint_C \vec{H} \cdot d\vec{l}$$



$$I_{enc} = \int_{(1)} \vec{H} \cdot d\vec{l} + \int_{(2)} \vec{H} \cdot d\vec{l} + \int_{(3)} \vec{H} \cdot d\vec{l} + \int_{(4)} \vec{H} \cdot d\vec{l}$$

Path No	$d\vec{l}$	Path is at	Path limit	$\vec{H} \cdot d\vec{l}$	$\vec{H} \cdot d\vec{l}$ at $x=1$
①	$dy \hat{a}_y$	$x=1$	$-2 \leq y \leq 2$	$x(x^2+y^2)dy$	$(1+y^2)dy$
②	$dx \hat{a}_x$	$y=2$	$+1 \leq x \leq -1$	$-y(x^2+y^2)dx$	$-2(x^2+4)dx$
③	$dy \hat{a}_y$	$x=-1$	$2 \leq y \leq -2$	$x(x^2+y^2)dy$	$-(1+y^2)dy$
④	$dx \hat{a}_x$	$y=-2$	$-1 \leq x \leq 1$	$-y(x^2+y^2)dx$	$2(x^2+4)dx$

$$\int_{(1)} \vec{H} \cdot d\vec{l} = \int_{-2}^2 (y^2+1) dy = \left[ \frac{y^3}{3} + y \right]_{-2}^2 = \frac{8}{3} + 2 + \frac{8}{3} - 2 = \frac{16}{3} + 4$$

$$\int_{(2)} \vec{H} \cdot d\vec{l} = \int_{1}^{-1} -2(x^2+4) dx = 2 \left[ \frac{x^3}{3} + 4x \right]_{1}^{-1} = \frac{4}{3} + 16$$

$$\int_{(3)} \vec{H} \cdot d\vec{l} = \int_{2}^{-2} -(1+y^2) dy = \left[ \frac{y^3}{3} + y \right]_{2}^{-2} = \frac{16}{3} + 4$$

$$\int_{(4)} \vec{H} \cdot d\vec{l} = \int_{-1}^1 2(x^2+4) dx = 2 \left[ \frac{x^3}{3} + 4x \right]_{-1}^1 = \frac{4}{3} + 16$$

$$\therefore I = \oint \vec{H} \cdot d\vec{\ell}$$

$$= \frac{16}{3} + \frac{16}{3} + \frac{4}{3} + \frac{4}{3} \cdot 20$$

$$\therefore I = \frac{40}{3} \cdot 20$$

$$I = \frac{160}{3} \text{ A}$$

\* Application of Ampere's Law:

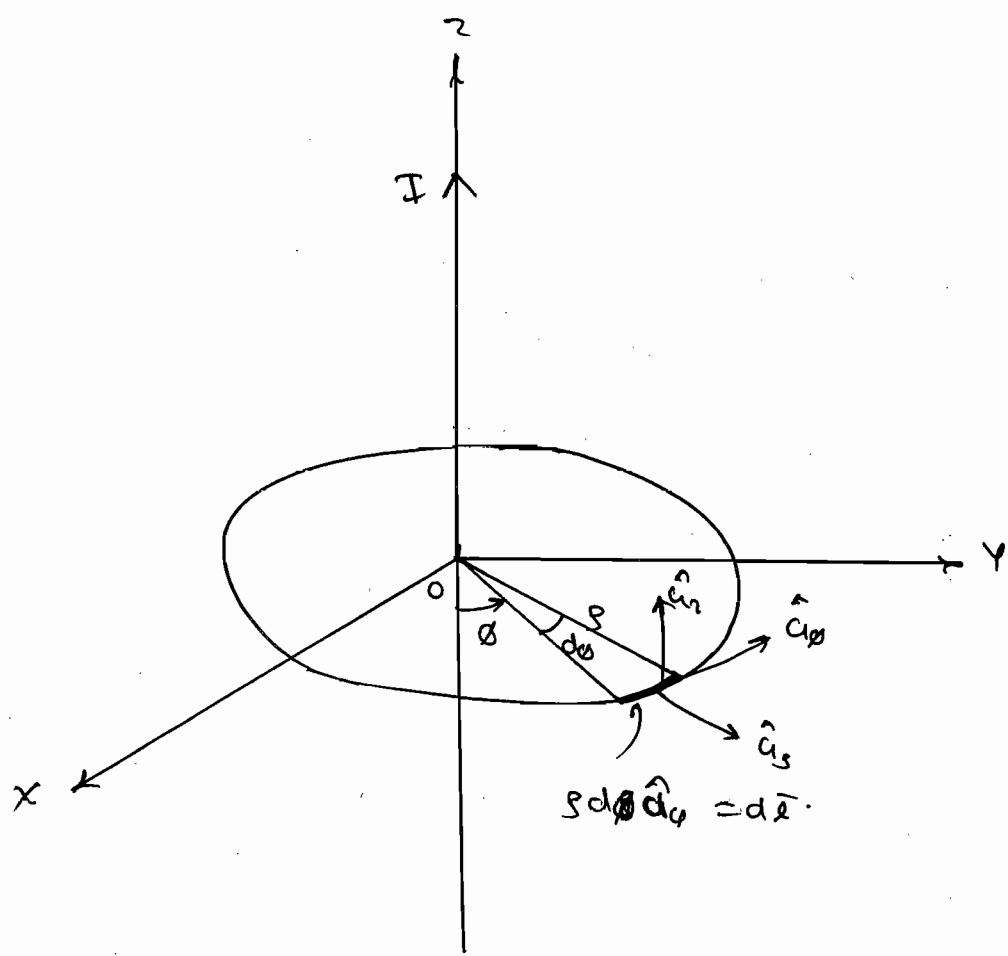
⇒ For symmetrical current distribution where we have an idea about the direction of magnetic field intensity then one can find out magnitude of the magnetic field intensity by using the following procedure.

- ① one has to choose a suitable appropriate closed path which is enclosing partially (or) fully the given current distribution
- ②  $d\vec{\ell}$  always lies along the path ✓
- ③ The closed path is so chosen in such a way that  $\vec{H}$  may lie along the path or normal to the path
- ④  $\vec{H} \cdot d\vec{\ell} = H \cdot d\ell$  if  $H$  lies along the path,  
 $\vec{H} \cdot d\vec{\ell} = 0$  if  $\vec{H}$  normal to the path.
- ⑤ over that part of the path where  $H$  lies along the path, on that part of the path

$\vec{H}$  is constant.

Ex-1 Find  $\vec{H}$  due to a long straight infinite filamentary conductor which carries a direct current of  $I$  A.

Ans: We assume that the infinite current filament lies along  $z$  axis



① A <sup>closed</sup> circular path is chosen of  $s = \text{const.}$  ( $s > 0$ ) is chosen.

②  $dl = s d\phi \hat{a}_\phi$

③  $\vec{H} = H_\phi \hat{a}_\phi$  only  $\vec{H}$  would be around the conductor.

$\vec{H} \cdot dl = \int H_\phi s d\phi$

④  $|\vec{H}| = H_\phi$  must be const. on  $s = \text{const.}$   
 $\therefore \vec{H}$  lies along the path.



$I_{enc} = I$  (The total current is enclosed). 137

$$\therefore \oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$\therefore I_{enc} = H_{\phi} \int_0^{2\pi} d\phi$$

$$\therefore I = H_{\phi} \int_0^{2\pi} d\phi$$

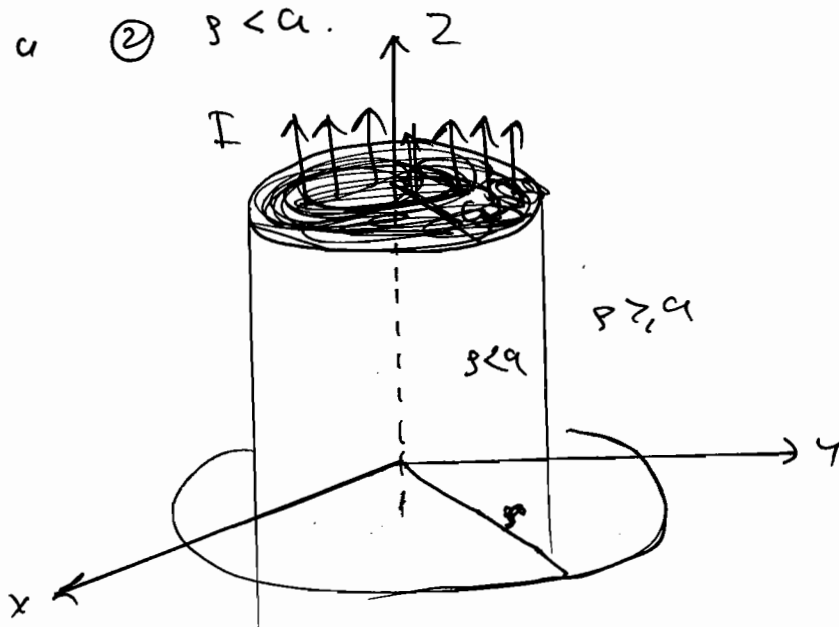
$$\therefore H_{\phi} = \frac{I}{2\pi r}$$

$$\therefore \boxed{\vec{H} = \frac{I}{2\pi r} \hat{a}_{\phi}}$$

Ex 2 Find  $\vec{H}$  due to a cylindrical conductor of radius  $a$  where current  $I$  is uniformly distributed throughout the cross section.

Ans 2 We assume that the solid cylindrical conductor is positioned along the  $z$ -axis as shown in the figure. where the current  $I$  is uniformly distributed throughout the cross section one can find  $\vec{H}$  for

- ①  $r \geq a$     ②  $r < a$ .



① The circular (closed) path of  $\rho = \text{constant}$  ( $\rho > 0$ ) is chosen.

②  $d\vec{\ell} = a d\phi \hat{a}_\phi$ .

③  $\vec{H} = H_\phi \hat{a}_\phi$ .

$$\vec{H} \cdot d\vec{\ell} = a H_\phi d\phi.$$

④  $|\vec{H}| = H_\phi$  must be const. on  $\rho = \text{const.}$

$\therefore \vec{H}$  lies along the path.

$I_{\text{enc}} = I$  (The total current is enclosed).

$$\therefore \oint \vec{H} \cdot d\vec{\ell} = I_{\text{enc}}.$$

$$\therefore a H_\phi \int_0^{2\pi} d\phi = I.$$

$$\therefore 2\pi a H_\phi = I.$$

$$\therefore H_\phi = \frac{I}{2\pi a}.$$

$$\therefore \boxed{\vec{H} = \frac{I}{2\pi a} \hat{a}_\phi}$$

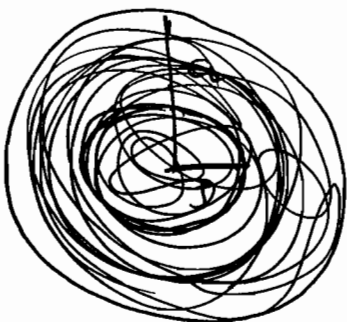
②  $\rho < a$ .

$$\pi a^2 \rightarrow I$$

$$\pi \rho^2 \rightarrow I'$$

$$\therefore I_{\text{enc}} = \frac{\pi \rho^2}{\pi a^2} \times I$$

$$\therefore I_{\text{enc}} = \frac{I \rho^2}{a^2}.$$



$$\oint \vec{H} \cdot d\vec{\ell} = I_{\text{enc}} \Rightarrow H_\phi (2\pi \rho) = \frac{I \rho^2}{a^2}.$$

$$\therefore H_{\phi} = \frac{I \rho}{2\pi a^2}$$

$$\therefore \boxed{\bar{H} = \frac{I \rho}{2\pi a^2} \hat{a}_{\phi}} \quad \text{for } \rho < a.$$

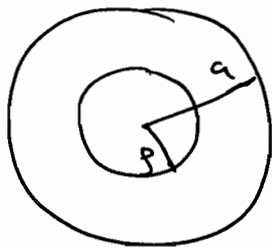
$$(i) \quad \rho \geq a \quad \bar{H} = \frac{I}{2\pi \rho} \hat{a}_{\phi} \Rightarrow |\bar{H}| \propto \frac{1}{\rho}$$

$$(iii) \quad \rho < a \quad \bar{H} = \frac{I \rho}{2\pi a^2} \hat{a}_{\phi} \Rightarrow |\bar{H}| \propto \rho$$

Ex-2 Repeat the above problem if it is a hollow cylindrical conductor of radius  $a$ .

$$\underline{\text{Ans:}} \quad (i) \quad \rho \geq a \quad \bar{H} = \frac{I}{2\pi \rho} \hat{a}_{\phi} =$$

$$(ii) \quad \rho < a \quad \bar{H} = 0$$



$\rho < a$   
 $I_{enc} = 0.$

# ★ Magnetic Flux Density ( $\bar{B}$ )

→ Unit  $\Rightarrow$  T (or)  $\text{wb/m}^2$ .

$$\bar{B} = \mu H.$$

$$\mu = \mu_0 \mu_r \text{ H/m.}$$

$\therefore \mu$ : permeability | Inductivity (H/m).

$\mu_0$ : Absolute permeability | Inductivity (H/m).

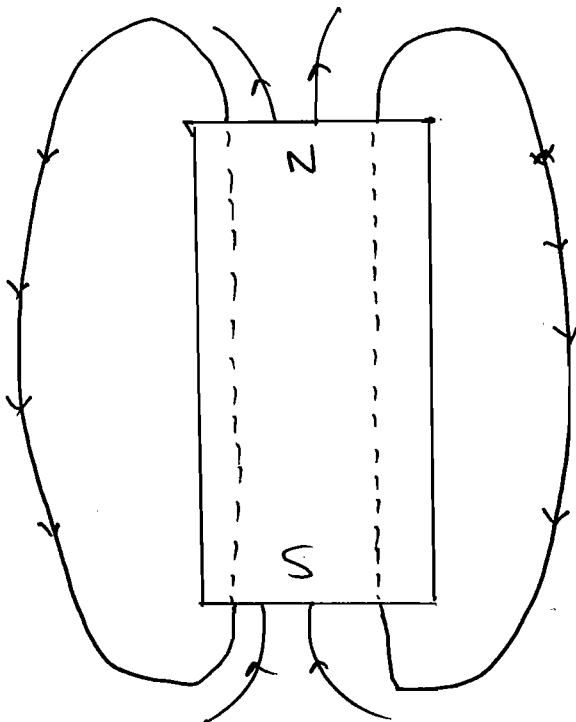
$\mu_r$ : Relative " "

→ Ⓚ Permeability or Inductivity specifies

property of a medium and that indicates the ability to store the magnetic energy.

~~Here~~ ~~is~~ ~~the~~ ~~definition~~ ~~of~~ ~~the~~ ~~term~~ ~~used~~

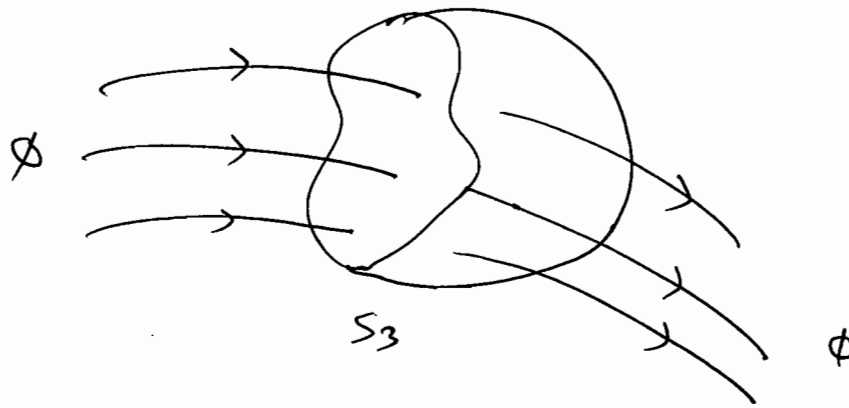
\* Magnetic flux:  $\Phi$  wb.



→ The amount of magnetic flux passing through a cross sectional surface 's' is given by.

$$\phi = \int_s \vec{B} \cdot d\vec{s}$$

↙ cross sectional



$S_3 =$  arbitrary closed surface.

→  $\oint_s \vec{B} \cdot d\vec{s} = 0.$

$\therefore \oint_v \nabla \cdot \vec{B} \cdot d\vec{v} = 0.$

$\therefore \boxed{\nabla \cdot \vec{B} = 0.}$

Gauss law for H-fields.

→ for electric field

$$\psi_{net} = q_{enc} = \int_s \vec{D} \cdot d\vec{s} = \int_v \nabla \cdot \vec{D} \cdot d\vec{v}.$$

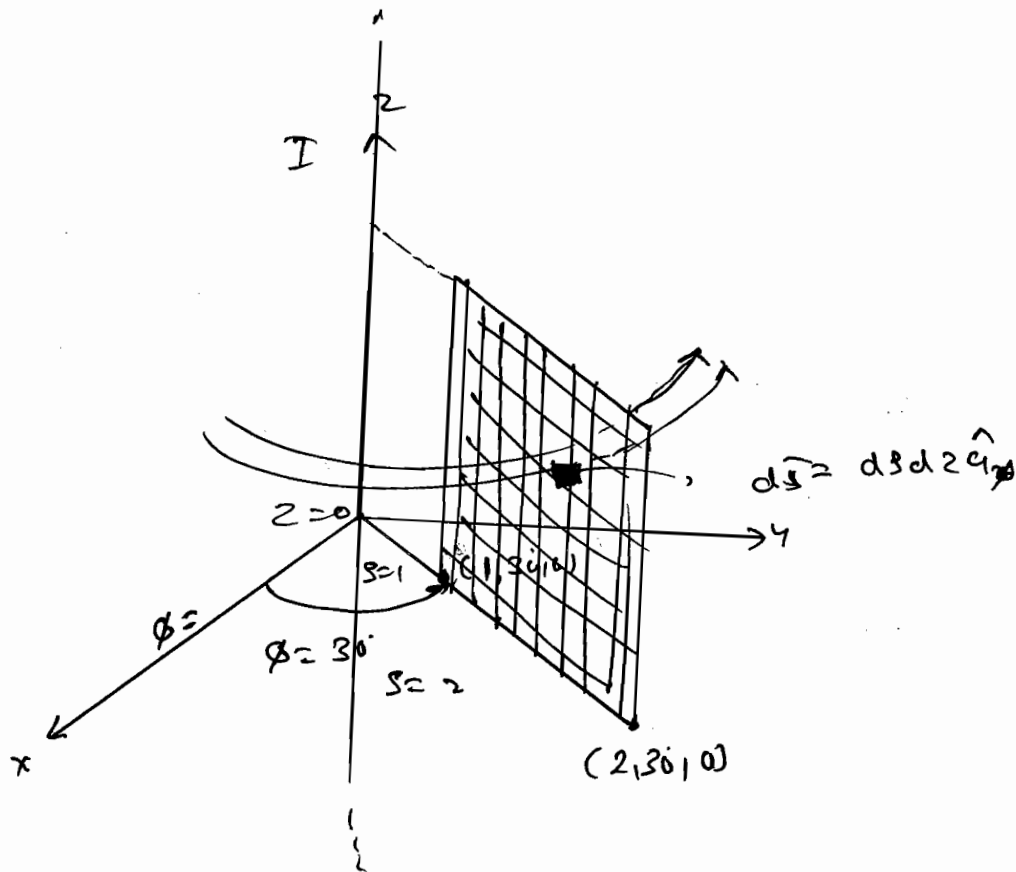
$\therefore \boxed{\nabla \cdot \vec{D} = \rho_v}$

Gauss field for E-fields.

→ Unlike a electric flux the magnetic flux would not have starting point and an ending point it enters the closed surface and leaves the same closed surface as shown above. one can find out the amount of magnetic flux passing through a cross sectional surface.

Ex-1 Find the amount of magnetic flux passing through a cross-sectioned surface define by  $\phi = 30^\circ$ ,  $1 \leq \rho \leq 2$ ,  $0 \leq z \leq 3$ . due to an infinite current filament lies along  $z$ -axis. which carries a direct current of  $2.5A$  along +ve  $z$ -direction. Assume  $\mu = \mu_0$ .

Ans:



$$\rightarrow d\vec{s} = ds dz \hat{a}_\phi$$

$$\vec{B} = \mu \vec{H}$$

$$\therefore \vec{B} = \mu_0 \vec{H}$$

$$\therefore \vec{B} = \frac{\mu_0 I}{2\pi r} \hat{a}_\phi$$

$$\therefore \vec{B} \cdot d\vec{s} = \frac{\mu_0 I}{2\pi r} ds dz$$

$$\therefore \phi = \int_S \vec{B} \cdot d\vec{s}$$

$$= \int_1^2 \int_0^3 \frac{\mu_0 I}{2\pi r} ds dz$$

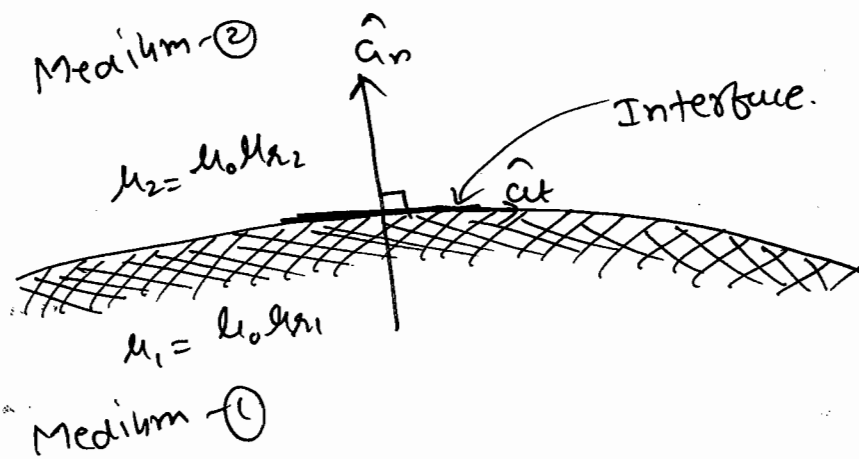
$$= \frac{\mu_0 I}{2\pi r} \times [z^2 - 1] \times [3]$$

$$\therefore \phi = \frac{3\mu_0 I \ln 2}{2\pi r} \omega b$$

$$\therefore \phi = \frac{3\mu_0 I \ln 2}{2\pi} \omega b$$

$$\phi = \frac{7.5 \mu_0 \ln 2}{2\pi} \omega b$$

# \* Boundary Condition:



(I) Using Ampere's Law, one can show that

$$(a) \quad \boxed{H_{t1} = H_{t2}}$$

Tangential components of H-fields are continuous across a current free interface.

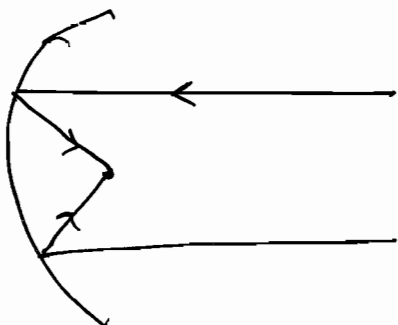
$$(b) \quad \boxed{(\vec{H}_1 - \vec{H}_2) \times \hat{a}_n = \vec{J}_s} \quad (\text{A/m})$$

→ Tangential components of H-fields are discontinuous by an amount of surface current densities.

(II) Using Gauss Law for H-field,

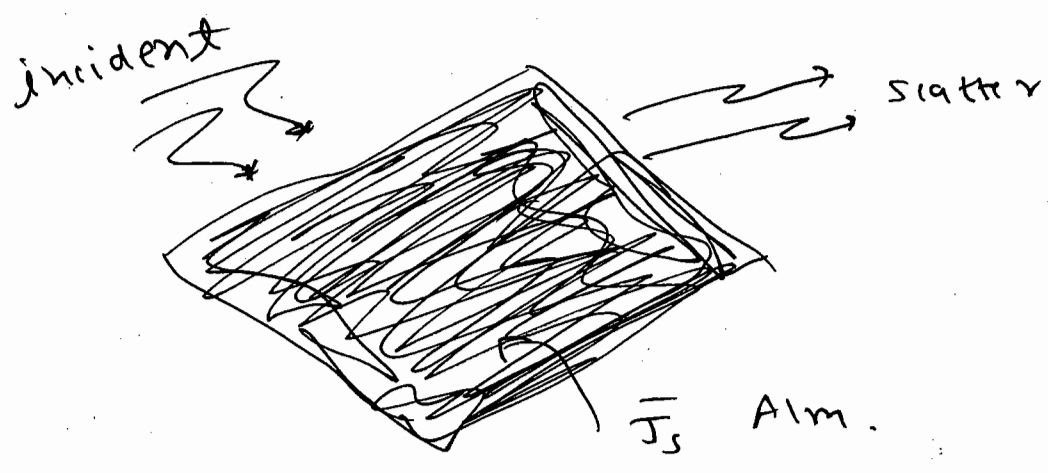
$$\boxed{B_{n1} = B_{n2}}$$

i.e. Normal component of magnetic flux densities are continuous across the interface.



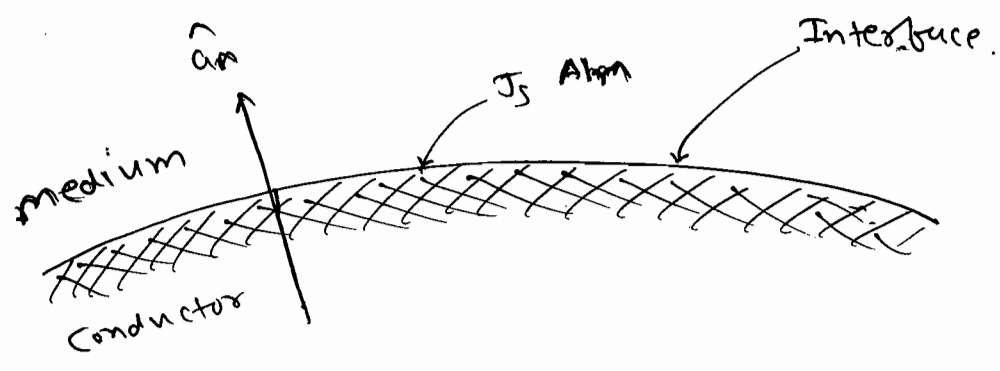
Parabolic entering.





PEC: Perfect electric Conductor  
 $\vec{J}_s$ : current per unit width (Alm)

\* Behaviour of Magnetic field intensities  
across a conductor interface.



①  $\hat{a}_n \times \vec{H} = \vec{J}_s$

→ Tangential components of magnetic fields are equal to surface current density.

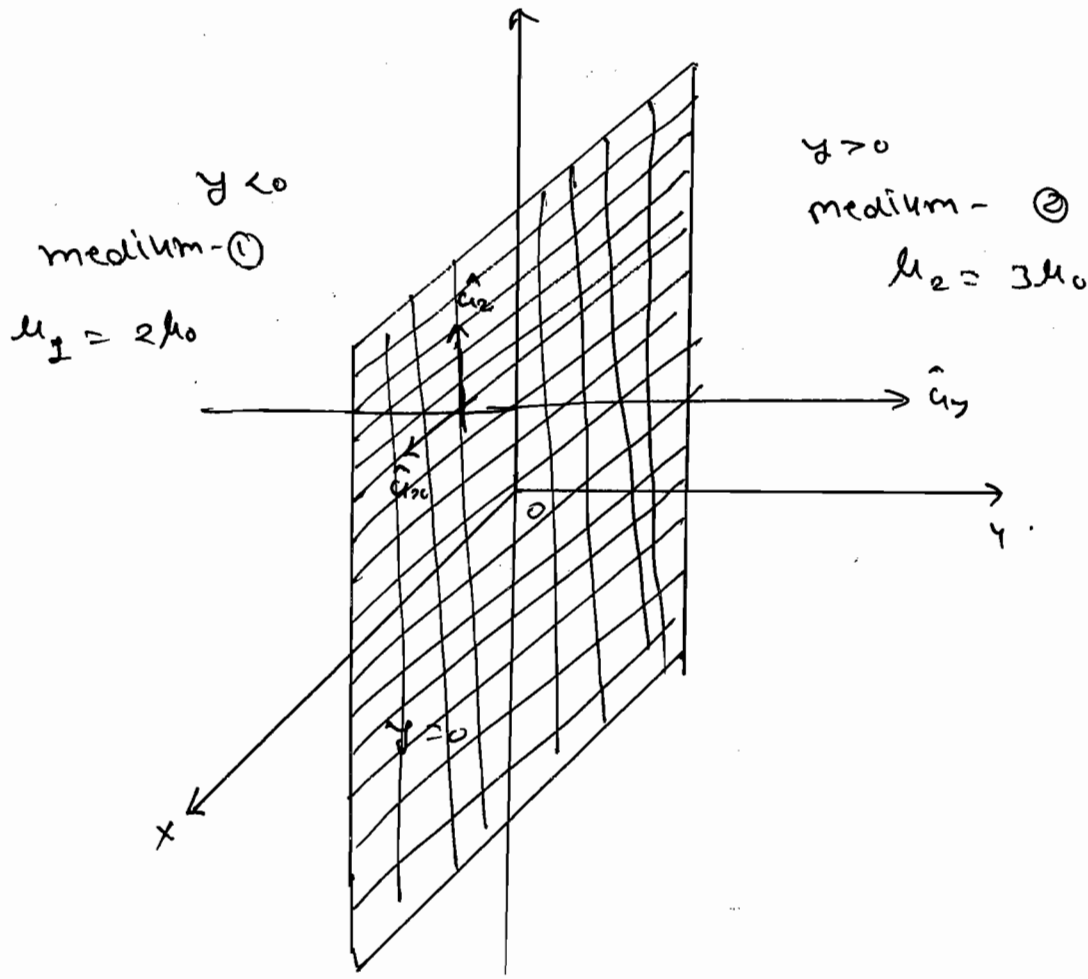
②  $B_n = 0$  (or)  $H_n = 0$ .

→ Normal components of magnetic field intensities are vanished across the conductor interface.

$\vec{J}_s$ : surface current density across the conductor interface.

Ex 1 The plane  $y=0$  separates two mediums  
 $y < 0$  is medium-① and is characterised by  $2\mu_0$  and  $y > 0$  is medium-② and is characterised by  $3\mu_0$  given that  
 $\vec{H}_1 = 10\hat{a}_z$  and  $\vec{H}_2 = 10\hat{a}_x$ . Find the surface current density across the interface.

Ans:



$\vec{H}_1 = 10\hat{a}_z$  ,  $\vec{H}_2 = 10\hat{a}_x$ .

$(\vec{H}_1 - \vec{H}_2) \times \hat{a}_n = \vec{J}_s$

$\therefore \vec{J}_s = (10\hat{a}_z - 10\hat{a}_x) \hat{a}_y$

$\vec{J}_s = -10\hat{a}_x - 10\hat{a}_z$  Alm.

Ex-2 Retesting to the above figure 147

Let,  $\vec{H}_1 = (3\hat{a}_x + 4\hat{a}_y + 5\hat{a}_z) \text{ A/m}$

$\vec{H}_2 =$

assume current free interface find  $\vec{B}_1, \vec{H}_2$  and  $\vec{B}_2$

Ans:

$\vec{B}_1 = \mu_1 [\vec{H}_1]$

$\vec{B}_1 = \mu_0 [6\hat{a}_x + 8\hat{a}_y + 10\hat{a}_z]$

$\vec{H}_1 = 3\hat{a}_x + 4\hat{a}_y + 5\hat{a}_z$

$\vec{H}_1 = H_{t1}\hat{a}_t + H_{n1}\hat{a}_n$

$H_{t1} = 3\hat{a}_x + 5\hat{a}_z, \quad H_{n1} = 4\hat{a}_y$

Now,  $H_{t1} = H_{t2}$  ( $\because \vec{J}_s = 0$ )

( $\because$  tangential components are equal)

$H_{t2} = 3\hat{a}_x + 5\hat{a}_z$

Now,  $\vec{H}_2 = H_{t2}\hat{a}_t + H_{n2}\hat{a}_n$

$B_{n1} = B_{n2}$  ( $\because \vec{J}_s \neq 0$ )

$B_{n2} = B_{n1}$

$\mu_2 H_{n2} = \mu_1 H_{n1}$

$H_{n2} = \frac{\mu_1}{\mu_2} \times 4\hat{a}_y$

$H_{n2} = \frac{2}{3} \times 4\hat{a}_y$

$H_{n2} = \frac{8}{3}\hat{a}_y$

$\vec{H}_2 = 3\hat{a}_x + \frac{8}{3}\hat{a}_y + 5\hat{a}_z$

$$\therefore \vec{B}_2 = \mu_2 \vec{H}_2$$

$$\therefore \vec{B}_2 = \mu_0 [ 9\hat{a}_x + 8\hat{a}_y + 15\hat{a}_z ]$$

Ex-3 In the above problem assume that the interface has non zero surface current density of  $\vec{J}_s = (5\hat{a}_x + 10\hat{a}_z)$  A/m. Find

$\vec{B}_1$ ,  $\vec{H}_2$  and  $\vec{B}_2$ .

Ans:

$$\vec{H}_1 = 3\hat{a}_x + 4\hat{a}_y + 5\hat{a}_z$$

$$\vec{B}_1 = \mu_1 \vec{H}_1$$

$$\vec{B}_1 = \mu_0 [ 6\hat{a}_x + 8\hat{a}_y + 10\hat{a}_z ]$$

Now,  $(\vec{H}_1 - \vec{H}_2) \times \hat{a}_n = \vec{J}_s$

$$\therefore \left[ (\mu_{k1} - \mu_{k2}) \hat{a}_t + (\mu_{n1} - \mu_{n2}) \hat{a}_n \right] \times \hat{a}_n = \vec{J}_s$$

$$\therefore (\mu_{k1} - \mu_{k2}) (\hat{a}_t \times \hat{a}_n) = \vec{J}_s$$

$$\therefore \hat{a}_t = \frac{3}{\sqrt{34}} \hat{a}_x + \frac{5}{\sqrt{34}} \hat{a}_z$$

$$\therefore \hat{a}_n = \hat{a}_y$$

$$\therefore \hat{a}_t \times \hat{a}_n = \frac{12}{\sqrt{34}} \hat{a}_z - \frac{20}{\sqrt{34}} \hat{a}_x$$

$$\therefore (\mu_{k1} - \mu_{k2}) \left( \frac{12}{\sqrt{34}} \hat{a}_z - \frac{20}{\sqrt{34}} \hat{a}_x \right) = 5\hat{a}_x + 10\hat{a}_z$$

$$\therefore \frac{12}{\sqrt{34}} (\mu_{k1} - \mu_{k2}) = 10, \quad -\frac{20}{\sqrt{34}} (\mu_{k1} - \mu_{k2}) = 5$$

$$(H_{t1} - H_{t2}) = \frac{5 \sqrt{34}}{\sqrt{34}}$$

$$H_{t2} - H_{t1} = \frac{\sqrt{34}}{4}$$

$$H_{t1} - H_{t2} = \frac{\sqrt{34}}{4}$$

$$\therefore \bar{H}_{t1} = H_{t1} \cdot \hat{a}_t$$

$$\therefore H_{t1} = \bar{H}_{t1} \cdot \hat{a}_t$$

$$\bar{H} = 3\hat{a}_x + 5\hat{a}_z$$

$$(\bar{H}_1 - \bar{H}_2) \times \hat{a}_n = \vec{f}_s$$

$$\therefore \left[ (3 - H_{x2}) \hat{a}_x + (4 - H_{y2}) \hat{a}_y + (5 - H_{z2}) \hat{a}_z \right] \times \hat{a}_y = 5\hat{a}_x + 10\hat{a}_z$$

$$\therefore 7 - 3 - H_{x2} = 10 \Rightarrow H_{x2} = -7$$

$$\therefore -(5 - H_{z2}) = 5$$

$$\therefore H_{z2} = 10$$

$$\therefore \bar{H}_2 = -7\hat{a}_x + H_{y2}\hat{a}_y + 10\hat{a}_z$$

$$\therefore B_2 = \mu_2 \bar{H}_2$$

$$\therefore B_2 \Rightarrow \cancel{2\hat{a}_x} \rightarrow 2\hat{a}_x$$

$$-7\mu_2 \hat{a}_x + \mu_2 H_{y2} \hat{a}_y + 10\mu_2 \hat{a}_z = B_{x2} \hat{a}_x + 4\mu_1 \hat{a}_y + B_{z2} \hat{a}_z$$

$$\therefore B_{x2} = -7\mu_2$$

$$B_{z2} = 10\mu_2$$

$$H_{y2} = \frac{4\mu_1}{\mu_2} \text{ A/m}$$

$$\therefore H_{y2} = \frac{8}{3} \hat{a}_y$$

$$\therefore \boxed{\bar{H}_2 = -7\hat{a}_x + \frac{8}{3}\hat{a}_y + 10\hat{a}_z}$$

$$\bar{B}_2 = (-21\hat{a}_x + 8\hat{a}_y + 30\hat{a}_z) \mu_2$$

$$\bar{B}_1 = \mu_1 \bar{H}_1$$

$$\boxed{\bar{B}_1 = (6\hat{a}_x + 8\hat{a}_y + 10\hat{a}_z) \mu_1}$$

# ☆ Time Varying Fields:

→ The existing Ampere's Law, when it is applied to the time-varying fields in a non-conducting medium the Law is having some inconsistency or unsatisfaction. This inconsistency is been eliminated by adding a new term  $\vec{J}_D$  as follows:

$$\boxed{\nabla \times \vec{H} = \vec{J}_c + \vec{J}_D} \rightarrow \text{Modified Ampere's Law}$$

∴ take  $\nabla$  on both the side.

$$\nabla \cdot \nabla \times \vec{H} = \nabla \cdot \vec{J}_c + \nabla \cdot \vec{J}_D$$

∴ Divergence of curl is zero.

$$\nabla \cdot \vec{J}_c = - \nabla \cdot \vec{J}_D$$

$$\nabla \cdot \vec{J}_c = - \frac{\partial \rho_u}{\partial t}$$

$$\nabla \cdot \vec{J}_D = + \frac{\partial \rho_u}{\partial t}$$

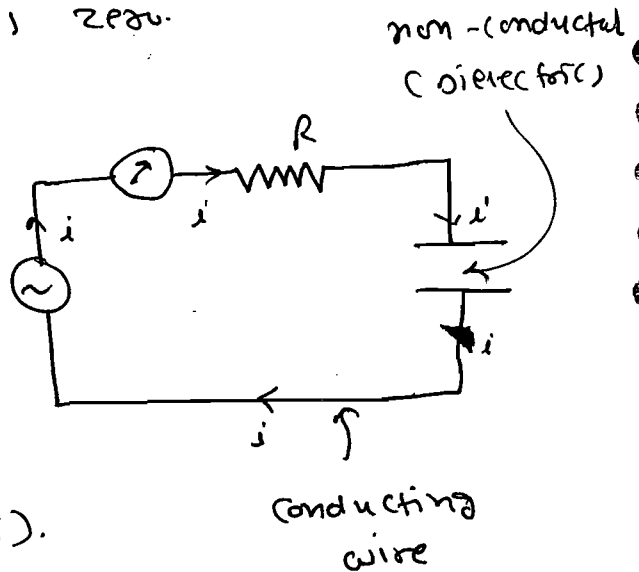
$$\nabla \cdot \vec{J}_D = \frac{\partial}{\partial t} (\nabla \cdot \vec{D})$$

$$\nabla \cdot \vec{J}_D = \nabla \cdot \frac{\partial \vec{D}}{\partial t}$$

∴ Suppressing  $\nabla$  both the side.

$$\boxed{\vec{J}_D = \frac{\partial \vec{D}}{\partial t}}$$

$\vec{J}_D =$  Displacement current density.



→  $\bar{J}_D$  is defined as time rate of change of electric flux density.

→  $\bar{J}_c$  dominates in a conducting medium and is zero in perfect dielectric.

→  $\bar{J}_D$  dominates in a dielectric medium and is zero in perfect conductor.

→ The modified Ampere's Law is written

$$\text{as } \boxed{\bar{J}_c + \bar{J}_D = \nabla \times \bar{H}}$$

$$\therefore \nabla \times \bar{H} = \bar{J}_c + \bar{J}_D$$

$$\therefore \boxed{\oint \bar{H} \cdot d\bar{l} = \int_S (\bar{J}_c + \bar{J}_D) \cdot d\bar{S}}$$

$$\therefore \boxed{\begin{aligned} \bar{J}_c &= \sigma \bar{E} \quad \text{A/m}^2 \\ \bar{J}_D &= \frac{\partial D}{\partial t} = \epsilon \frac{\partial \bar{E}}{\partial t} \quad \text{A/m}^2 \end{aligned}}$$

# \* Faraday's Law of Electromagnetic Conduction:

→ When a stationary conductor cuts by a moving magnetic flux then or vice versa then emf will be induced. This induced emf will in turn produces a magnetic flux which opposes original flux [Lenz's law]. Mathematically we write

$$\text{emf} = - \frac{\partial \Phi}{\partial t}$$

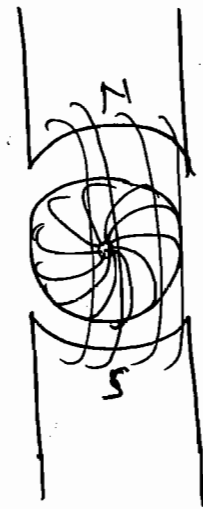
$$\therefore \oint_{\ell} \vec{E} \cdot d\vec{\ell} = - \frac{\partial \Phi}{\partial t}$$

↓

$$\therefore \oint_{\ell} \vec{E} \cdot d\vec{\ell} = - \frac{\partial}{\partial t} \int_S \vec{B} \cdot d\vec{S}$$

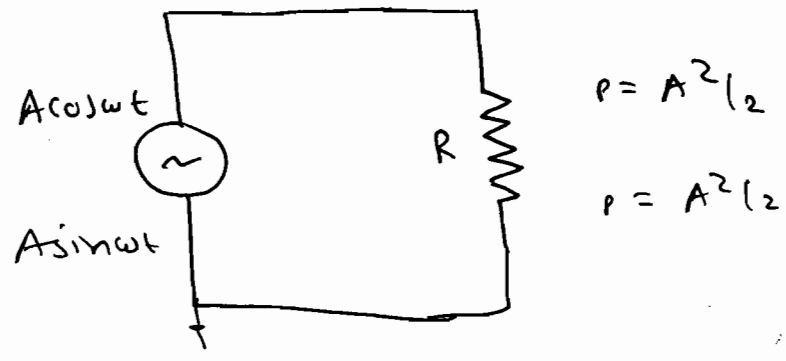
$$\therefore \int_S (\nabla \times \vec{E}) \cdot d\vec{S} = - \frac{\partial}{\partial t} \int_S \vec{B} \cdot d\vec{S}$$

$$\therefore \boxed{\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}}$$





→ Whether source is  $A \cos \omega t$  or  $A \sin \omega t$  the average power deliver to  $1 \Omega$  resistor is identically same which is equal to  $A^2/2$ .



0.1  $\angle 45^\circ$  volts → phasor form.

- $0.1 \cos (\omega t + 45^\circ)$  (or)
- $0.1 \sin (\omega t + 45^\circ)$ .
- or  $\text{Im} [0.1 e^{j(\omega t + 45^\circ)}]$  (or)
- $\text{Re} [0.1 e^{j(\omega t + 45^\circ)}]$ .

→ When the quantities are represented in the phasor form we suppress the time variation for the mathematical convenience this time variations are approximated as cosine or sine or  $e^{j\omega t}$ .

→  $\vec{E} \rightarrow \vec{E}(x, y, z)$  (or)  $\vec{E}(r, \theta, \phi, t)$  or  $\vec{E}(r, \theta, \phi, t)$ .  
 ↳ It is a function of time and space coordinates.

$$\vec{E} = \text{Re} [ \vec{E}_a \cdot e^{j\omega t} ]$$

$\bar{E}_z$  is called phasor form of  $\bar{E}$ .

$$\bar{E}_z \rightarrow \bar{E}_z(x, y, z) \text{ (or) } \bar{E}_z(r, \phi, z) \text{ (or) } \bar{E}_z(r, \theta, \phi).$$

↳ It is a f<sup>n</sup> of space coordinates only.

$$\rightarrow \nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}.$$

$$\therefore \nabla \times [\text{Re}\{\bar{E}_z \cdot e^{j\omega t}\}] = -\frac{\partial}{\partial t} [\text{Re}\{\bar{B}_z \cdot e^{j\omega t}\}].$$

$$\therefore \nabla \times [\text{Re}\{\bar{E}_z \cdot e^{j\omega t}\}] = -j\omega [\text{Re}\{\bar{B}_z \cdot e^{j\omega t}\}].$$

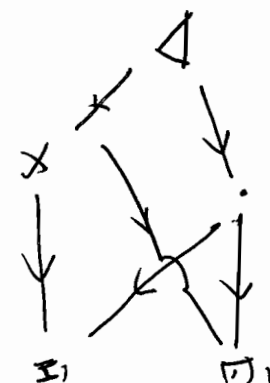
∴ Suppressing time variation both the side.

$$\therefore \boxed{\nabla \times \bar{E}_z = -j\omega \bar{B}_z}$$

So,

$$\frac{\partial/\partial t = j\omega = s}{\int dt = \frac{1}{j\omega} = 1/s}.$$

→ This is Faraday's law in phasor form.

Name of the laws	Integral form	Point form	Phasor form
1. Faraday's Law	$\oint \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \int \vec{B} \cdot d\vec{s}$	$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ $= -\mu \frac{\partial \vec{H}}{\partial t}$	$\nabla \times \vec{E}_s = -j\omega \vec{B}_s$
2. Modified Ampere's Law	$\oint \vec{H} \cdot d\vec{l} = \int (\vec{J}_c + \vec{J}_d) \cdot d\vec{s}$	$\nabla \times \vec{H} = \vec{J}_c + \vec{J}_d$ $= \sigma \vec{E} + \epsilon \frac{\partial \vec{E}}{\partial t}$	$\nabla \times \vec{H}_s = \vec{J}_{cs} + \vec{J}_{ds}$ $= \sigma \vec{E}_s + \epsilon \frac{\partial \vec{E}_s}{\partial t}$
3. Gauss Law for E-field	$\oint \vec{D} \cdot d\vec{s} = Q_{enc}$ $= \int \rho_{enc} \cdot dV$	$\nabla \cdot \vec{D} = \rho_v$	$\nabla \cdot \vec{D}_s = \rho_s$
Gauss Law for H-field	$\oint \vec{B} \cdot d\vec{l} = 0$	$\nabla \cdot \vec{B} = 0$	$\nabla \cdot \vec{B}_s = 0$
Maxwell's Equation	$\vec{\nabla} \cdot \vec{D} = \frac{\partial \rho}{\partial t} = \epsilon \frac{\partial \vec{E}}{\partial t}$ $\vec{\nabla} \cdot \vec{J}_c = \sigma \vec{E}$		

→ Maxwell had proved that any Electromagnetic problem can be solved by using above four eqns.

Ex-1 Let  $\vec{D} = (3x\hat{a}_x + ky\hat{a}_y + 7z\hat{a}_z) \text{ nC/m}^2$

Assume Charge free region.  
 $\rho_v = 0$

Ans:

$\therefore \nabla \cdot \vec{D} = \rho_v$   
 But,  $\rho_v = 0$ .

$\therefore k = 11 \text{ nC/m}^3$   
 $k = 11/y \text{ nC/m}^2$   
 $\therefore k = 11 \text{ nC/m}^3$

$\therefore 3 + k + 7 = 0$   
 $\therefore k = -11 \text{ nC/m}^3$

Ex-2 Let,  $\vec{E} = (kx - 100t)\hat{a}_y \text{ V/m}$ ,  $\vec{H} = (x + 20t)\hat{a}_z$   
 A/m. Assume  $\mu = 0.25 \text{ H/m}$ .

→  $\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}$

$\therefore \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ 0 & kx - 100t & 0 \end{vmatrix} = -\mu (0 + 20)\hat{a}_z$

$\therefore 0 - 0 + (k(1) - 0)\hat{a}_z = -20\mu\hat{a}_z$       unit is meter  
 $k = -20\mu$   
 $k = -20 \times \frac{1}{4}$   
 $\therefore k = -5 \text{ V/m}^2$

$\therefore k = -50 \text{ V/m}^2$

$\therefore k = -5 \text{ V/m}^2$

\* EM Waves:

⇒ Linear Medium:-

→ A medium is said to be linear if that medium  $\underline{\bar{D}}, \underline{\bar{E}}$  must have same direction (or)  $\underline{\bar{B}}, \underline{\bar{H}}$  must have same direction.  
 It does not mean that all are having same direction.

⇒ Homogeneous Medium:-

→ Usually at high frequency medium <sup>properties</sup> is characterised by  $\mu$  and  $\epsilon$ . If these are constant throughout the medium then the medium is said to be a homogeneous medium.

⇒ Isotropic Medium:-

→ In this medium  $\mu$  and  $\epsilon$  scalar constant.

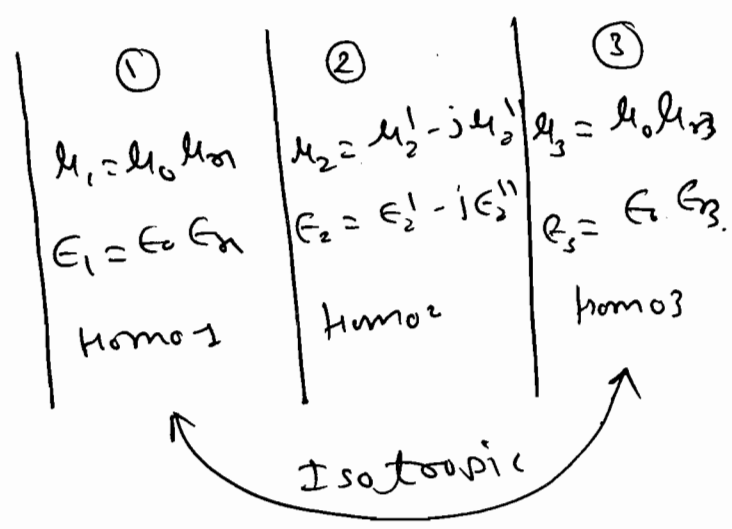
In general,

$$\mu = \begin{matrix} \mu' - j\mu'' \\ \epsilon' - j\epsilon'' \end{matrix}$$

Real part  
↓  
Imag. part

$$\mu = \mu_0 \mu_r$$

$$\epsilon = \epsilon_0 \epsilon_r$$



→ Real part of  $\mu$  &  $\epsilon$  indicate storage property of medium.

→ Imaginary part of  $\mu$  &  $\epsilon$  indicate, dissipate property of medium.

→ An isotropic medium is homogeneity  
✓ whereas homogeneity medium need not be isotropic.

→ Charge free medium:  $\rho_v = 0$ .

→ Non-Conducting medium:  $\sigma = 0$ .

\* Unbounded medium:

→ There are no boundaries to meet in any direction.

→ We assume that the wave is propagating through a linear homogeneity isotropic charge free non-conducting and unbounded medium.

⇒ Writing the Maxwell's eq<sup>n</sup> for the above assumed medium.

$$(1) \nabla \times \bar{E} = -\mu \frac{\partial \bar{H}}{\partial t}$$

$$(2) \nabla \times \bar{H} = \epsilon \frac{\partial \bar{E}}{\partial t} \quad (\text{Non conducting medium is assumed } \sigma = 0).$$

(3)  $\nabla \cdot \bar{D} = 0$  ( $\because$  Charge free medium is assumed  $\rho_v = 0$ ).

$\Rightarrow \nabla \cdot \epsilon \bar{E} = 0$

$\Rightarrow \nabla \cdot \bar{E} = 0$  ( $\because$  homogeneous medium is assumed).

(4)  $\nabla \cdot \bar{H} = 0$ .

$\nabla \cdot \bar{B} = 0$ .

$\rightarrow$  Taking curl on (1) both the sides.

$\nabla \times \nabla \times \bar{E} = -\mu \nabla \times \frac{\partial \bar{H}}{\partial t}$

$\therefore \nabla(\nabla \cdot \bar{E}) - \nabla^2 \bar{E} = -\mu \frac{\partial}{\partial t} (\nabla \times \bar{H})$   
 $\downarrow$  0  $\downarrow$   $+\frac{\partial \bar{E}}{\partial t} \times \epsilon$

$\therefore \nabla^2 \bar{E} = \mu \epsilon \frac{\partial^2 \bar{E}}{\partial t^2}$   $\rightarrow$  Vector wave eq<sup>n</sup>

Similarly taking curl on (2) both sides.

$\nabla^2 \bar{H} = \mu \epsilon \frac{\partial^2 \bar{H}}{\partial t^2}$

$\rightarrow$  For simplicity let us solve the problem in Cartesian coordinate.

$\rightarrow$  Expanding wave eq<sup>n</sup> in Cartesian coordinate.

$\therefore \left. \begin{aligned} \frac{\partial^2 \bar{E}_x}{\partial x^2} + \frac{\partial^2 \bar{E}_x}{\partial y^2} + \frac{\partial^2 \bar{E}_x}{\partial z^2} &= \mu \epsilon \frac{\partial^2 \bar{E}_x}{\partial t^2} \\ \frac{\partial^2 \bar{H}_x}{\partial x^2} + \frac{\partial^2 \bar{H}_x}{\partial y^2} + \frac{\partial^2 \bar{H}_x}{\partial z^2} &= \mu \epsilon \frac{\partial^2 \bar{H}_x}{\partial t^2} \end{aligned} \right\} \begin{aligned} &\text{These are} \\ &\text{2nd order} \\ &\text{4 dim.} \\ &\text{PDE'S.} \end{aligned}$

→  $\bar{E}$  and  $\bar{H}$  are fns of time and Space Coordinates.

→ For simplicity let us assumed that wave is propagating along  $z$ -direction in unbounded medium.

→ since there are no boundaries to meet along  $x$  &  $y$  directions. Then we conclude the partial variation of any field component with respect to  $x$  and  $y$  i.e.

$$\frac{\partial}{\partial x} ( ) = 0, \quad \frac{\partial}{\partial y} ( ) = 0.$$

←—————→ ( $z$ ).

→ the eq<sup>n</sup> reduced to

$$\frac{\partial^2 \bar{E}}{\partial z^2} = \mu \epsilon \frac{\partial^2 \bar{E}}{\partial t^2}$$

Similarity  $\frac{\partial^2 \bar{H}}{\partial z^2} = \mu \epsilon \frac{\partial^2 \bar{H}}{\partial t^2}$

These are 2<sup>nd</sup> order 2-Dim PDES.

→ we assumed charge free region:

$$\nabla \cdot \bar{E} = 0.$$

$$\therefore \frac{\partial (E_x)}{\partial x} + \frac{\partial (E_y)}{\partial y} + \frac{\partial (E_z)}{\partial z} = 0.$$

$$0 + 0 + \frac{dE_z}{dz} = 0.$$

∴  $E_z$  may be zero (or) constant.



→ Max. Value of D.D. =  $|\nabla\phi|$ .

(OR)  
Greatest rate of increase.

\* Angle bet<sup>n</sup> the two surfaces:

→ Let,  $\phi_1(x, y, z) = c_1$  &

$\phi_2(x, y, z) = c_2$

$$\therefore \cos\theta = \frac{\nabla\phi_1 \cdot \nabla\phi_2}{|\nabla\phi_1| \cdot |\nabla\phi_2|}$$

\* For solenoidal vector  $\nabla \cdot \vec{F} = 0$ .

\* For irrotational vector  $\nabla \times \vec{F} = 0$ .

\* Green Theorem in a plane.

$$\rightarrow \int M(x, y) dx + N(x, y) dy = \iint_R \left[ \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right] dx dy.$$



\* Del operator ( $\nabla$ ).

$\rightarrow \nabla = \partial/\partial x \bar{a}_x + \partial/\partial y \bar{a}_y + \partial/\partial z \bar{a}_z$ .

\* gradient of a scalar field:

$\rightarrow \text{grad } V = \nabla V = \frac{dV}{dn} \Big|_{\text{max}} \bar{a}_n$ .

\* Divergence of a vector:

$\therefore \text{grad } V = \nabla V = \frac{\partial V}{\partial x} \bar{a}_x + \frac{\partial V}{\partial y} \bar{a}_y + \frac{\partial V}{\partial z} \bar{a}_z$ .

\* Divergence of a vector:

$\nabla \cdot \bar{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$ .

\* 

	Coordinate			Multiplier			Unit vector		
	u	v	w	$h_1$	$h_2$	$h_3$	$\bar{a}_u$	$\bar{a}_v$	$\bar{a}_w$
Cartesian	x	y	z	1	1	1	$\bar{a}_x$	$\bar{a}_y$	$\bar{a}_z$
Cylindrical	$\rho$	$\phi$	z	1	$\rho$	1	$\bar{a}_\rho$	$\bar{a}_\phi$	$\bar{a}_z$
Spherical	$r$	$\theta$	$\phi$	1	$r$	$r \sin \theta$	$\bar{a}_r$	$\bar{a}_\theta$	$\bar{a}_\phi$

$\rightarrow \nabla \phi = \frac{1}{h_1} \frac{\partial \phi}{\partial u} \hat{a}_u + \frac{1}{h_2} \frac{\partial \phi}{\partial v} \bar{a}_v + \frac{1}{h_3} \frac{\partial \phi}{\partial w} \bar{a}_w$

$\rightarrow \nabla \cdot \bar{A} = \frac{1}{h_1 h_2 h_3} \left[ \frac{\partial}{\partial u} (h_2 h_3 A_u) + \frac{\partial}{\partial v} (h_3 h_1 A_v) + \frac{\partial}{\partial w} (h_1 h_2 A_w) \right]$

$\rightarrow \nabla \times \bar{A} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \bar{a}_u & h_2 \bar{a}_v & h_3 \bar{a}_w \\ \partial/\partial u & \partial/\partial v & \partial/\partial w \\ h_1 A_u & h_2 A_v & h_3 A_w \end{vmatrix}$

$$\rightarrow \nabla^2 \phi = \frac{1}{h_1 h_2 h_3} \left[ \frac{\partial}{\partial u} \left( \frac{h_2 h_3}{h_1} \frac{\partial \phi}{\partial u} \right) + \frac{\partial}{\partial v} \left( \frac{h_1 h_3}{h_2} \frac{\partial \phi}{\partial v} \right) + \frac{\partial}{\partial w} \left( \frac{h_1 h_2}{h_3} \frac{\partial \phi}{\partial w} \right) \right]$$

$$\rightarrow \nabla^2 \bar{A} = \frac{1}{h_1 h_2 h_3} \left[ \frac{\partial}{\partial u} \left( \frac{h_2 h_3}{h_1} \frac{\partial \bar{A}_1}{\partial u} \right) + \frac{\partial}{\partial v} \left( \frac{h_1 h_3}{h_2} \frac{\partial \bar{A}_1}{\partial v} \right) + \frac{\partial}{\partial w} \left( \frac{h_1 h_2}{h_3} \frac{\partial \bar{A}_1}{\partial w} \right) \right]$$

### \* Divergence Theorem:

$$\int_V (\nabla \cdot \bar{A}) dv = \oint_S \bar{A} \cdot d\bar{s}$$

Surface to Volume

$$\therefore \oint_S \bar{A} \cdot d\bar{s} = \int_V \nabla \cdot \bar{A} dv$$

### \* Stoke's Theorem:

$$\int_S (\nabla \times \bar{A}) \cdot d\bar{s} = \oint_C \bar{A} \cdot d\bar{l}$$

line to

Surface

$$\therefore \oint_C \bar{A} \cdot d\bar{l} = \int_S \nabla \times \bar{A} \cdot d\bar{s}$$

### \* Directional derivative (D.D):

The Directional derivative of a diff<sup>n</sup> scalar function in the direction of vector  $\bar{a}$  is

$$D.D = \nabla \phi \cdot \frac{\bar{a}}{|\bar{a}|}$$

\* Unit Vector, Vector and its magnitude. 165

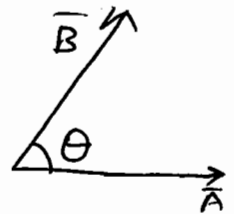
$$\rightarrow \hat{a}_{AB} = \frac{\vec{AB}}{|\vec{AB}|}$$

$$\rightarrow \vec{AB} = (x_2 - x_1) \hat{a}_x + (y_2 - y_1) \hat{a}_y + (z_2 - z_1) \hat{a}_z$$

$$\rightarrow |\vec{AB}| \text{ or } AB = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

\* Scalar or Dot Product:

$$\rightarrow \boxed{\vec{A} \cdot \vec{B} = AB \cos \theta}$$

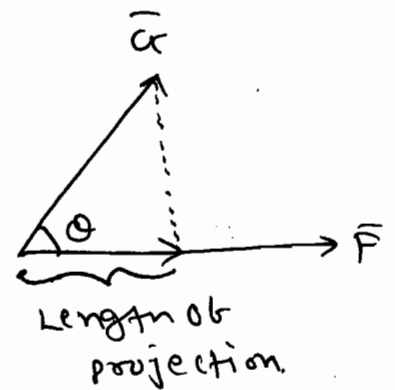


where  $\theta$  = angle bet<sup>n</sup>  $\vec{A}$  &  $\vec{B}$

\* Length of Projection:

Per

$$\rightarrow \text{Length of projection} = \vec{C} \cdot \hat{a}_F$$



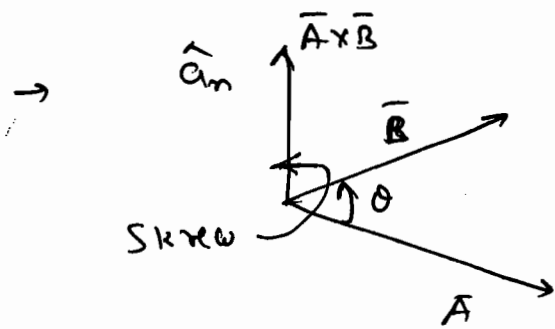
$$\rightarrow \text{Vector projection} = (\vec{C} \cdot \hat{a}_F) \hat{a}_F$$

$$= \frac{\vec{C} \cdot \vec{F}}{F^2} \times \vec{F}$$

\* Cross Product

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

$$\rightarrow \bar{A} \times \bar{B} = -\bar{B} \times \bar{A}$$



$$\therefore \bar{A} \times \bar{B} = AB \sin \theta \hat{a}_m$$

### \* Application of cross product:

$$\rightarrow \text{Area of parallelogram} = |\bar{A} \times \bar{A}c| \checkmark$$

$$\rightarrow \text{Area of the triangle ABC} = \frac{1}{2} |\bar{A} \times \bar{A}c| \checkmark$$

### \* Scalar triple Product:

$$\rightarrow \bar{A} \times (\bar{B} \times \bar{C}) = \bar{A} \cdot \bar{C} (\bar{B}) - \bar{A} \cdot \bar{B} (\bar{C})$$

$$\rightarrow \bar{A} \cdot \bar{B} \times \bar{C} = \begin{vmatrix} A_x & A_y & A_z \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{vmatrix}$$

### \* Coordinates systems:

1. Cartesian (or) rectangular coordinate system
2. Cylindrical coordinate system
3. Spherical coordinate system.

## ① Cartesian (or) Rectangular Coordinate System. 167

→ Any point in Cartesian system is the intersection of  $x = \text{constant}$ ,  $y = \text{constant}$  and the  $z = \text{constant}$  planes.

→ Point in Cartesian system =  $P(x, y, z)$

Unit vectors are  $\bar{a}_x, \bar{a}_y, \bar{a}_z$ .

$$d\bar{l} = dx, dy, dz$$

$$\rightarrow d\bar{l} = dx \bar{a}_x + dy \bar{a}_y + dz \bar{a}_z.$$

$$\rightarrow d\bar{s} = dy dz \hat{a}_x \quad (x = \text{constant})$$

$$d\bar{s} = dz dx \hat{a}_y \quad (y = \text{constant}).$$

$$d\bar{s} = dx dy \hat{a}_z \quad (z = \text{constant}).$$

$$\rightarrow dV = dx dy dz \circ$$

## ② Cylindrical System:

→ Point is  $(\rho, \phi, z)$ .

→ Unit vectors  $\bar{a}_\rho, \bar{a}_\phi, \bar{a}_z$ .

→ Differential lengths are  $d\rho, \rho d\phi, dz$ .

$$\rightarrow d\bar{l} = d\rho \bar{a}_\rho + \rho d\phi \bar{a}_\phi + dz \bar{a}_z.$$

$$d\bar{s} = \rho d\phi dz \hat{a}_\rho \quad (\rho = \text{constant}).$$

$$d\bar{s} = d\rho dz \hat{a}_\phi \quad (\phi = \text{constant}).$$

$$d\bar{s} = \rho d\rho d\phi \hat{a}_z \quad (z = \text{constant}).$$

③ Spherical coordinate system:

→  $P(r, \theta, \phi)$ .

→  $\hat{a}_r, \hat{a}_\theta, \hat{a}_\phi$ .

→  $dr, r d\theta, r \sin\theta d\phi$ .

→  $d\bar{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$  ( $r = \text{constant}$ )

→  $d\bar{s} = r \sin\theta dr d\phi \hat{a}_\theta$  ( $\theta = \text{constant}$ )

→  $d\bar{s} = r d\theta d\phi \hat{a}_\phi$  ( $\phi = \text{constant}$ )

→  $d\bar{r} = dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin\theta d\phi \hat{a}_\phi$ .

\* Transformation from Cartesian to cylindrical vectors and vice versa:

	$\bar{a}_x$	$\bar{a}_y$	$\bar{a}_z$
$\bar{a}_x$	$\cos\theta$	$-\sin\theta$	0
$\bar{a}_y$	$\sin\theta$	$\cos\theta$	0
$\bar{a}_z$	0	0	1

$x = \rho \cos\theta$   
 $y = \rho \sin\theta$   
 $z = z$

$[B]_y = [A^T] [B]_x$

$\rho = \sqrt{x^2 + y^2}$   
 $\theta = \tan^{-1}(y/x)$   
 $z = z$

\* Transformation of vectors from Cartesian to spherical or vice versa:

	$-\bar{a}_x$	$\bar{a}_y$	$\bar{a}_z$
$\bar{a}_x$	$\sin\theta \cos\phi$	$\cos\theta \cos\phi$	$-\sin\phi$
$\bar{a}_y$	$\sin\theta \sin\phi$	$\cos\theta \sin\phi$	$\cos\phi$
$\bar{a}_z$	$\cos\theta$	$-\sin\theta$	0

$x = r \sin\theta \cdot \cos\phi$   
 $y = r \sin\theta \cdot \sin\phi$   
 $z = r \cos\theta$

$r = \sqrt{x^2 + y^2 + z^2}$   
 $\theta = \cos^{-1}(z/r)$   
 $\phi = \tan^{-1}(y/x)$